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Final Technical Report  
June 1978



16 KILOBIT MODEM EVALUATION

Frank A. Perkins  
Daniel D. McRae

Harris Corporation  
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F30602-76-C-0460

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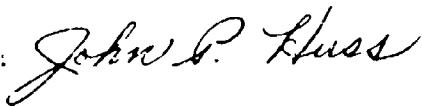
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19. KEY WORDS (Continue on reverse side if necessary and identify by block number) <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 33%;">Digital Networks</td> <td style="width: 33%;">Equalizer Weights</td> <td style="width: 33%;">8 kb/s Modem</td> </tr> <tr> <td>Key Generator Tests</td> <td>Modem Algorithms</td> <td></td> </tr> <tr> <td>Envelope Delay</td> <td>Telephone Modems</td> <td></td> </tr> <tr> <td>Amplitude Variation</td> <td>Secure Voice</td> <td></td> </tr> <tr> <td>Phase Jitter</td> <td>16 KB/S Modem</td> <td></td> </tr> </table>			Digital Networks	Equalizer Weights	8 kb/s Modem	Key Generator Tests	Modem Algorithms		Envelope Delay	Telephone Modems		Amplitude Variation	Secure Voice		Phase Jitter	16 KB/S Modem	
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Phase Jitter	16 KB/S Modem																
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)  The primary objective of this program was to perform extensive testing of the 16 kb/s modem on the AUTOVON network to establish the adequacy of the modem design. The goal was to provide good voice quality over the Network when used with 16 kb/s CVSD's. The modem was tested in Europe, the Pacific, on Trans-Atlantic and Trans-Pacific Networks and on some CONUS lines.  Test results were very encouraging and provide a high level of confidence that the modem design is sufficient to provide good voice quality over the																	

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existing AUTOVON Network as well as over planned network improvements.

In addition to excellent error rate performance, the modem demonstrated an extremely high probability of synchronization, even under very adverse conditions. The modem was able to achieve synchronization on all tested lines and considering all calls and all conditions, including extreme burst phenomena, the average synchronization probability was 96.4 percent.

Compared to presently operational 9.6 kb/s modems, the 16 kb/s modem using the same CVSD (Hy-11) provided essentially identical voice quality with error rates up to 3-5 percent as did the 9.6 kb/s system operating error free.

Only two classes of disturbances were found to significantly affect modem performance. These were harmonic distortion and fading associated with tropo links. Harmonic distortion is significant only in CONUS. Here the use of D conditioned lines, rather than existing C-3 conditioning will specify harmonic distortion to a satisfactory level. Tropo fades are significant only on European lines. For this application a good probability exists that additional or modified modem algorithms will provide significant immunity to fades. Even though the modem was found most sensitive to distortion and fading, the performance was satisfactory even on links exhibiting these characteristics.

Limited tests performed on existing digital links associated with the FKV project indicate that a high probability exists that the modem performance will not be degraded by the eventual digitization of the network.

A short HF link was tested in the Pacific resulting in adequate performance. However, the link was short and is not a true representation of HF phenomena on long links. The results, although not conclusive are encouraging.

Subsidiary program objectives included measurement of line parameters and characteristics and performance of interface tests with standard key generators to establish the level of synchronization loss relative to modem bit error rate. All of these objectives were accomplished.

Several logical recommendations regarding the 16 kb/s modem can be made. Research, Development, Test and Evaluation (RDT&E) units should be procured to provide a larger sample of modems for additional test as well as for user evaluation. Additional investigation should take place to determine modem algorithms which will improve performance in the presence of fades and high levels of harmonic distortion. Additional testing should be performed over HF simulators and active HF links to characterize modem performance as well as provide insight into additional algorithms that may provide enhanced performance.

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## EVALUATION

The Department of Defense requirement for an improved, inexpensive, end-to-end secure voice communications system using the existing analog AUTOVON Network has fostered the investigation of various secure voice transmission approaches. One such approach being considered is the 16 KBPS Continuously Variable-Slope Delta Modulation (CVSD) Digital Voice Technique which offers much improved speaker recognition and voice intelligibility as compared to that obtained with slower data rate digital voice systems presently available. This technique and moreover the use of existing narrowband (4kHz) voice channels of the AUTOVON Network have created the need for a 16 KB/S Modem.

Under a previous CY-75 program, practical 16 KBPS Modem techniques were developed to provide satisfactory voice quality with 16 KBPS CVSD on a large percentage of dialed-up calls on the AUTOVON Network. The 16 Kilobit Modem Evaluation Program is responsible for providing the first in-depth step in determining the adequacy of the 16 KBPS Modem design. Reliable modem operation was obtained over AUTOVON facilities in the CONUS, Europe and the Pacific, as well as over Transoceanic (satellite and subcable) transmission links.

Additional work will continue in this area to further evaluate the performance of the modem over the existing CONUS AUTOVON and commercial telephone networks. In addition, an Advanced Solid State Study will investigate the possible use of state-of-art microprocessor technology in implementing the successful 16 KBPS Modem design in future production versions. A follow-on 16 KBPS Modem Development Program, to be conducted in FY 78-79 time frame, will further refine the modem design with the objective of achieving operational hardware.



JOSEPH E. LAPOSA, Capt, USAF  
Project Engineer

## 1.0 INTRODUCTION AND BACKGROUND

### 1.1 Prior Study Activity

In February 1975 Harris Corporation was awarded a contract (F30602-75-C-0129) from the Rome Air Development Center (RADC) to study approaches available for developing a 16 kb/s modem capable of providing adequate voice quality over the AUTOVON network when operated with 16 kb/s continuously variable slope delta modulator (CVSD). The principal outcome of that study activity was a breadboard modem which was subsequently tested on a number of CONUS AUTOVON circuits from RADC with encouraging results.

The results of the study activities, as well as the test results are provided in the study final report.<sup>1</sup>

### 1.2 Objectives

Because of the favorable outcome of the first study program, RADC initiated a follow-on activity (Contract No. F30602-76-C-0460 ) with the following objectives:

- a. Repackage the breadboard modem to make it suitable for transporting overseas for testing.
- b. Modify selected modem algorithms to allow selection of optimum final design approaches during Overseas (OCONUS) testing.
- c. Plan and conduct tests on the Overseas Autovon network to determine the optimum approaches.
- d. Conduct interface tests with several standard key generators (KG's) to establish the level of synchronization loss relative to the modem bit error rate (BER).

### 1.3 General Outline

In this report consideration has been made first to the line test results and secondly, the supporting items such as design changes incorporated in the modem prior to testing and KG interface tests. Section 2.0 presents the results of the test program. Section 3.0 describes the various approaches which were tested and discusses other modifications made to the modem during the course of the program. Section 4.0 discusses the KG interface tests and Section 5.0 presents conclusions and recommendations. The Appendices contain the detail test data and supporting information.

### 2.0 TEST PHASE

Since a major objective of the test phase was to establish the adequacy of the design approach, the first step in planning the tests was a determination of the potential applications for the modem in the OCONUS network. Considerable effort was devoted to reviewing future plans for the digital network, and determining potential modem applications. A review of the findings of this effort are provided in Appendix A. Three categories of potential use are:

- a. Upgrading the voice quality compared to that presently available from the existing 2.4 kb/s vocoders and the 9.6 kb/s CVSD units in present use in the AUTOSEVOCOM network. This implies that the modem signal is treated as analog by all of the switches in the network independent of whether or not specific trunks may have been digitized.
- b. Interfacing subscriber locations which do not have digital service with the digital network. This implies that the modem signal is treated as an analog signal only on the access lines connecting the subscriber to the digital switch, and at that point is converted to a

digital signal for transmission over the digital network. This presupposes the existence of digital switches as well as digital trunks.

- c. Handling 16 kb/s digital traffic over interswitch trunks which either cannot be digitized or which will not be digitized in the earlier phases of the digital conversion. Specific examples of this are undersea cables and other leased Telpak service. However, it would appear that on an interim basis, interswitch trunks requiring tropo hops and commercial satellite links also fall in this category. In this case, several links may be in tandem and the error rates of the individual links will add.

It is apparent that the first category of use is the most demanding on modem performance since it requires operation of the modem over all segments of the network. However, testing which allowed conclusions to be drawn concerning the last two categories individually appeared prudent since inadequate modem performance for the first category would not necessarily imply inadequacy for the last two categories.

The remainder of this section presents material associated with testing. Paragraph 2.1 discusses the method of testing and other subjects necessary to understand and interpret the test results. Modem performance data obtained from all of the different test areas is provided in Paragraph 2.2. Paragraph 2.3 provides the line measurement data obtained in the test program. Paragraph 2.4 discusses the test procedures used to obtain these results. The comparative error rates obtained in the different modem modes that were tested are presented in Paragraph 2.5.

## 2.1        Test Philosophy

Before presenting the test results several items need to be presented so that the results can be understood and properly interpreted. This section discusses the range of CVSD error rates necessary to provide adequate voice quality, the nature and types of tests conducted and a brief review of the AUTOVON network.

The objective of the test program was to establish the best modem design approach and to evaluate the adequacy of that approach in the network. The "adequacy" in this case means the adequacy of the voice quality available from the modem in conjunction with an appropriate 16 kb/s CVSD unit. The adequacy of the modem from the standpoint of operational features and maintainability was not evaluated at this time since only an advanced breadboard unit was used in the test program.

The CVSD unit used during the tests was the HY-11 which is presently being used in the network for the 9.6 kb/s service. Voice recordings as well as BER measurements were made on the majority of calls. Although the voice recordings are quite interesting, in virtually all cases the general quality of the voice is quite predictable from the BER numbers. If the listener is listening to the conversation rather than specifically listening to the background noise he will likely not notice the noise increase due to the modem until the BER exceeds  $10^{-2}$  or 1%. At 2% the noise is noticeable but does not impair the conversation. At a BER of 5% the noise is objectionable but a reliable conversation can easily be held. At a BER of 10% abbreviated communications are possible, such as a request to hang up and call back on another line, but in general, the quality is unsatisfactory. Based upon the subjective judgment of the test teams, the quality of the voice provided by the HY-11 operating at 9.6 kb/s error free is approximately equivalent to that provided by the HY-11 at 16 kb/s operating with an error rate between 3% and 5%.

The approach taken in planning the modem tests was to attempt to maximize the number of locations and routings involved with the calls. Seven test sites were selected, three in Europe, three in the U.S. and one in the Pacific. The three European sites were: Hillingdon, England; Feldberg, Germany; and Coltno, Italy. The Pacific site was Pearl Harbor on Oahu, Hawaii. The three U.S. sites utilized were: Ft. Dietrich, Maryland; Stockton, California; and Melbourne, Florida.

A combination of one way calls and loop around calls were used. Since the advanced breadboard modem from the original study contract contained only one

transmitter and one receiver, a second transmitter was constructed for the tests. The bulk of the calls were planned to be loop-around calls conducted from the site of the modem. In addition to these calls a number of one-way calls were planned from the transmitter site to the modem site. On these calls the parameters were measured for both one-way calls and looped calls on the same line so that estimates might be made as to the probable performance of normal one-way calls on the lines measured by the loop-around technique.

The results given in Paragraph 2.2.1 indicate that the error rates achieved on loop-around calls were substantially worse than those obtained on one-way calls on the same lines. Therefore, to fairly interpret the loop-around results it is necessary to recognize that substantial improvement should exist if the same two locations were involved in a normal one-way call.

The tests were divided into the following five segments:

- a) European network tests
- b) Tests from Europe to CONUS or Trans-Atlantic tests
- c) Pacific network tests
- d) Tests from Hawaii to CONUS or Trans-Pacific tests
- e) CONUS network tests

As discussed in Appendix A the AUTOVON system can be thought of as four networks connected together. The European network has ten AUTOVON switches that supply telephone service to over 100 subscriber locations. The Pacific network has four AUTOVON switches which serve a smaller number of subscriber locations. The Caribbean network has only one switch which serves a relatively small number of subscriber locations. The CONUS network has 70 switches serving a large number of subscriber locations. The four networks making up the AUTOVON system are interconnected via "gateway switches."

There are three gateway switches in Europe that connect to two CONUS gateway switches. Similarly the Pacific network has three gateway switches which connect to two different CONUS gateway switches.

Within one of the networks it is convenient to think in terms of two categories of trunks and channels. These are those that connect the switches together (interswitch trunks, or IST's), and those that connect a subscriber location to a switch (access lines). In the European network testing, four varieties of calls were made. These were:

- a) IST loop-around calls
- b) IST one-way calls
- c) Access line loop-around calls
- d) Remote access line loop-around calls

The remote access line calls were calls to a subscriber of a switch other than the switch where the modem was located. Thus the calls involved both IST and access lines. The calls in the Pacific network were limited to IST loops and remote access loops. Since only one Pacific site was used, no one-way tests were conducted. The Pacific calls all involved an access line from Pearl Harbor to the switch at Wahiawa in addition to the IST's and remote access lines where these were involved. However, the access line to Wahiawa was extremely good so that the performance should not be significantly affected by it. Access lines from the Wahiawa switch were not tested because it was felt that the data obtained from remote access calls would be of greater interest. Hence, calls involving access lines off other switches were selected instead.

The trans-Atlantic calls were conducted from Hillingdon, England, one of the gateway switches, to Ft. Dietrich, Maryland. The trans-Pacific calls were conducted from Pearl Harbor, Hawaii to Stockton, California. Both one-way and looped calls were

made on these connections. The CONUS calls were all loop-around calls from Melbourne, Florida to various CONUS switches. These have been categorized as IST loops since it is felt that the access lines from Melbourne to the switch at Polk City, Florida are not likely to adversely affect modem performance.

The AUTOVON network contains lines with different quality specifications. On interswitch circuits outside of CONUS, these lines are either V2 or S3 (voice grade or data grade) conditioned. On a normal dialed call, the AUTOVON switch will first try the voice grade lines, and if they are busy, it will then try the data grade lines. By dialing a special prefix the switch will try only data grade lines. All of the access lines to normal PBX exchanges in Europe are voice grade. All of the access lines to AUTOSEVOCOM subscribers are data grade. The AUTOSEVOCOM network is presently designed to utilize data grade lines only.

Most of the calls placed during the modem tests were placed without dialing the data prefix. The majority of loop-around calls to access locations were placed to PBX locations and hence were voice grade lines. Thus the data obtained should be representative of that available when the modem is used on the voice grade lines as well as on the data grade lines.

The modem was tested in four different modes. A comparison of performance in these modes is given in Paragraph 2.5. All of the data presented in the Paragraph 2.2 applies to operation in the "standard mode." A description of the modes is given in Paragraph 3.5.

A detailed schedule for all of the testing, except CONUS, is given in Appendix B. The CONUS tests were conducted from the Harris ESD facility in Melbourne, Florida subsequent to the other tests.

## **2.2      Modem Test Results**

This section is subdivided into five parts. The primary test results are presented in Paragraph 2.2.1. Paragraph 2.2.2 discusses the degree of network coverage which was achieved in the testing. Paragraph 2.2.3 provides data as an aid to correlating the difference between one-way and looped calls. Paragraph 2.2.4 discusses interpretation of the basic modem performance data if calls from one network to another were involved. Paragraph 2.2.5 discusses results obtained in "special calls" which did not fall into any of the categories of calls presented in Paragraph 2.2.1.

### 2.2.1 Test Results

This section presents summarized results of the error rate data given in the tables of Appendix C, which give a complete listing of all measurements taken on each call. Perhaps the best overall summary of the 16 kb modem test results is given in Table 2.2.1-1. As can be seen, a total of 334 calls are included in the nine categories listed. The percentage of calls with bit error rate equal to or better than 1 percent, 2 percent and 5 percent are given. As previously explained, these error rates correspond to good, fair, and poor voice quality when taking the CVSD's into consideration. The quality of the 16 kb voice at 5 percent, however, is not much worse than that of 9.6 kb CVSD voice error free. In the categories involving loop-around calls, both the line percentiles corresponding to the actual error rates and those corresponding to the predicted one-way error rates are given. The conversion is that of the conservative curve given in Figure 2.2.3.

In addition to the BER data given, the total number of syncs and the number of sync successes for each category of line test is given. It should be noted that the probability of obtaining successful synchronization (sync) was better than 50 percent on each of the individual calls and was 96.4 percent averaged over all calls. Thus, there were no lines tested where sync could not be achieved. However, a number of lines in European tests had burst phenomena that caused a missed sync to occur during the test. The normal line test involved several syncs per call.

Approximately half of the sync misses occurring in the European tests occurred within the 2 days preceding the detection of an equipment malfunction which caused unreliable synchronization. This malfunction involved a logic circuit that produced excessive delay when cold. The problem was eliminated when the defective circuit was located and replaced. Since it was not possible to separate the sync misses due to this cause and those legitimately due to line characteristics, all sync misses have been included in the table. In any case, fades in the signal on calls involving tropo

Table 2.2.1-1. Summary of 16 kb Test Results

Type of Call	Total	Successful	Calls with BER ≤ 5%	% of Looped Calls with BER ≤ 5%		% of One-Way Calls with BER ≤ 5%		Synchronization Performance	
				2%	1%	2%	1%	Tries	Successes %
European IST Loops	85	1.03E-3	92	80	70	100	98	96	346
Pacific IST Loops	25	4.50E-4	100	99	97	100	100	93	93
CONUS IST Loops	78	4.70E-3	100	85	80	100	100	234	100
European IST One-Way	21	5.40E-4	-	-	-	100	96	90	91
Trans-Atlantic One-Way	32	4.00E-3	-	-	-	100	92	75	161
Trans-Pacific One-Way	24	1.18E-4	-	-	-	100	100	99	109
European Access Loops	34	3.80E-5	100	99	97	100	100	100	151
European Remote Access Loops	26	1.03E-2	85	66	46	95	93	88	118
Pacific Remote Access Loops	9	3.80E-3	89	73	67	100	100	27	27
Total	334							1330	1282
									96.4

transmission were still a significant cause of sync misses. Even so, the percentage of successful syncs is quite reasonable, especially where degradation of loop-around calls is considered.

Loop-around data, as well as one-way data, was taken on most of the trans-Atlantic and trans-Pacific calls. This data is presented in Tables C.5 and C.6 of Appendix C but was not reduced for presentation in this section since all of these looped calls had corresponding one-way calls and hence are of no value in improving the prediction of one-way performance of trans-Atlantic and trans-Pacific calls. They have been used, however, to compare one-way versus looped performance in general, and are tabulated in Tables 2.2.3-2 and 2.2.3-3 of Paragraph 2.2.3. The looped data on the trans-Pacific calls was generally similar to looped performance of European calls but the looped data on trans-Atlantic calls was considerably worse. This appeared to be due to the high levels of harmonic distortion present in the one-way trans-Atlantic calls which was nearly doubled for looped calls. Although the looped trans-Atlantic performance was generally unsatisfactory, the actual one-way performance on the same lines was acceptable.

Table 2.2.1-2 presents a summary of the 8 kb test results. No attempt has been made to convert looped performance to one-way performance for the 8 kb test. As will be discussed in more detail later, the block throughput figures are the percentage of 8000-bit blocks that were transmitted error free.

Figures 2.2.1-1 through 2.2.1-3 show the percent of the lines which provided performance equal to or better than a specified bit error rate. The curves are for the IST loop-around calls for the European, Pacific and CONUS network, respectively. Included on the curves is the same information for 8 kb tests that were conducted on the same lines used for the 16 kb tests. These curves present the error rates as measured directly on the loop-around calls and do not have a loop-around to one-way conversion factor applied. The 16 kb error rates were obtained by recording the first five 10-second error counts following completion of modem training. In some cases, burst phenomena, such as dropouts, occurred in only one of the five counts. In calculating the error rates shown in the curves of this section, the error caused by these anomalies has been included

although there is same argument that the error rate which determines voice quality should not include errors of this nature. In cases where comparison of performance is involved, such as the comparison of error rates for the different modem modes and comparison of one-way versus looped performance, these anomalous counts have been omitted since they do not bear on the relative performance of the techniques being investigated.

The 8 kb error rates were obtained by recording the errors in the first 100 1-second periods following modem training. These error counts were used to calculate both 8 kb BER and block throughput. The block throughput is defined as the percent of 1 second counts that contained no errors. Thus a "block" of data for the purposes of this test was defined as 8000 bits. This produces a lower block throughput number than would exist for a smaller block length. This should be taken into account in any comparison of results. In all cases, anomalous counts in the 8 kb measurements were included in calculating both BER and block throughput.

Table 2.2.1-2. Summary of 8 kb Test Results

<u>Type of Call</u>	<u>Percent of Calls With BER <math>\leq</math></u>		<u>Median BER</u>	<u>Median Block Throughput</u>
	$10^{-4}$	$10^{-5}$		
European IST Loops	79%	47%	$1.5 \times 10^{-5}$	99.3
Pacific IST Loops	94%	92%	$< 10^{-5}$	100
CONUS IST Loops	99%	89%	$< 10^{-5}$	100
European IST One-Way	83%	55%	$< 10^{-5}$	95.5
Trans-Atlantic One-Way	97%	76%	$< 10^{-5}$	100
Trans-Pacific One-Way	96%	84%	$< 10^{-5}$	100
European Access Loops	94%	83%	$< 10^{-5}$	100
European Remote Access Loops	59%	35%	$5.2 \times 10^{-5}$	96.6
Pacific Remote Access Loops	83%	73%	$< 10^{-5}$	100

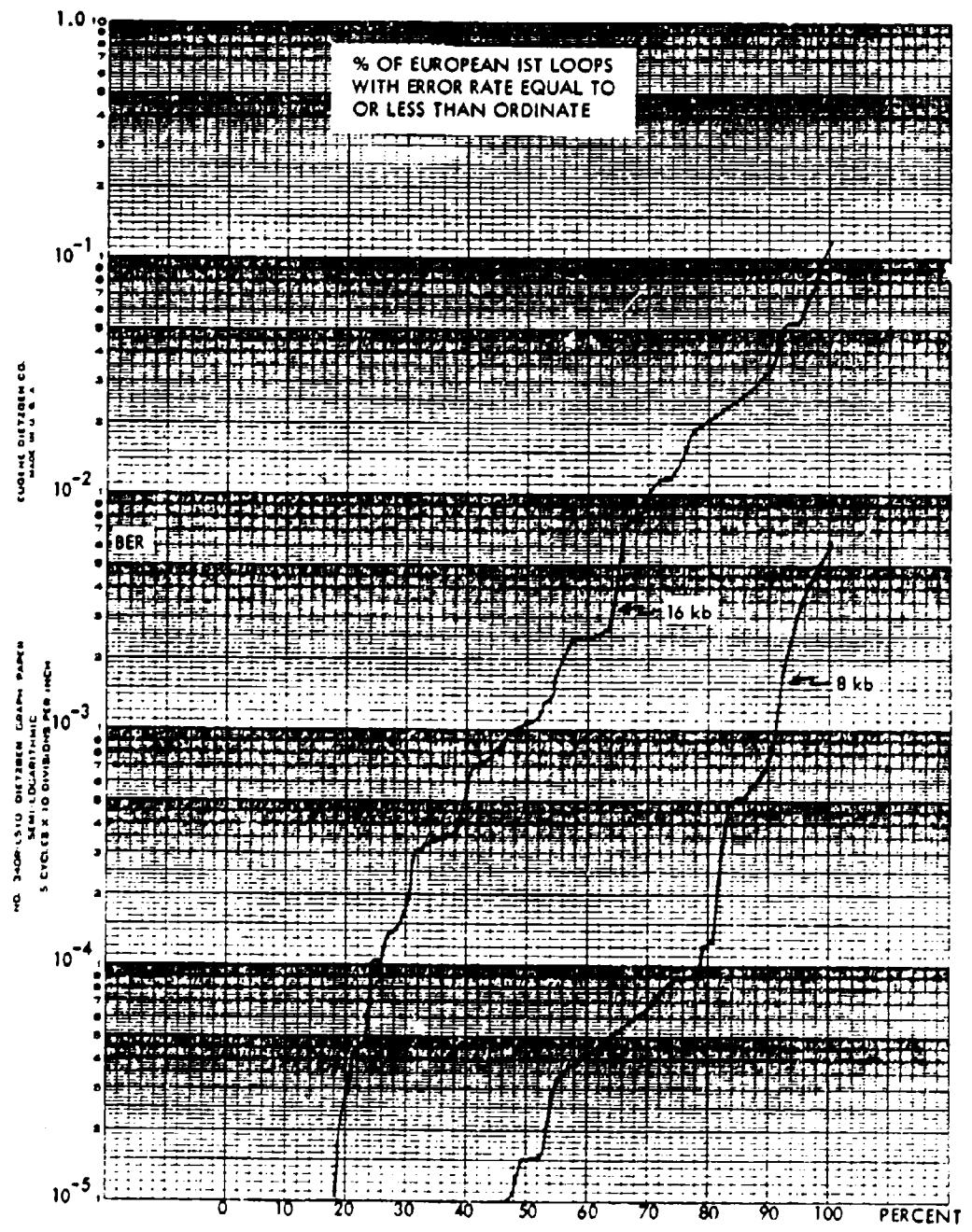


Figure 2.2.1-1

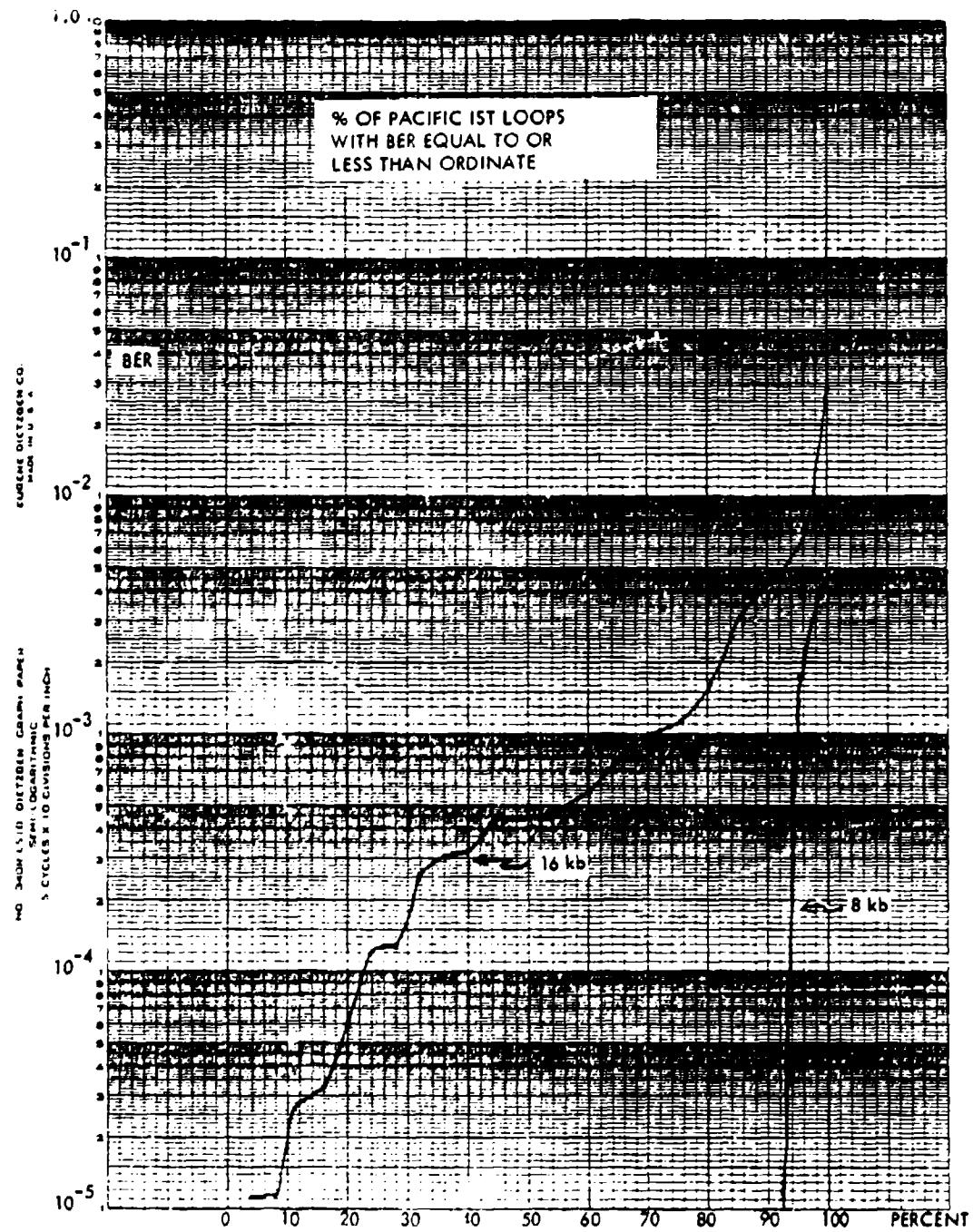


Figure 2.2.1-2

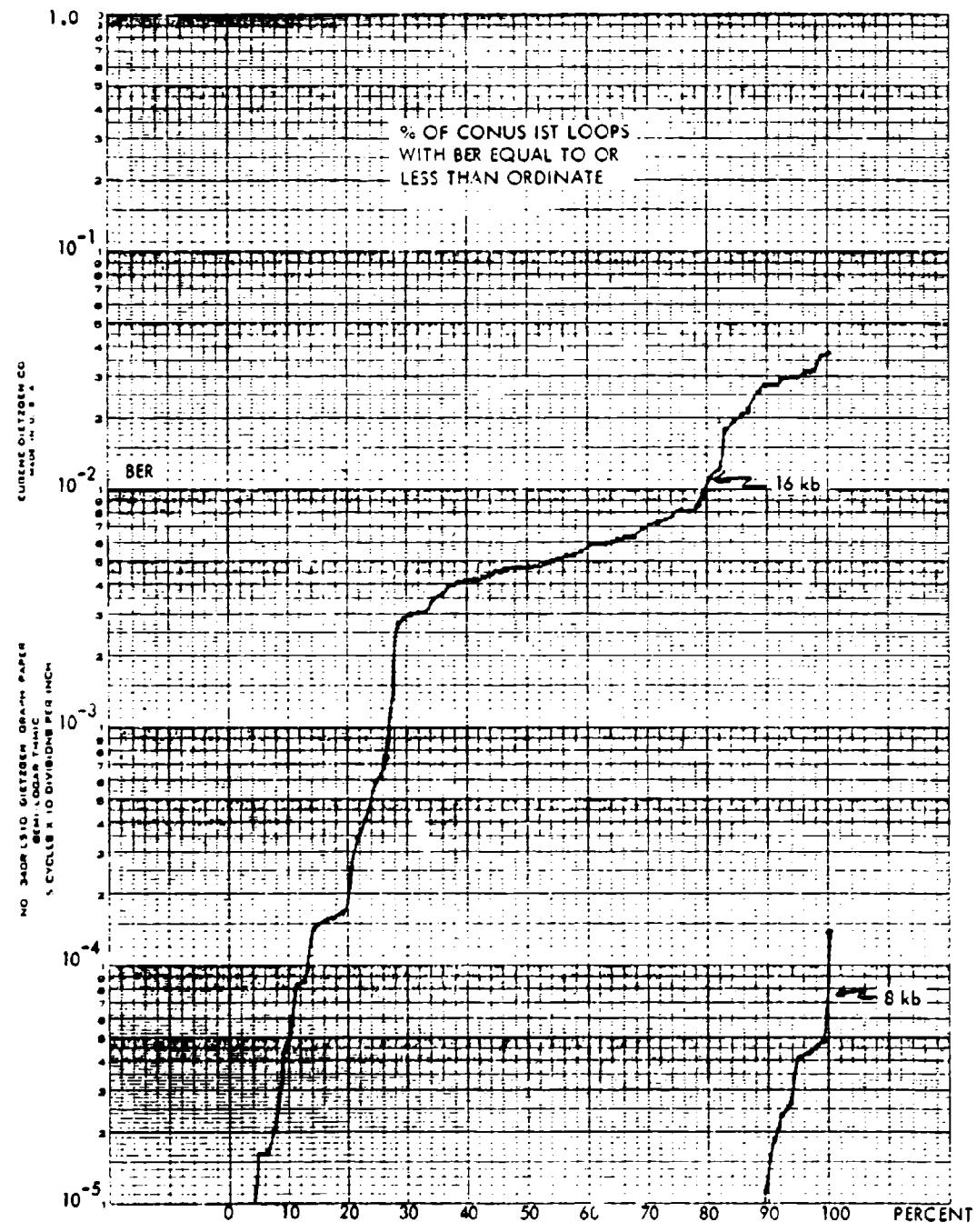


Figure 2.2.1-3

The performance curves for the three networks are interesting in that they reflect the effects of the two types of disturbance that present the greatest difficulty to the modem. These are fades associated with tropo links and harmonic distortion. The Pacific IST loops exhibited neither of these problems with the exception of two or three calls which involved tropo. The European error rates were dominated by the calls over tropo links which constitute approximately 60 percent of the calls. The CONUS lines do not involve tropo links but many of them do exhibit relatively high harmonic distortion content.

Figures 2.2.1-4, 2.2.1-5, and 2.2.1-6 indicate the performance of the one-way European, the one-way trans-Atlantic and the one-way trans-Pacific calls. The one-way trans-Atlantic calls were also characterized by relatively high harmonic distortion. Some evidence exists, however, that the primary cause of the distortion was the access line from the CONUS gateway switch to Ft. Dietrich rather than the actual trans-Atlantic lines. The harmonic distortion on the trans-Pacific calls was considerably smaller with resulting improvement in error rate.

Figures 2.2.1-7, 2.2.1-8, and 2.2.1-9 show the performance of the European access loops and the European and Pacific remote access loops. The performance shown in both of the remote access loop curves is dominated by the effects of tropo links. As discussed below, a number of these remote loops exhibited large line losses when the actual line loss should have been zero.

It was felt that in a number of these cases, the problem was due to the patching arrangement which was necessary at the remote switch to avoid insertion of an echo suppressor, or due to the manual loop patch, at the remote access location to provide the loop-around. The coordination of these calls was quite difficult from a communications standpoint and verification of the patching arrangements was not always possible. For instance, call 114, a remote loop to Vicenza, Italy from Feldberg, Germany, exhibited 16 dB line loss and provided a 16 kb error rate of 1.05 percent. The line was preempted before complete data was taken. A second call (115) to Vicenza was

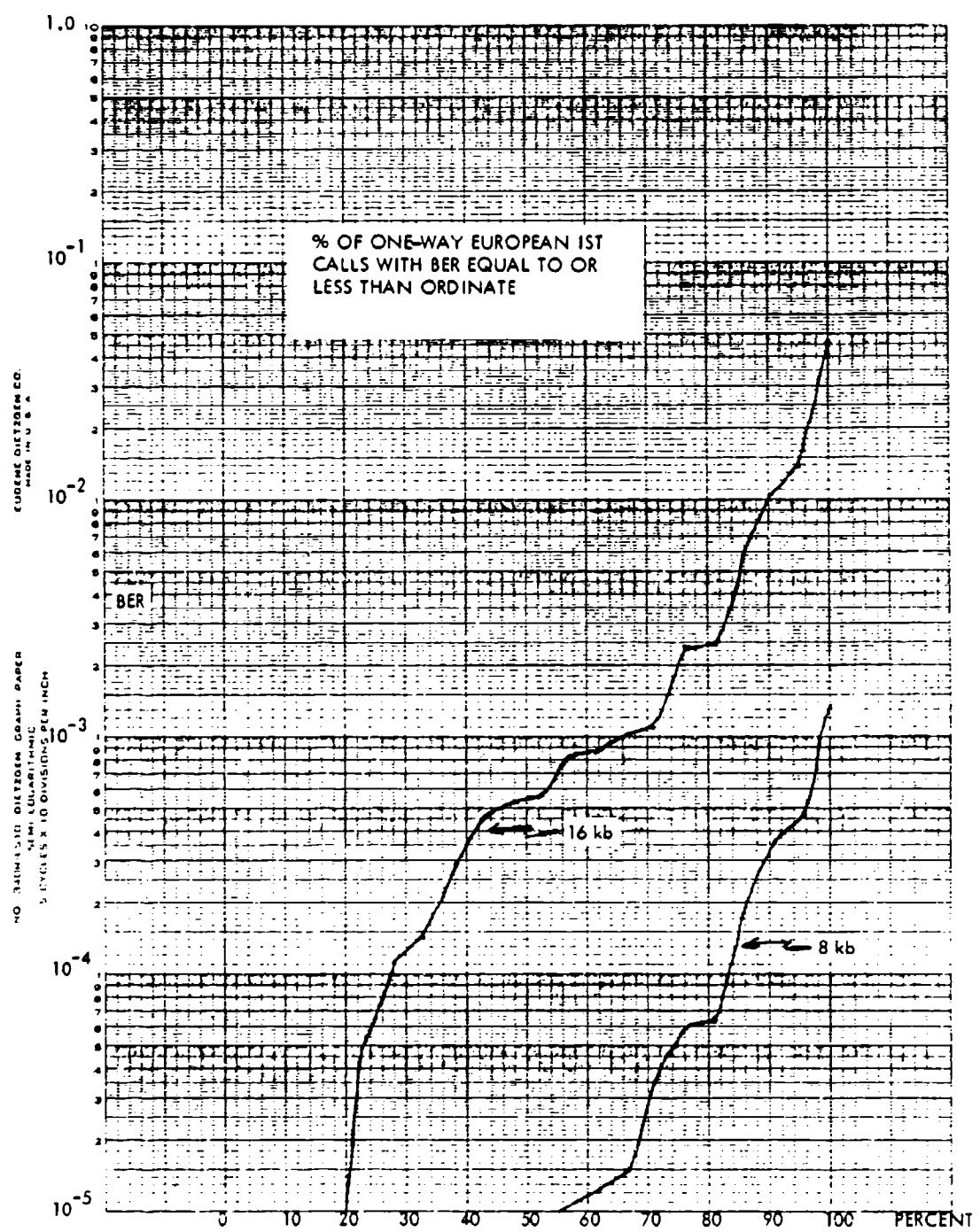


Figure 2.2.1-4

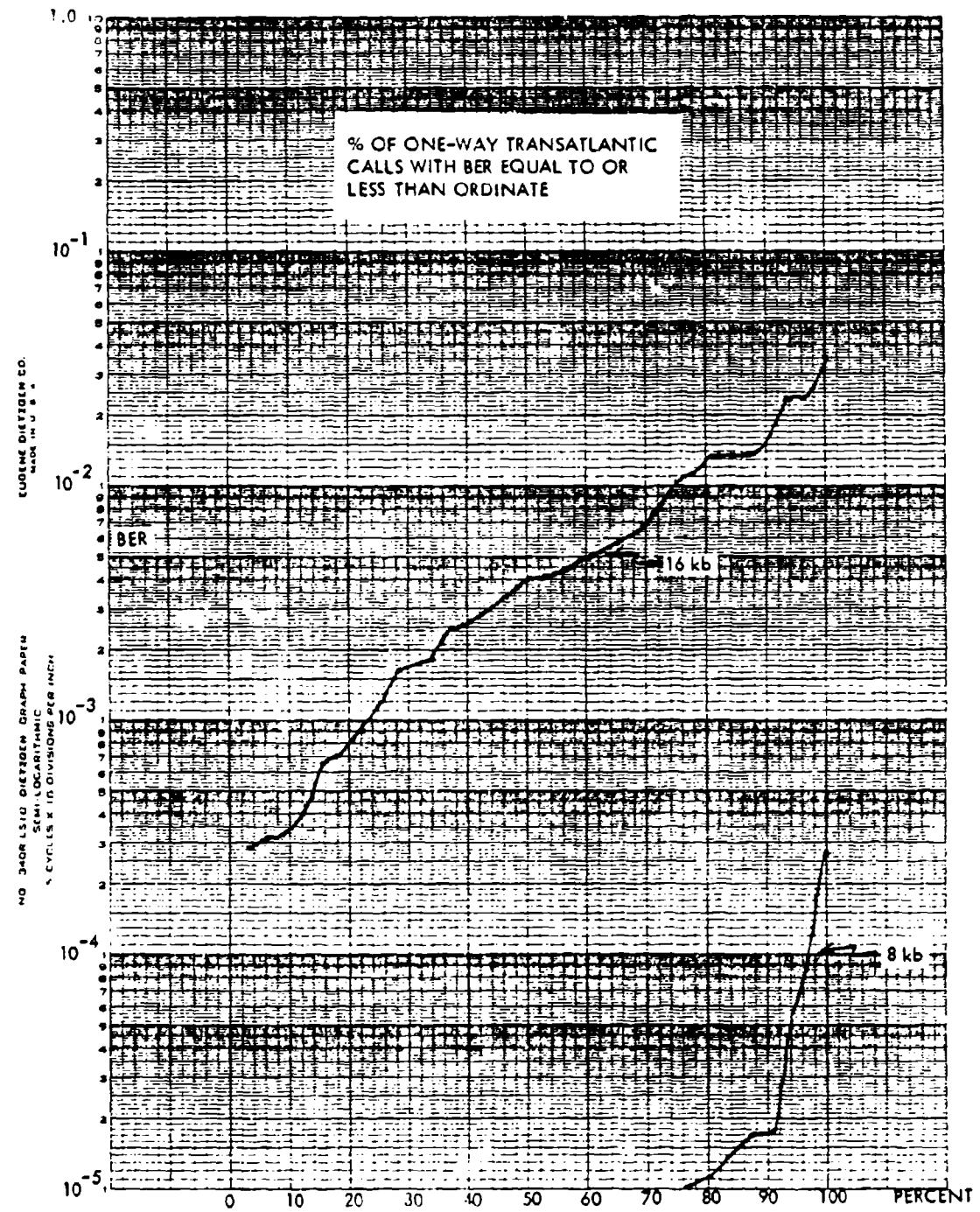


Figure 2.2.1-5

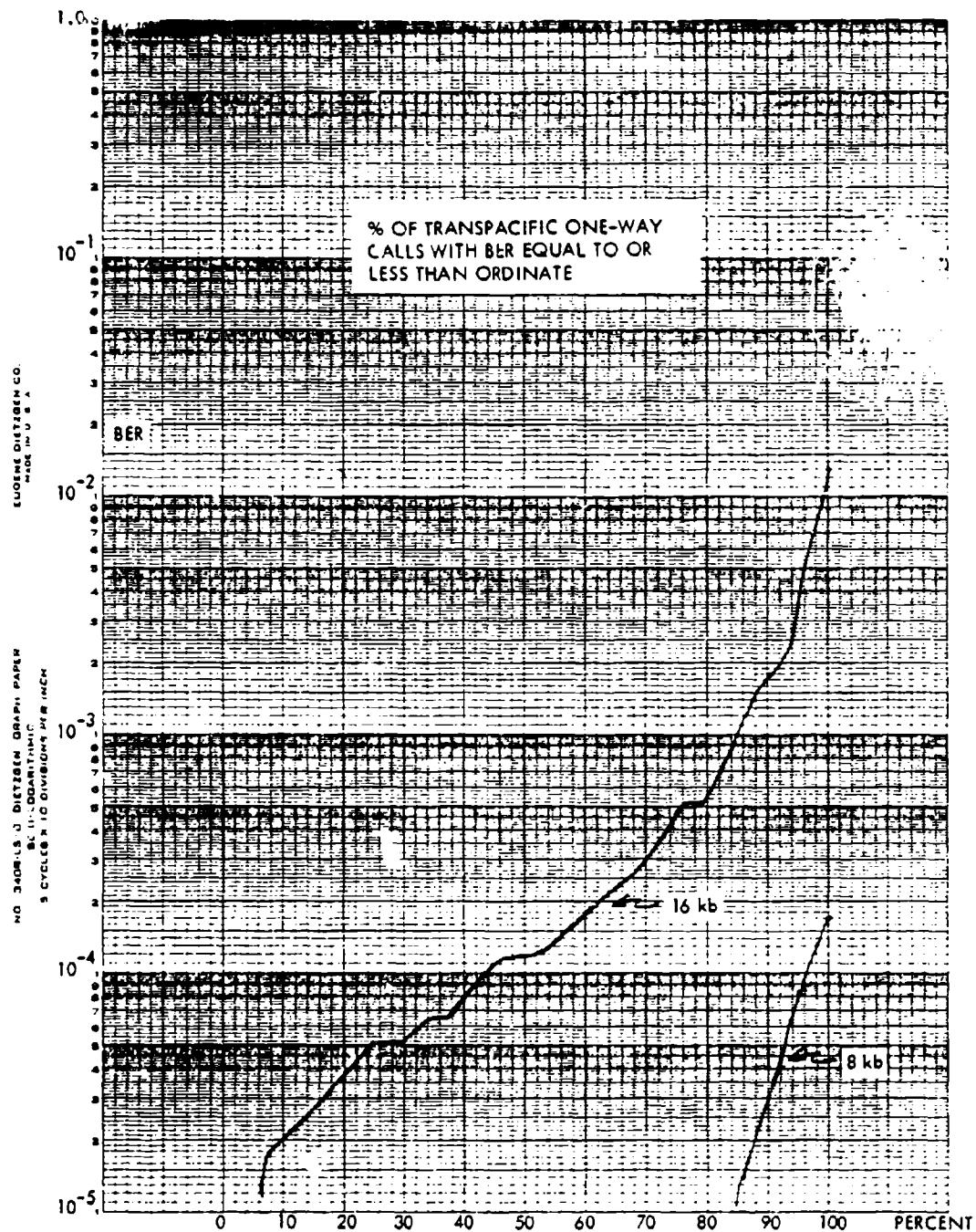


Figure 2.2.1-6

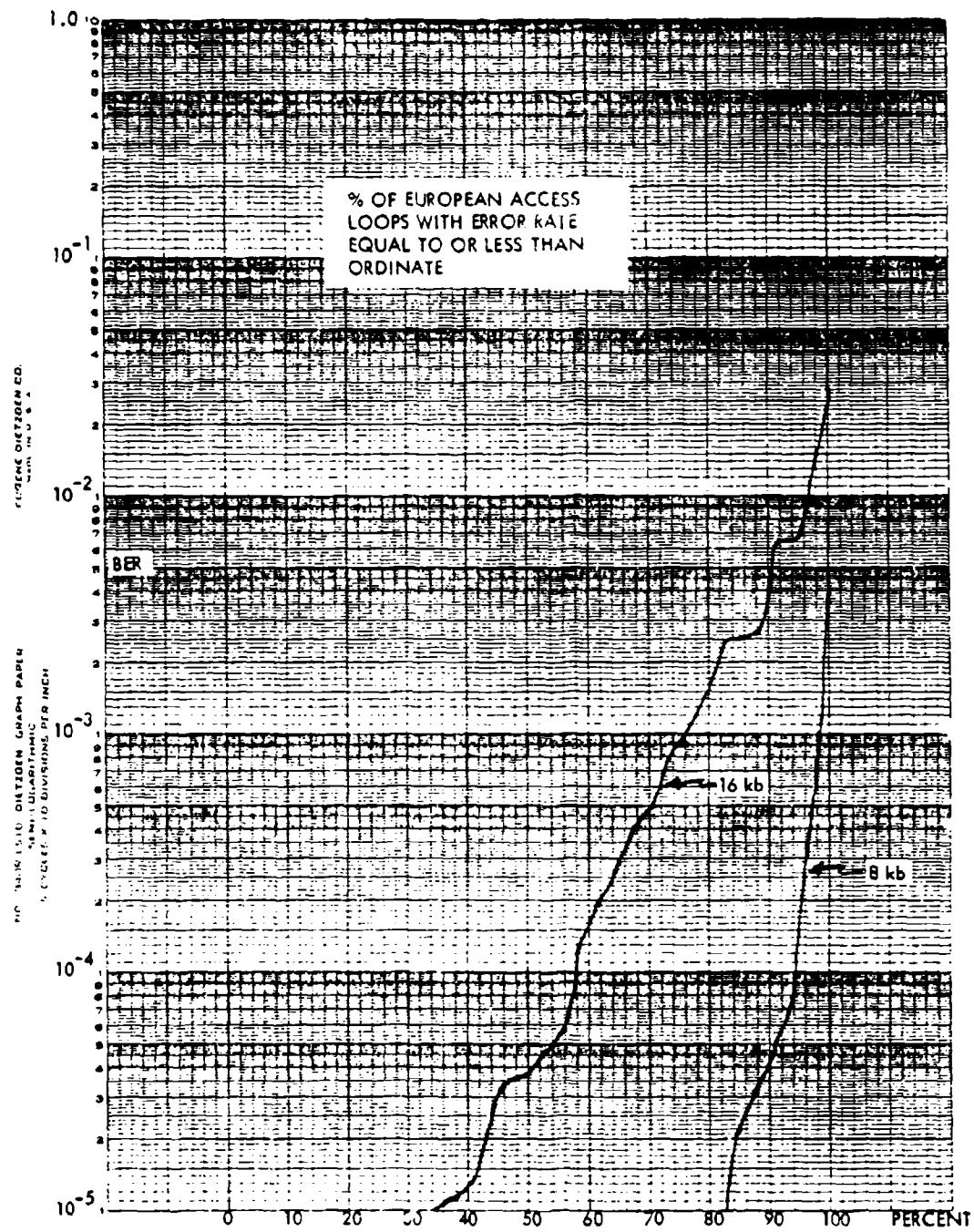


Figure 2.2.1-7

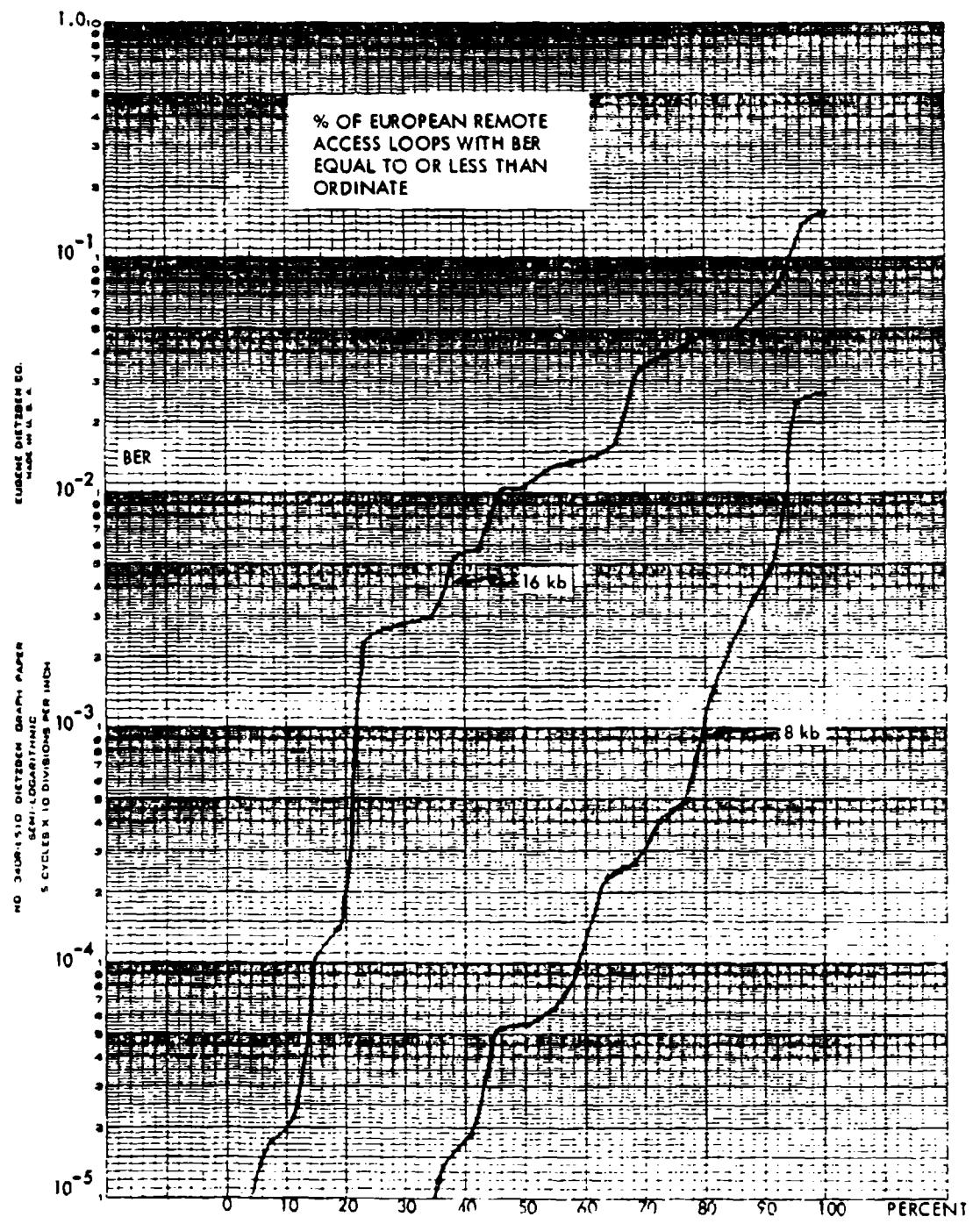


Figure 2.2.1-8

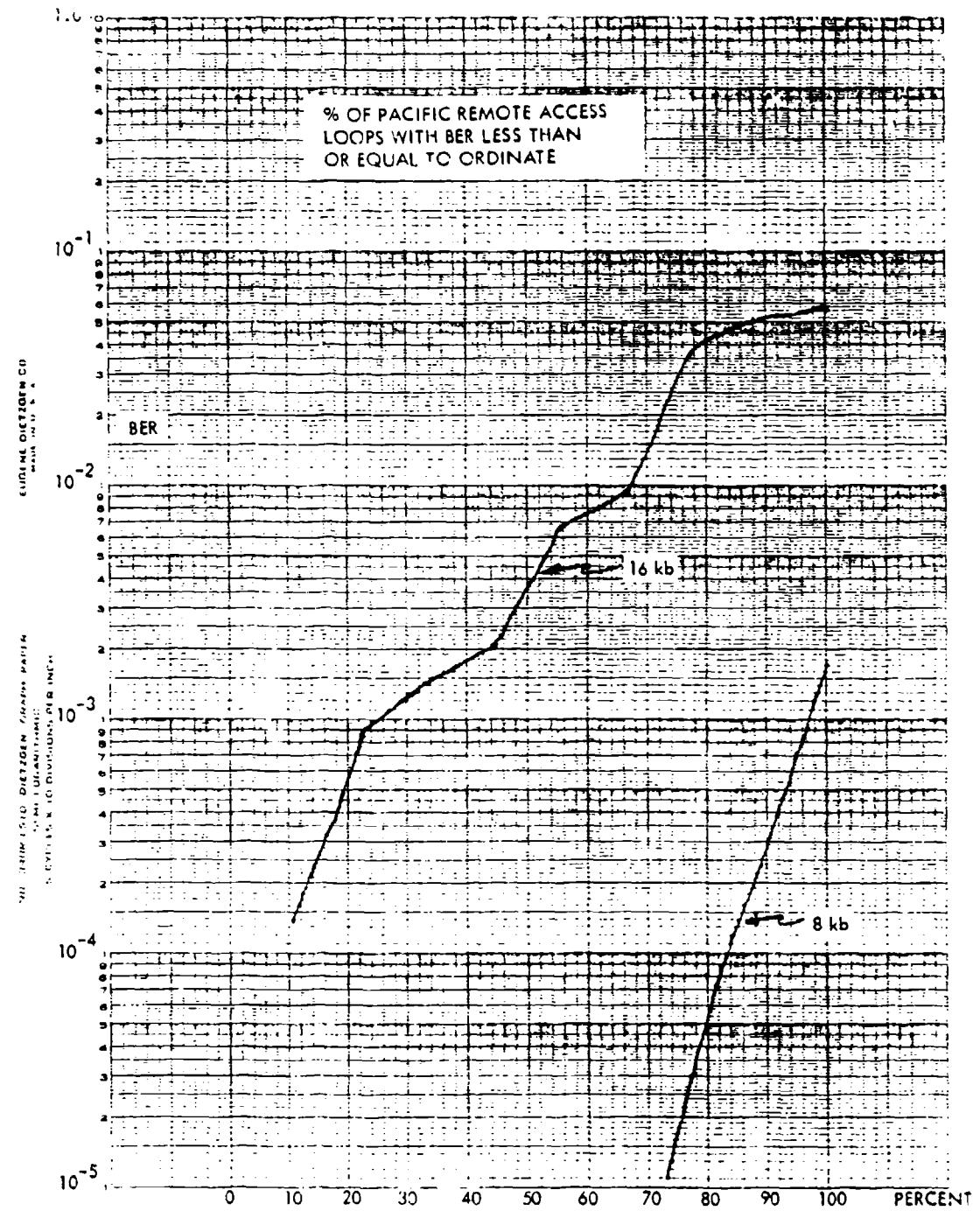


Figure 2.2.1-9

established over the same circuits as soon as the line became free. This time different personnel were utilized to provide the patches and the line loss was 6 dB with a resulting error rate of 0.229 percent.

As previously mentioned, the performance of the European calls and to a lesser extent, the Pacific calls was dominated by the error rates associated with those calls transiting tropo links. Of the 85 European IST loop calls, 49 of these transited one or more tropo links, and 33 did not involve tropo. (Calls with uncertain routing were excluded.) The median number of tropo links transited in these calls (taking into account the looped configuration) was six, and several IST loops transited 14 tandem tropo hops. Figure 2.2.1-10 shows the BER performance of the European IST loops separated into categories of those calls with one or more tropo hops and those with none. As can be seen, the worst error rate of the 33 loops which did not involve tropo was  $5 \times 10^{-3}$ . In addition to this categorization, it was noted that many of the calls with the worst error rates transited tropo link, T0055, between Coltano and Mt. Limbara. If those calls were excluded from the 49 calls involving tropo, it can be seen that the resulting performance of the remaining tropo links is better than that of all calls including the microwave links. The specific cause for the poor performance over this one link was not determined since the correlation was not discovered until after the tests were completed.

Figure 2.2.1-11 shows similar results for the one-way European IST calls. Twelve of the one-way calls involved tropo while eight did not. Figure 2.2.1-12 presents the performance with and without tropo for the European access loops. There were eight access calls involving tropo and 26 that did not. None of the access lines transited T0055. Figure 2.2.1-13 shows the results for the remote access lines in Europe. In this case, 18 calls involved tropo whereas eight did not. Again, omission of the tropo calls transiting T0055 makes a significant difference. Figures 2.2.1-14 and 2.2.1-15 present the performance with and without tropo for the Pacific calls. The effect is less pronounced in these cases because the number of calls involving tropo is much less. In the Pacific IST

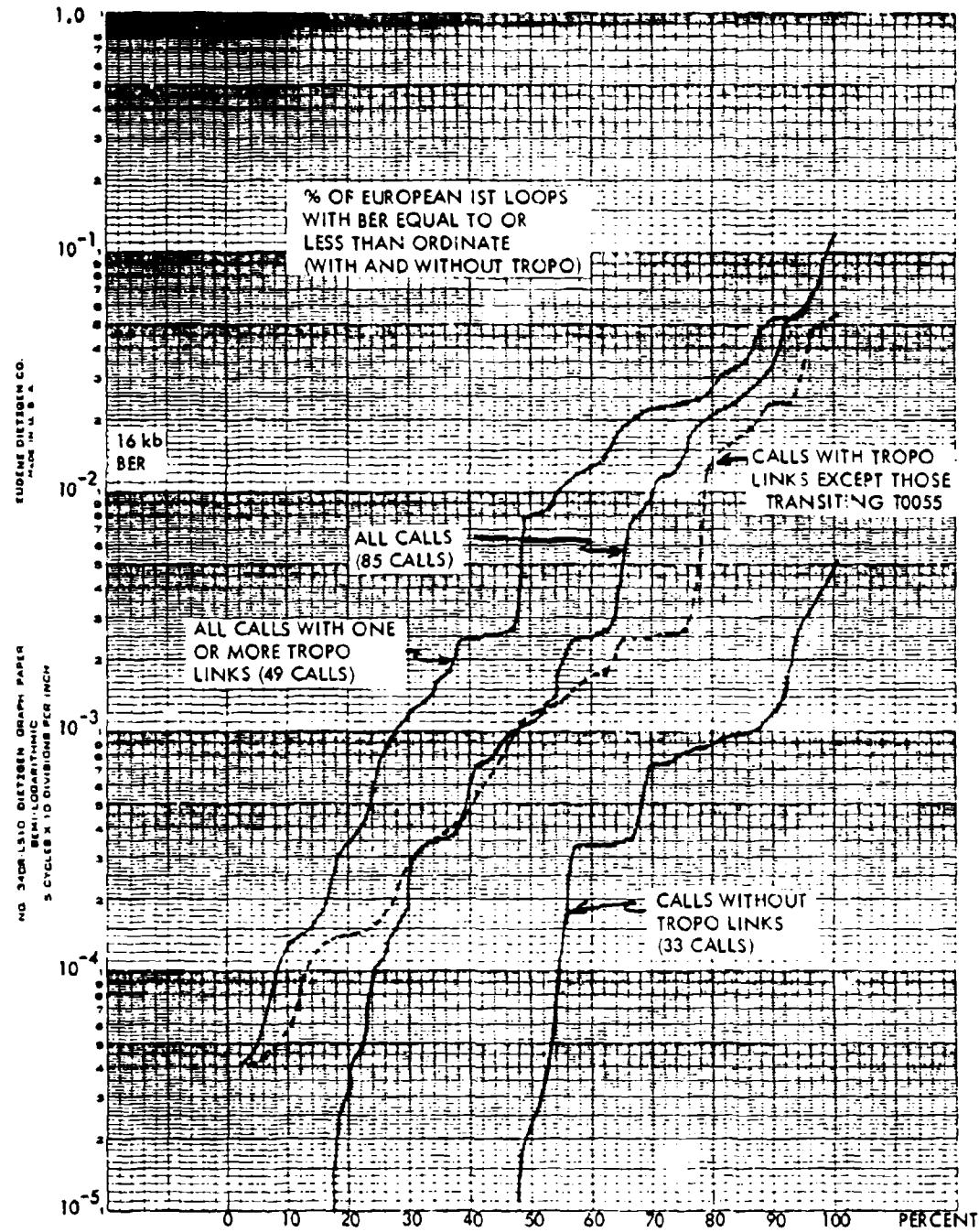


Figure 2.2.1-10

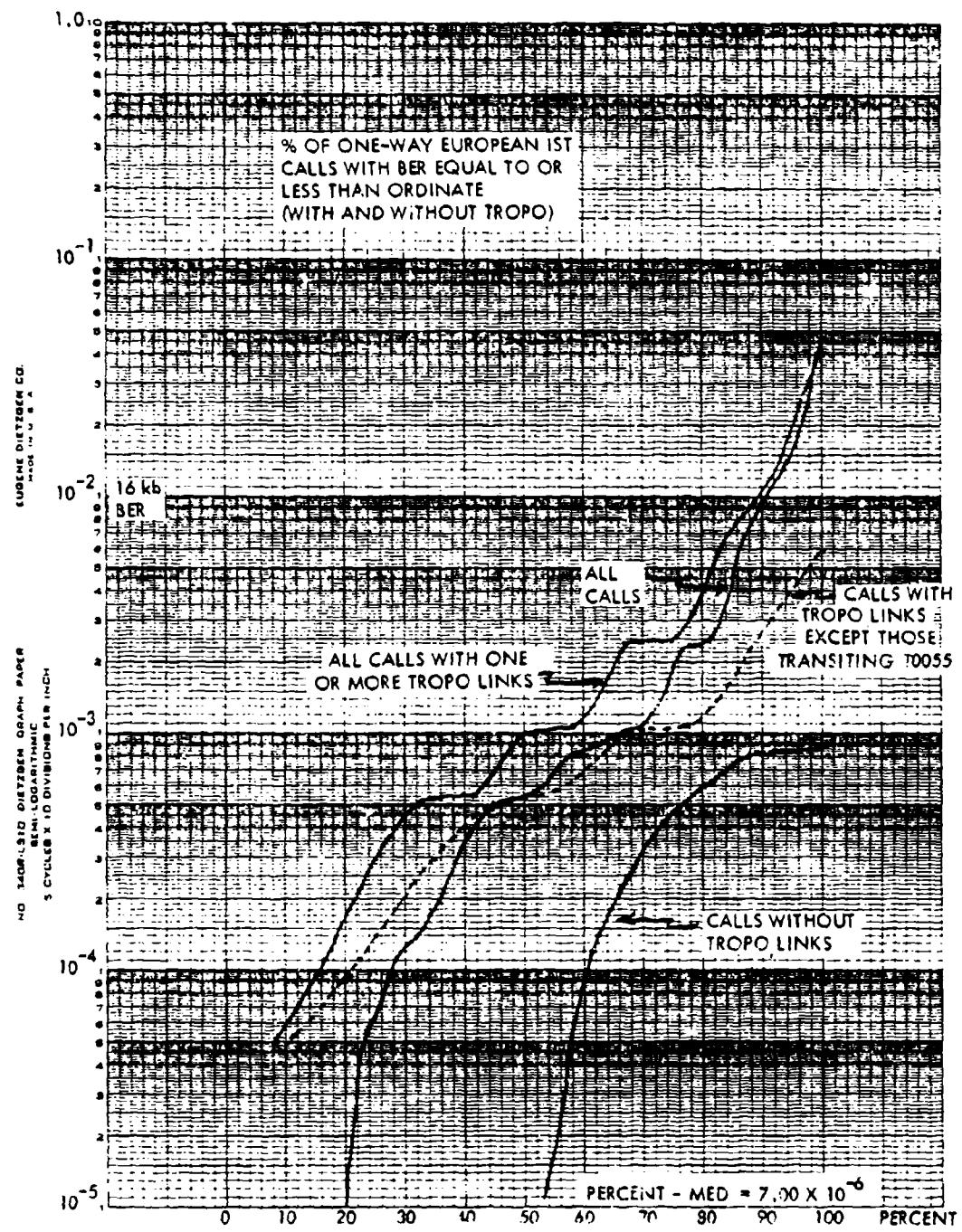


Figure 2.2.1-11

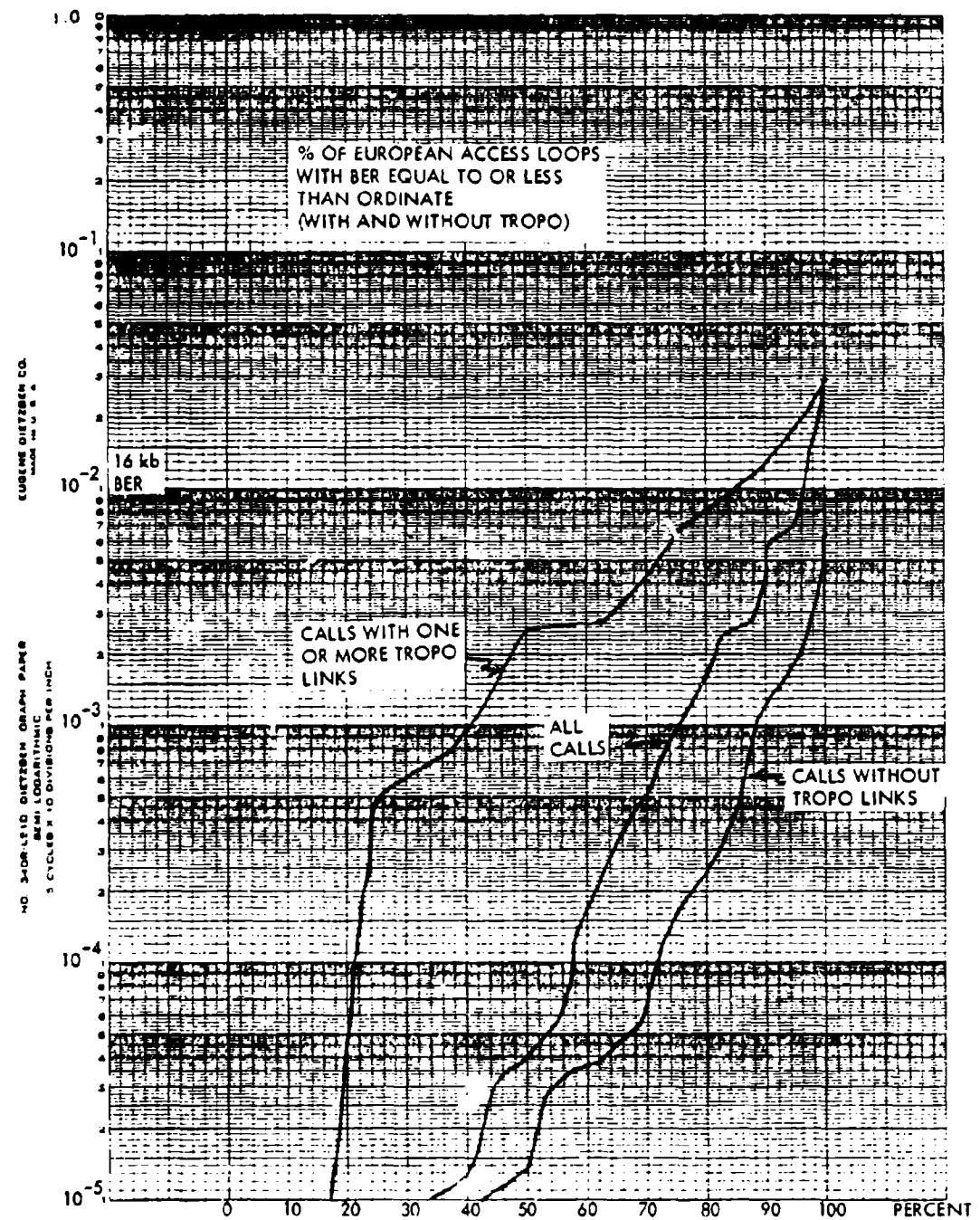


Figure 2.2.1-12

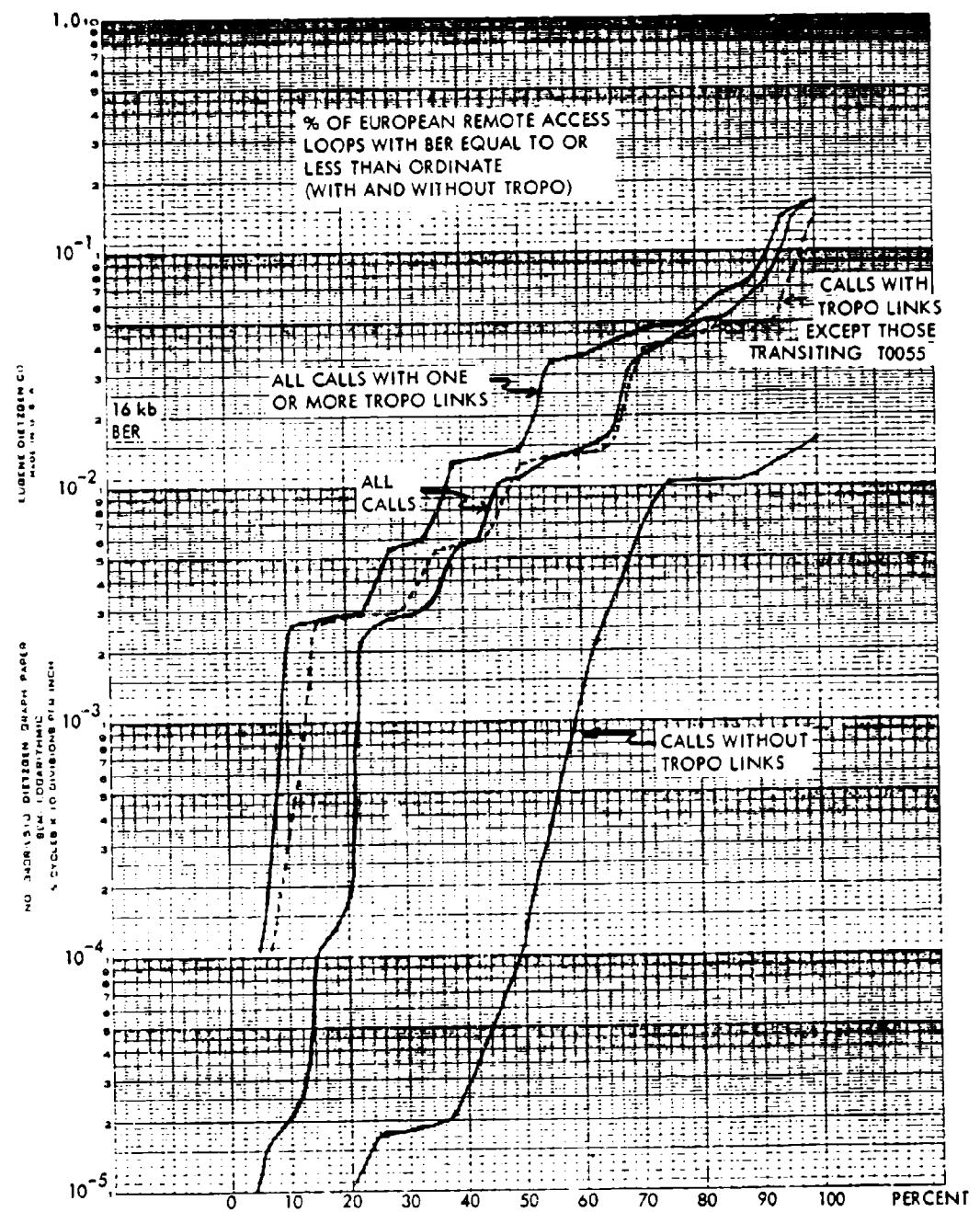


Figure 2.2.1-13

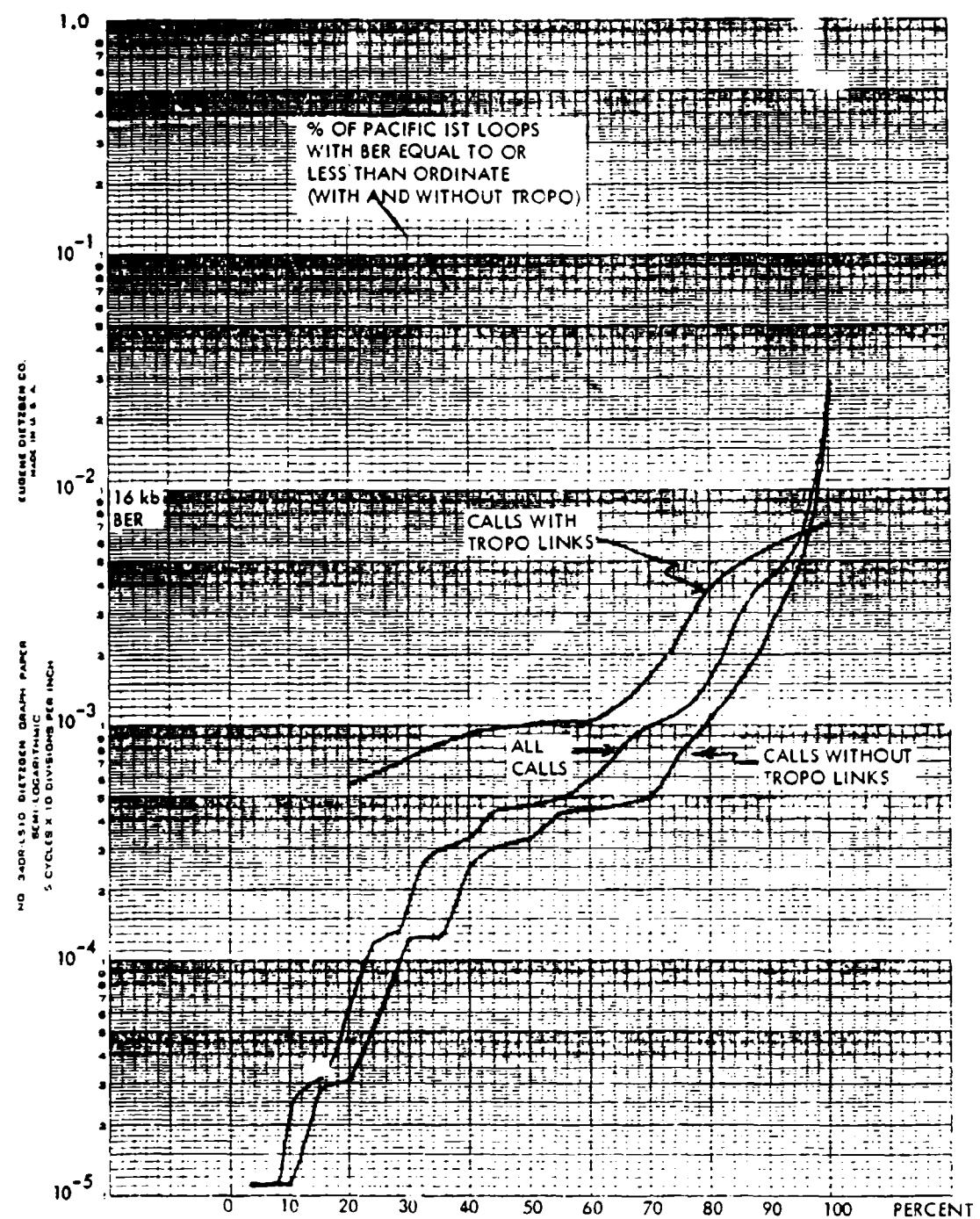


Figure 2.2.1-14

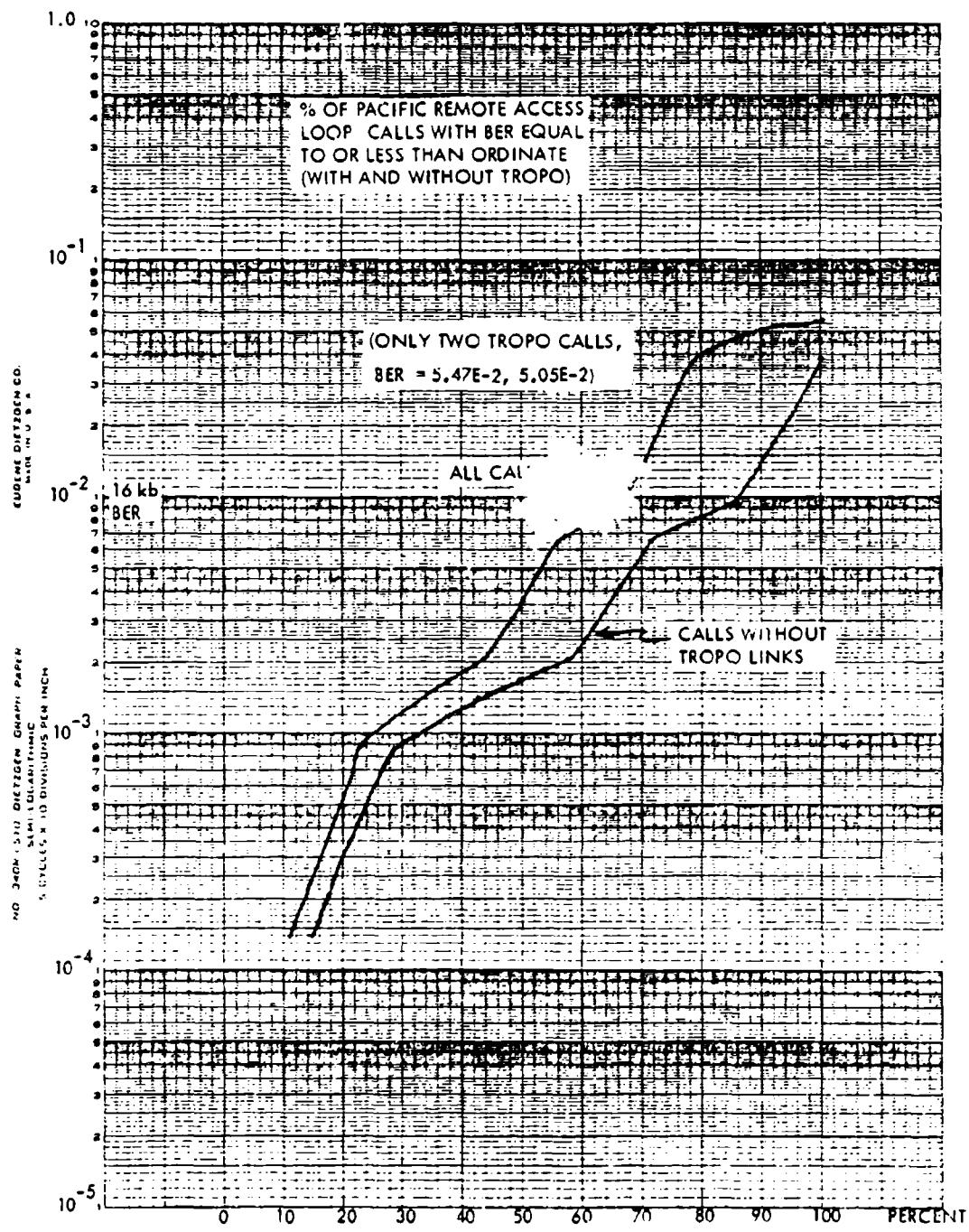


Figure 2.2.1-15

looped calls, five involved tropo and 20 did not. In the case of the remote access calls, two involved tropo and seven did not.

Figure 2.2.1-16 shows the BER performance of the CONUS loop when calls of different levels of distortion are excluded. As can be seen, the performance of the 21 calls with harmonic distortion less than 2 percent is considerably better than that of the 46 calls with harmonic distortion less than 3 percent which in turn is better than the performance for all 78 calls.

In evaluating the data associated with the CONUS testing it is worth noting that data obtained by testing of the CONUS network from a subscriber location can be easily dominated by the characteristics of the particular access line and not that of the IST's in the network. Figure 2.2.1-17 shows the CONUS IST looped data as measured from Melbourne, Florida, and the CONUS IST looped data previously taken from the RADC DICEF facility at Griffiss Air Force Base in Rome, New York. Although the modem design was improved slightly between the times that the two tests were conducted, the principal cause of difference is the higher harmonic distortion levels existing on the RADC calls which were undoubtedly associated with the digital access link from RADC to the AUTOVON switch at Tully, New York.

The conclusion that can be drawn from this is that the IST network is at least as good as it appears from a particular access location but may be better. Conversely, obtaining good performance over the IST network from a particular subscriber location does not guarantee good performance from all subscriber locations. However, if the number of subscriber locations causing problems is sufficiently small, it may be possible to do something about the access lines causing difficulty whereas poor performance on the IST network could likely not be corrected. In particular, D conditioned access lines, which have a specification in maximum distortion should improve bad lines significantly.

Figure 2.2.1-18 shows the performance on the European IST loops when calls which involved only V2 lines and those involving only S3 lines are separated. There

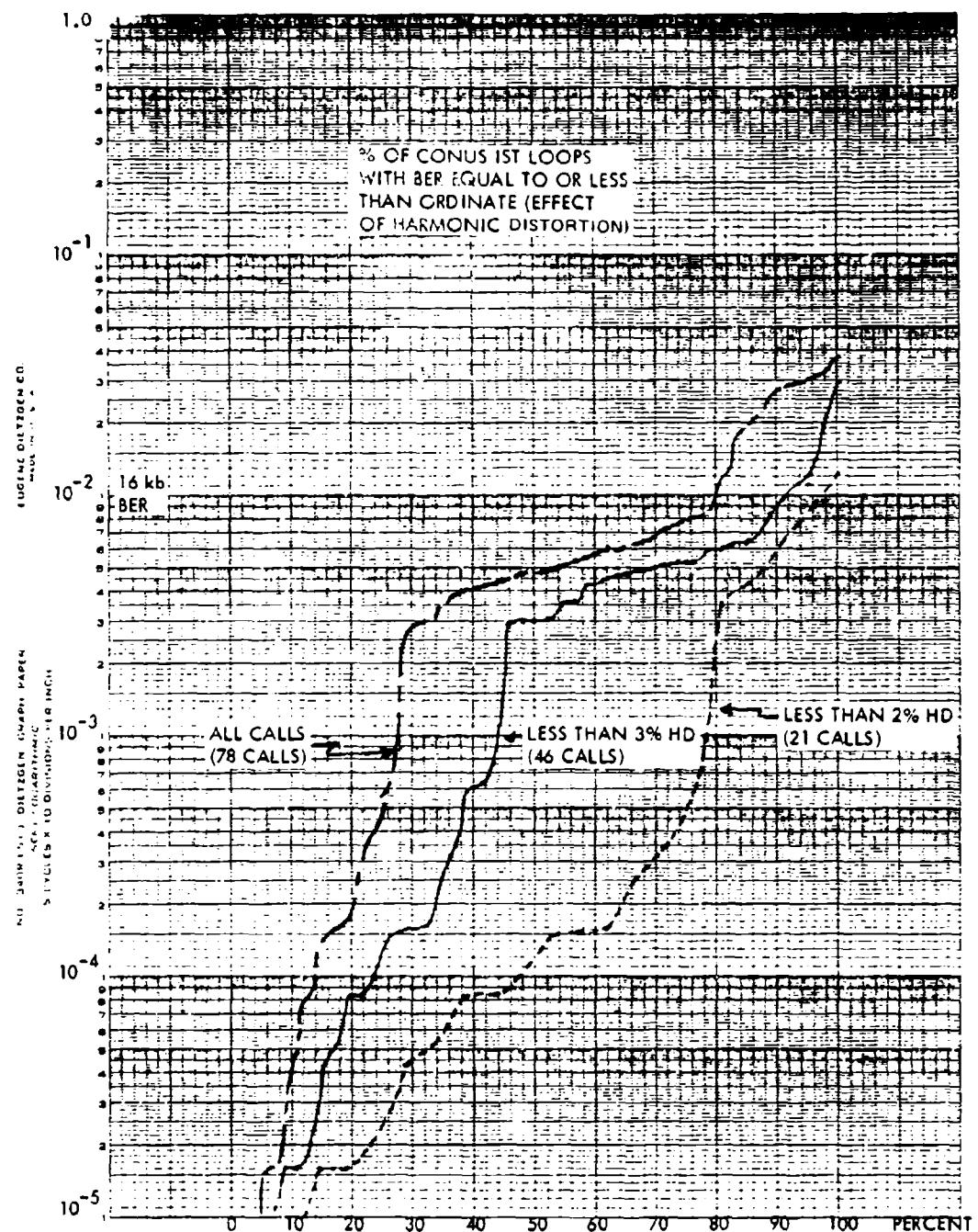


Figure 2.2.1-16

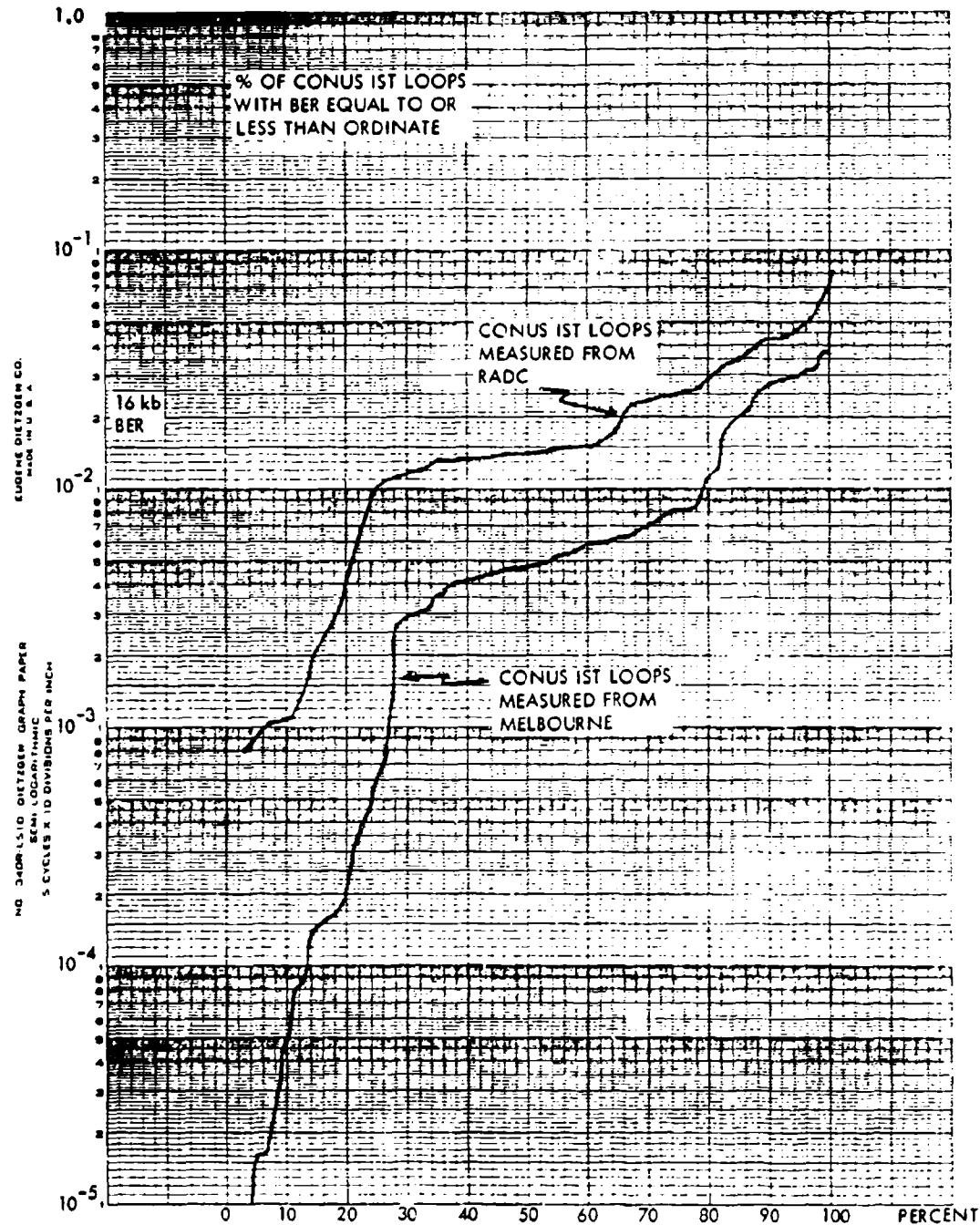


Figure 2.2.1-17

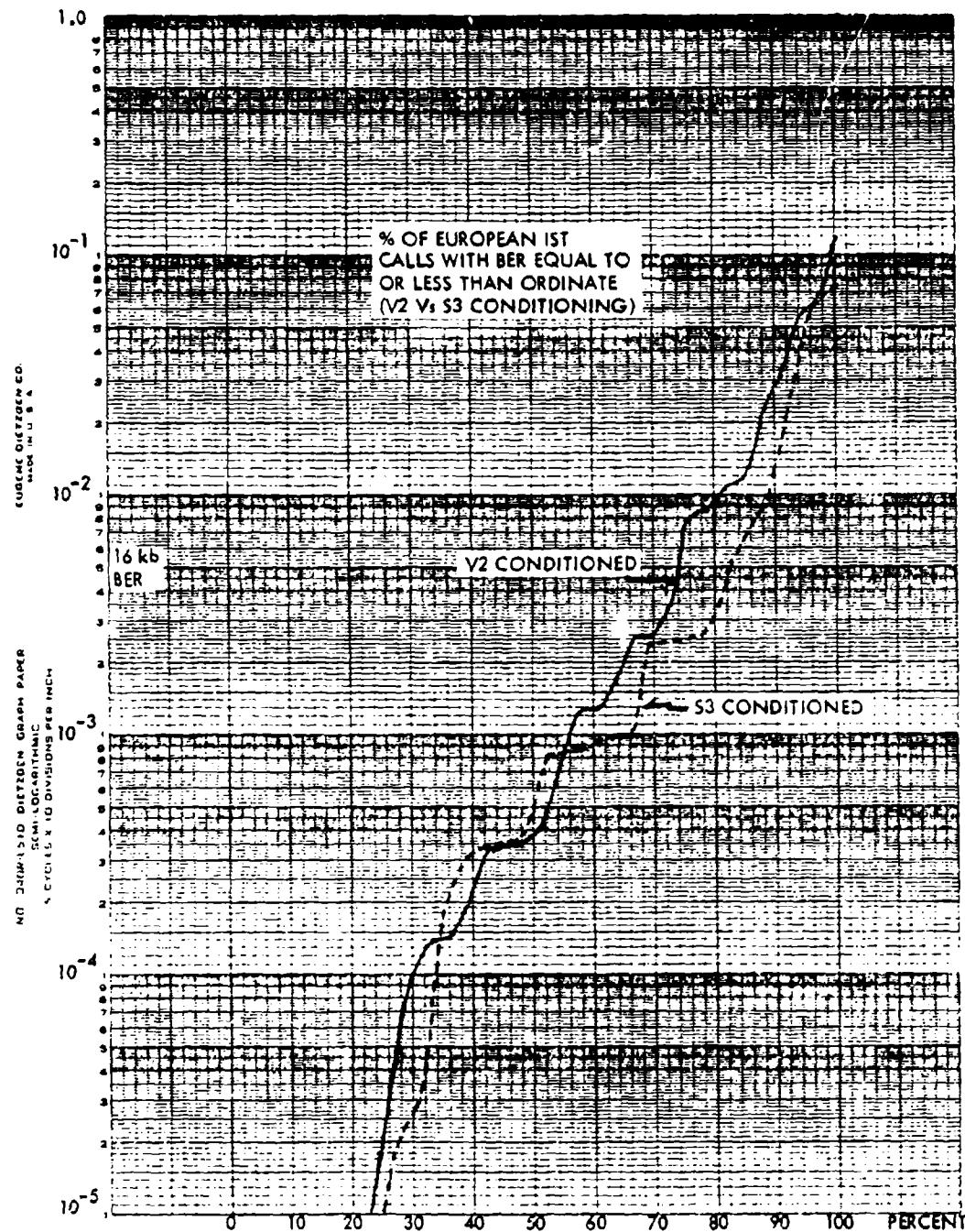


Figure 2.2.1-18

wer. 33 calls involving only V2 conditioned lines and 19 involving only S3 conditioned lines. As can be seen, the performance difference is slight indicating that use of data grade lines would not provide significant performance improvement so far as the IST network is concerned. The European access calls involved too few S3 conditioned lines to make a comparison whereas the Pacific calls involved too few V2 lines to provide a valid comparison. The latter statement is due to the fact that virtually all Pacific IST lines are S3 conditioned. Hence dialing with or without the data grade prefix is unlikely to affect the quality significantly from a statistical point of view.

Figures 2.2.1-19, 2.2.1-20, and 2.2.1-21 present BER curves for the trans-Atlantic, trans-Pacific and the Pacific IST loop subdivided into undersea cable calls and satellite calls. The Pacific IST loops are further subdivided in terms of DSCS and COMSAT calls. In general, it is felt that no significant difference in voice quality exists between these types of calls, although some BER performance was better in some cases, specifically for COMSAT calls and cable calls. The cause of this better performance was not investigated.

Figure 2.2.1-22 shows the block throughput achieved (at 8 kb/s) on all nine categories of lines. As can be noted the block throughput of the European lines was worse than those elsewhere due to the higher percentage of lines with burst phenomenon. Figures 2.2.1-23, 2.2.1-24, and 2.2.1-25 show the percentage of calls which provided equalizer S/N ratio equal to or less than the ordinate. The equalizer S/N ratio is defined as the ratio of the equalizer error signal before equalization (with the weights zero) to that after equalization. The equalizer S/N ratio is not monotonically related to BER since some of the processing algorithms improve BER without affecting equalizer S/N. However, the data has been included since it may be of interest to other modem designers.

To better assess the meaning of the BER curves presented in this section, it is interesting to compare the 16 kb/s results with those previously obtained with other modems in the European network. Figure 2.2.1-26 shows the cumulative BER performance of one-way European IST calls made on the 16 kb/s modem and those made on several varieties of 2.4 kb/s modems and a 4.8 × 1/2 modem in tests conducted in 1971. The 2.4

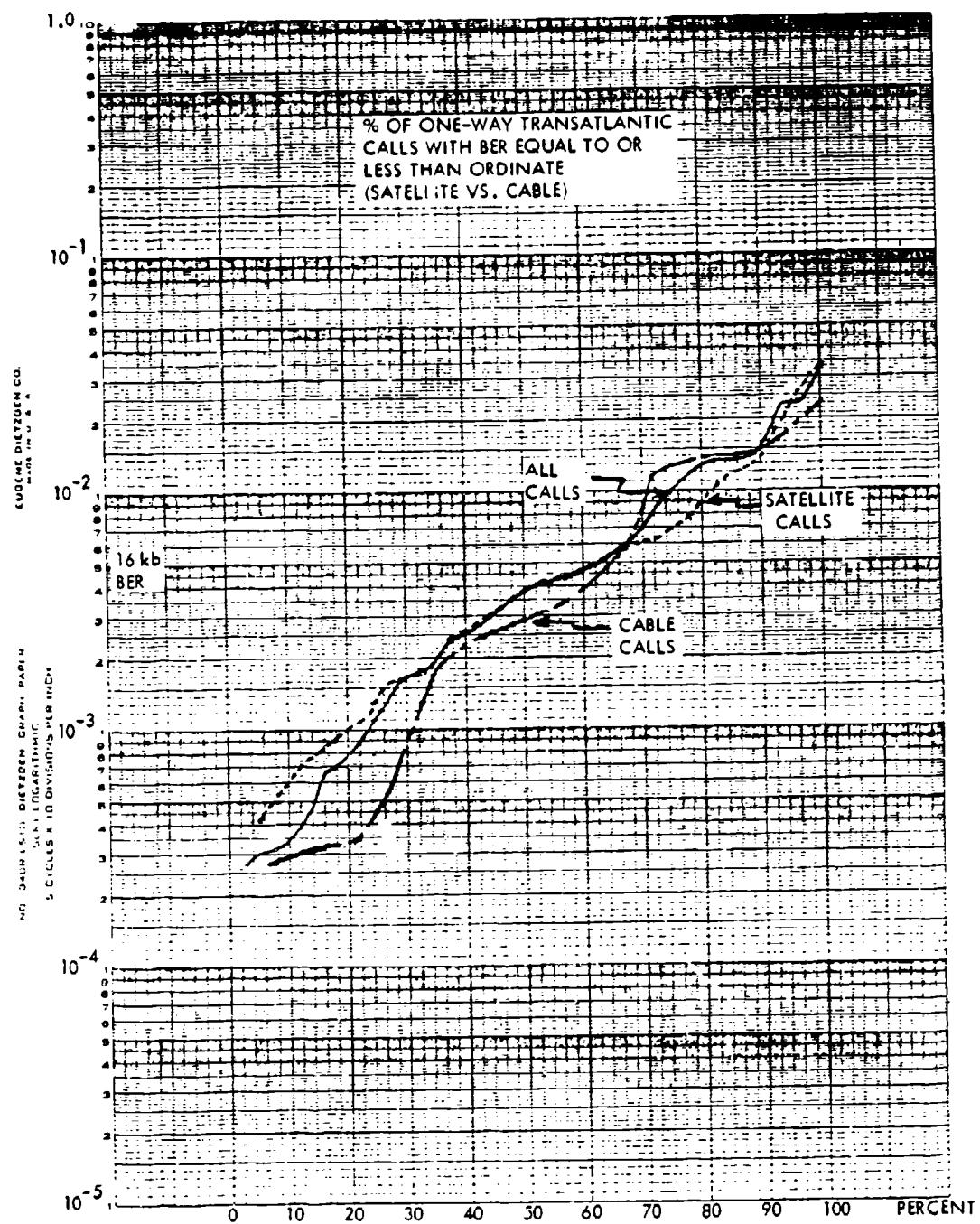


Figure 2.2.1-19

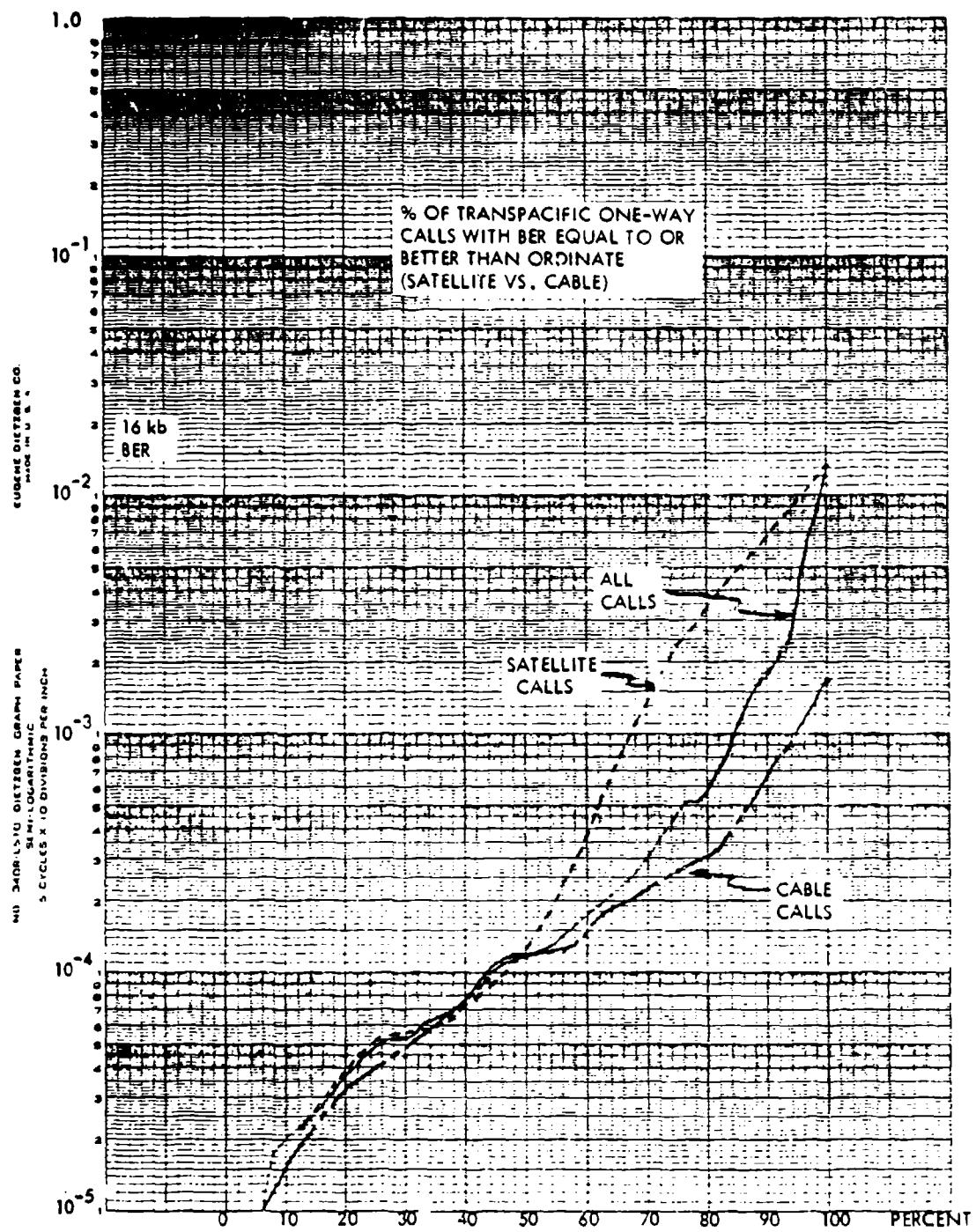


Figure 2.2.1-20

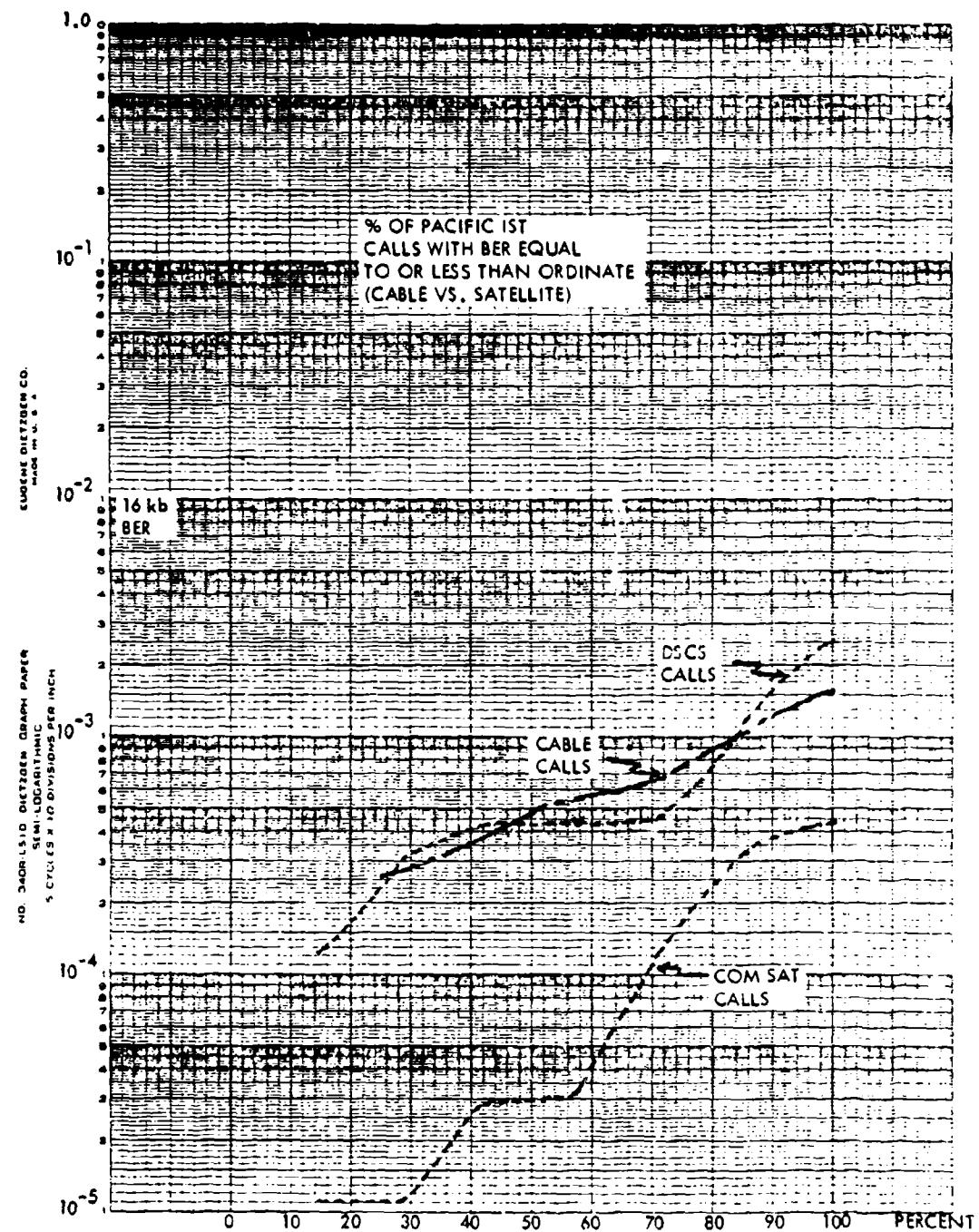


Figure 2.2.1-21

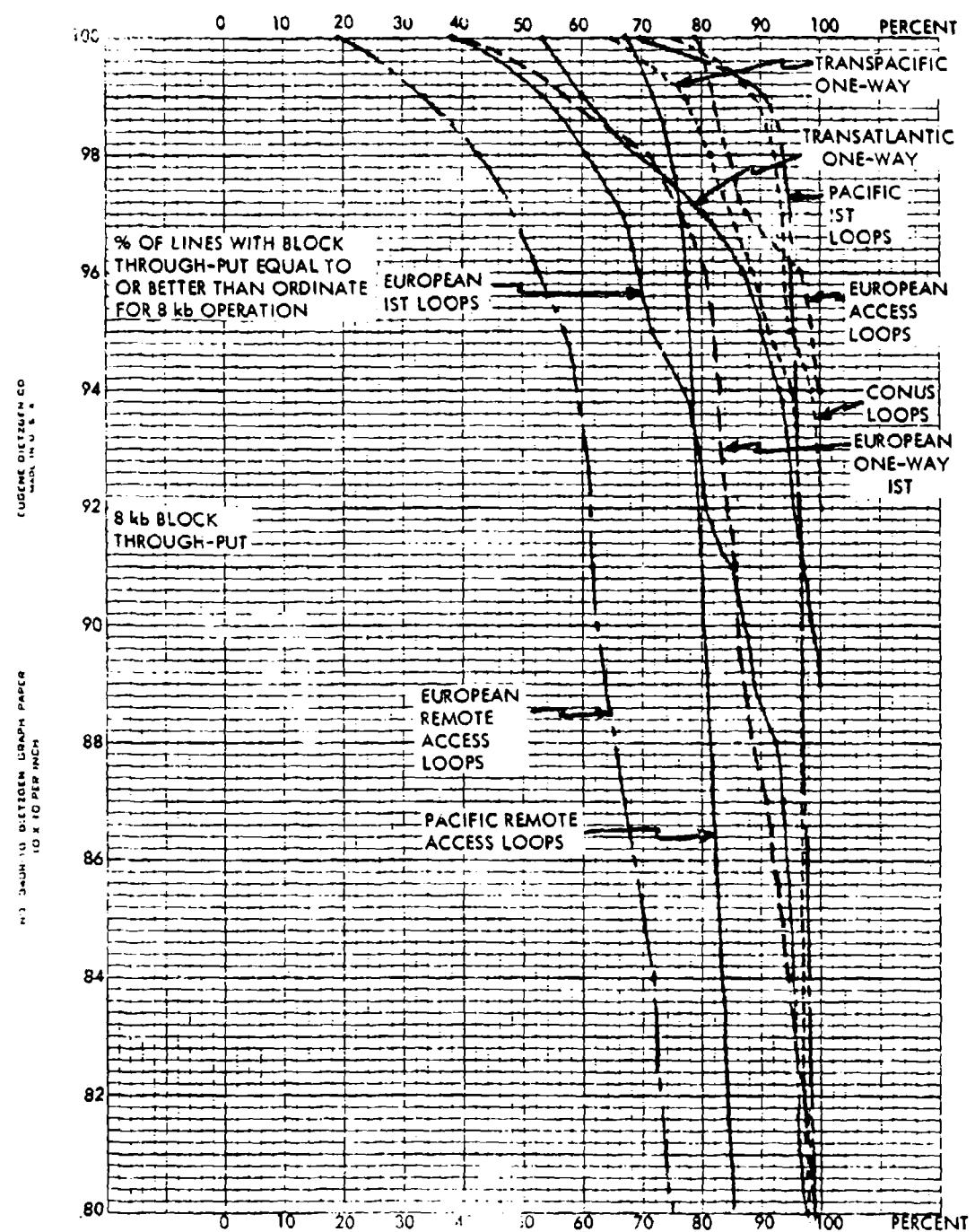


Figure 2.2.1-22

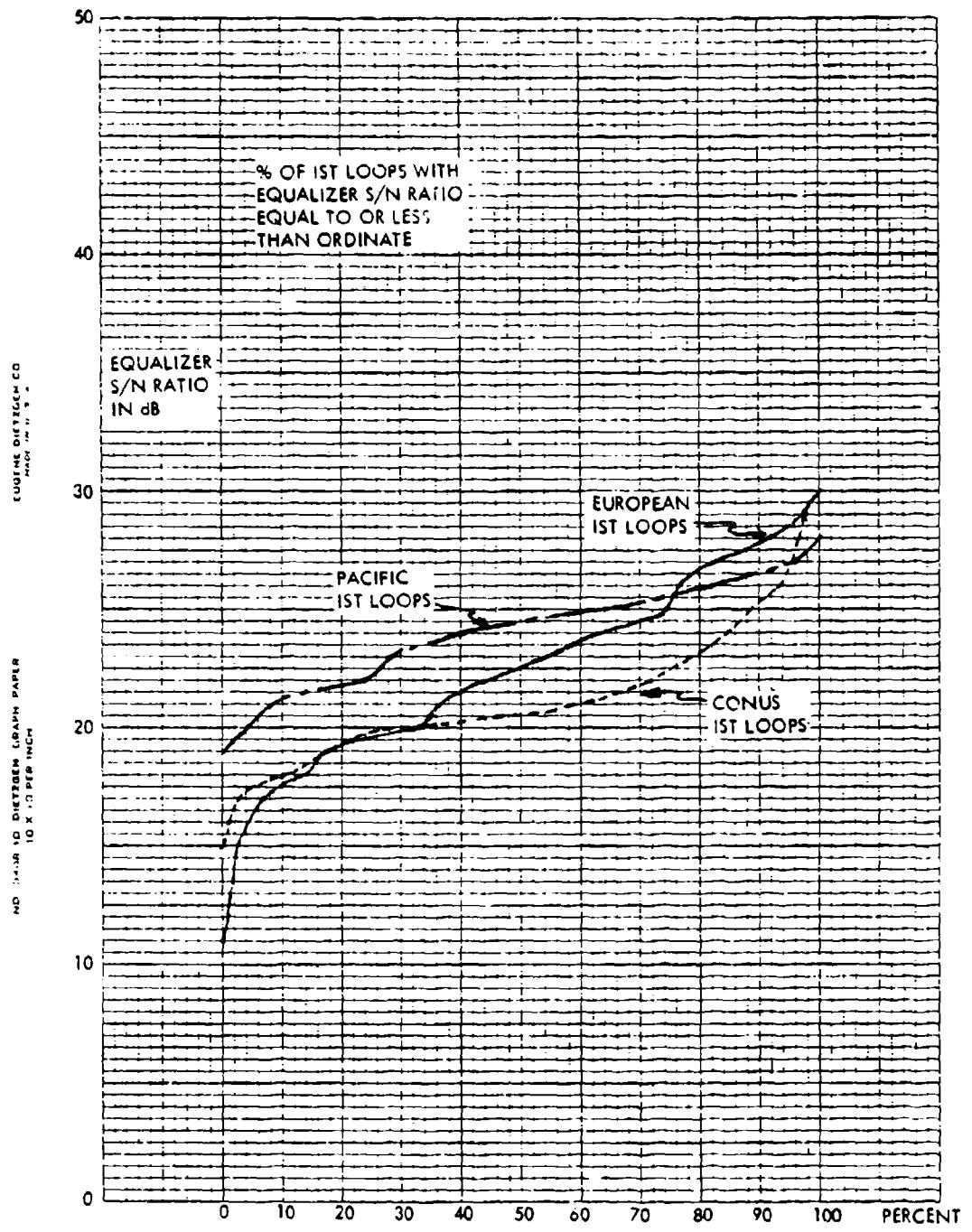


Figure 2.2.1-23

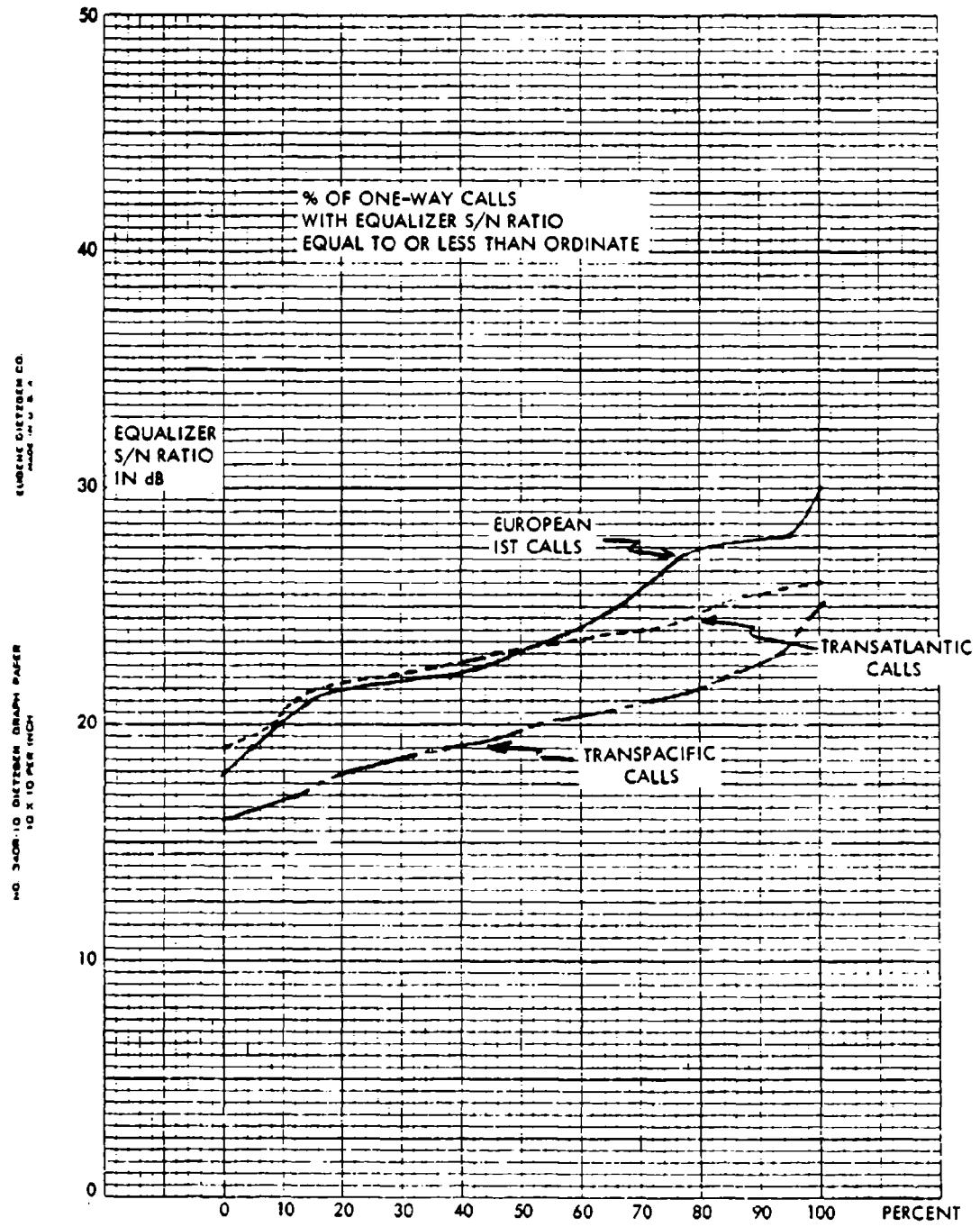


Figure 2.2.1-24

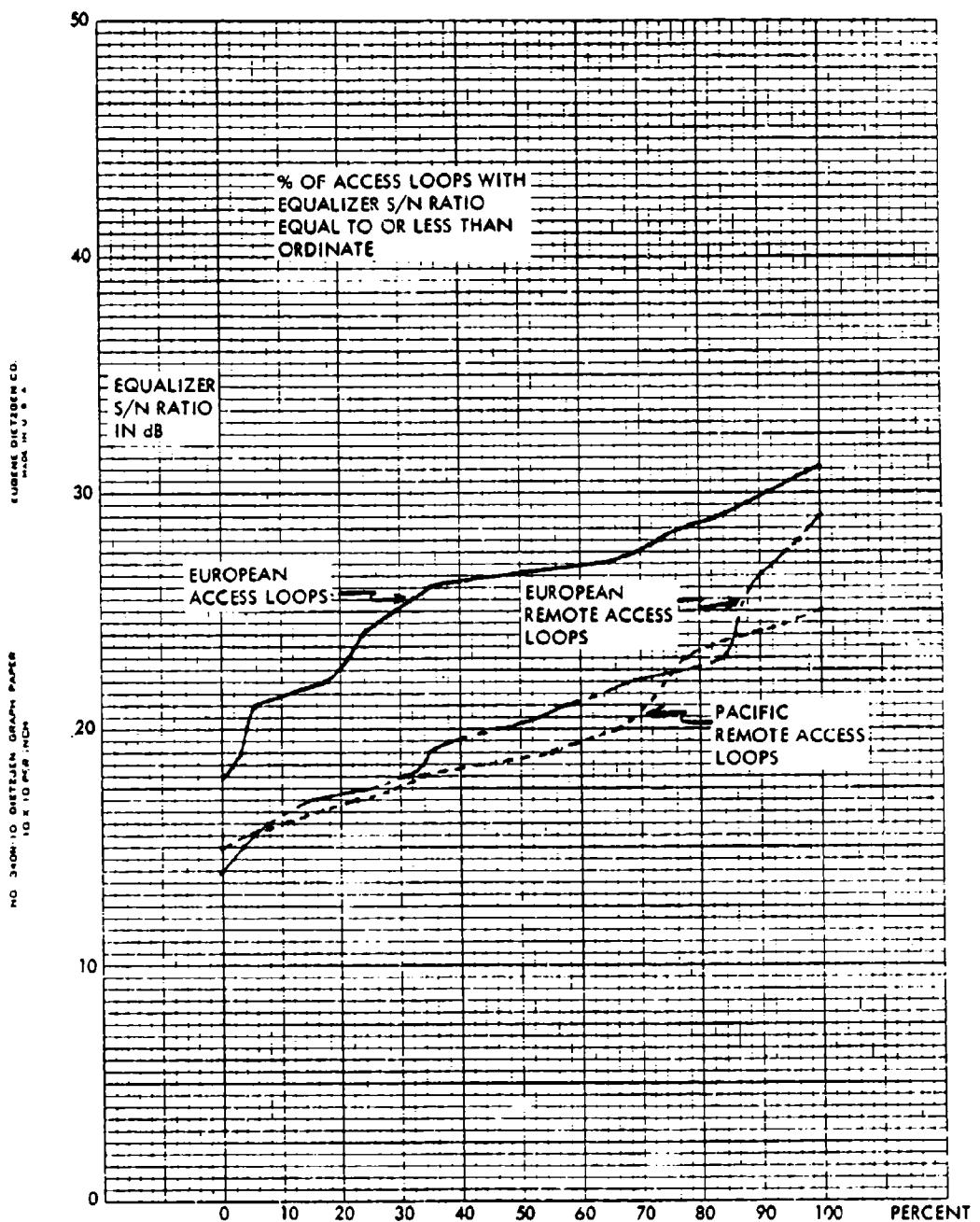


Figure 2.2.1-25

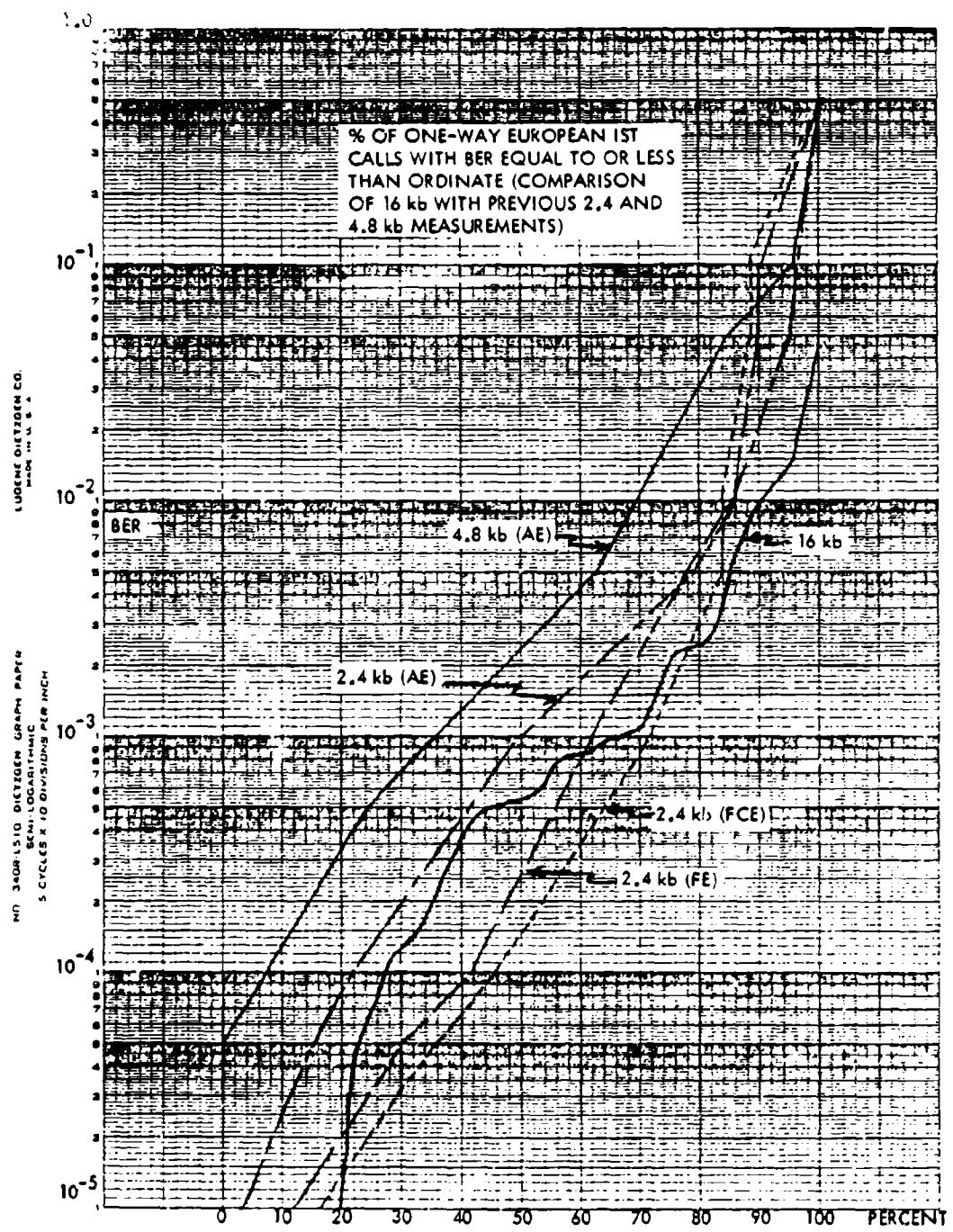


Figure 2.2.1-26

kb/s modem used was the DCS standard modem with several types of equalizers: a fixed equalizer (FE), a fixed compromise equalizer (FCE) and an automatic equalizer (AE). The measurements were made over voice grade circuits (one-way) on IST calls. As can be seen, in the region of error rates of concern to the 16 kb/s modem ( $BER \geq 0.5\%$ ), the 16 kb/s error rates were better than the best of 2.4 kb/s configurations. The data concerning the 1971 tests is taken from RADC-TR-72-70.<sup>2</sup> Although it is recognized that the locations of testing were not the same and that the network has improved since 1971, the comparison is still interesting.

In a number of instances, European calls displayed significant signal level changes that ranged from 1 second in duration to 10 to 20 seconds of duration. The error rate performance following these was observed to be approximately the same as that prior to the disturbance when the disturbance did not occur during the training mode. This feature is felt to be significant in providing satisfactory operation in the environment imposed by the European network.

Two calls were placed from Feldberg which transited digital links associated with the FKV project. Since these are the only digital links in the overseas network, it represents the closest test available to indicate performance when portions of the future network are digitized. Call number 74 from Feldberg to Stuttgart through Vaihingen was looped on a digital link from Stuttgart to Vaihingen in tandem with three microwave links and a tropo link from Feldberg to Vaihingen. The 16 kb/s BER on this call was  $6.53 \times 10^{-3}$ . This call involved two tandem a/d-d/a conversions since the loop back patch at Stuttgart was made at an analog point. Call number 90 from Feldberg to Vaihingen to Stuttgart to Kaiserlautern to Heidelberg transited six tandem digital links with a/d-d/a conversions on each. In addition, it transited the microwave and tropo links to Vaihingen and a government land line from Kaiserlautern to Heidelberg. The looped BER on this call was  $2.53 \times 10^{-3}$ . On both calls, the harmonic distortion was less than 1 percent. Both the error rate data and harmonic distortion numbers appear to be quite encouraging relative to performance through digital links in the future network.

## 2.2.2 Network Coverage

As was discussed in Section 2.1 it was an objective of the tests to "cover" as much of the network as possible so that the results would be as representative as possible of the operation of the modem in the network. On most calls the routing of the calls was traced so that the network coverage could be evaluated.

All AUTOVON switches in Europe have dialed loop-around capability. Thus it is always possible to obtain an IST loop to any of the 10 switches by simply dialing a special number. The switching strategy of the European network is such that a call placed from one switch to another will follow one of, at most, three routes to that switch so far as routing through other switches is concerned. Thus, a call placed from Hillingdon, England to Humosa, Spain may go directly (primary routing); it may go via Langerkopf and Donnersburg in Germany (secondary routing) or it may go via Feldberg, Germany and Mount Vergine, Italy (ternary routing). If all circuits on these three routings are busy with calls of equal or higher precedence a busy signal will occur. The routings associated with these switch to switch calls are referred to as engineered routings.

When placing the IST loop-around calls, all of the engineered routings from each of the three switch locations selected as test sites were obtained. This was achieved by first dialing the loop-around number of the other switches which usually resulted in a primary routing. The remaining secondary and ternary routings were obtained by seizing a trunk to the next switch involved in the routing and dialing the loop-around number from that location. In general, routings that resulted in poor error rate performance were selected for repeat calls when time was available. In addition, routings involved in one-way tests produced repeat calls on the loop-around connections. It should be noted that although there are no more than three routings from one switch to another, as far as the interconnecting switches are concerned, there may be a number of different circuit routings from one switch to another.

The European IST network is shown in Figure A-1 of Appendix A. All of the interswitch traffic transits a network involving 40 microwave links, 11 tropo links, 4 leased Telpak links and 3 diffraction links. During the course of European testing all of these links were utilized for at least one call. There are 41 different routes involved in interswitch circuits. Thirty of the routes were transited during the European testing. The remaining 11 that were not transited contain less than 4 percent of the IST circuits.

Table 2.2.2-1 lists the routings of interswitch circuits for the European AUTOVON network. The first column indicates the two switches that the circuit connects. (Table 2.2.2-2 identifies the locations corresponding to abbreviations given in this report.) The second column indicates the location of baseband patches involved in the connection. The next four columns indicate the number of microwave (M), tropo (T), diffraction (D), and leased Telpak (L) links employed by the circuit. The seventh column is the distance involved in statute miles. The next three columns indicate the number of V2 and S3 conditioned circuits and the total number of circuits on that routing. The last two columns indicate the number of different circuits on that routing involved in the 16 kb testing and the total number of calls using that routing. In all there are 41 different routes involved and 15 transit only microwave links. Twenty-two use at least one tropo link, eight use at least one diffraction link and six use at least one Telpak link. Of the 357 circuits involved, 198 or about 56 percent of them are S3 conditioned. Of the 357 different circuits, 104 were used during the tests representing 29 percent of all the IST voice circuits.

Good coverage of the network involved with access lines is much harder to obtain because of the large number of different access locations, as well as the increased difficulty in achieving loop-around connections to these locations (no usable automatic loop-around capability exists). This difficulty was especially severe in the case of remote access loops since echo suppressors which normally are employed on all such calls had to be disabled. Further many of the access locations involved in the network have only one voice channel and inherently do not have a capability to provide a loop-around.

Table 2.2.2-1. Routings of European IST Circuits

Via	M	T	D	L	Dist	V2	S3	Total	No. Channels	No. Cails
HIN-FEL	MAM	6	2	1	0	446	2	0	2	0
HIN-FEL	-	13	0	0	0	446	5	8	13	6
HIN-DON	FEL	15	0	0	0	490	0	5	5	1
HIN-LKF	-	13	0	0	0	445	6	8	14	3
HIN-MAM	-	5	0	0	0	102	15	19	34	5
HIN-HUM	FEL, LKF	24	4	0	0	1605	1	0	1	0
HIN-HUM	RIA	0	0	0	2	1632	3	1	4	2
HIN-HUM	-	0	0	0	1	932	0	4	4	3
HIN-MRE	HUM	1	4	0	1	1835	0	4	4	3
HIN-MRE	MAM, FEL, MCA	23	2	0	0	1476	3	0	3	10
MAM-FEL	-	1	2	1	0	344	8	5	13	4
MAM-DON	-	3	2	1	0	388	7	5	12	5
LKF-SCH	-	2	0	0	0	96	3	5	8	2
DON-MRE	CLO	0	3	2	0	923	5	6	11	1
DON-MRE	CLO	0	1	2	1	775	0	2	2	0

Table 2.2.2-1. Routings of European IST Circuits (Continued)

	Via	M	I	D	L	Dist	V2	S3	Total	No. Channels	No. Calls
DON-MRE	FEL, MCA	12	2	0	0	1104	2	0	2	0	0
DON-CLO	-	0	1	2	0	485	3	7	10	6	10
DON-CLO	LKF	10	0	0	0	525	2	0	2	2	3
DON-LKF	-	1	0	0	0	23	17	18	35	2	2
DON-PAT	FEL, MRE	12	5	0	0	1620	0	2	2	0	0
DON-PAT	CLO	0	6	2	0	1439	3	1	4	1	1
DON-PAT	LKF, CLO	10	5	0	0	1479	0	1	1	1	1
DON-HUM*	LKF	11	4	0	0	1450	2	5	7	3	5
DCN-HUM*	LKF,CLO	11	4	0	0	1450	1	0	1	0	0
DON-HUM	CLO	1	5	1	0	1410	2	2	4	1	2
DON-SCH*	FEL	4	0	0	0	141	1	1	2	0	0
DON-SCH*	-	4	0	0	0	141	3	5	8	2	2
DON-SCH	LKF	3	0	0	0	119	2	0	2	0	0
DON-FEL	-	2	0	0	0	44	14	16	30	9	12
HUM-MRE	-	1	4	0	0	903	8	10	18	6	8

Table 2.2.2-1. Routings of European IST Circuits (Continued)

	Via	M	T	D	L	Dist	V2	S3	Total	No. Channels	No. Calls
CLO-MRE	-	0	0	0	1	290	3	4	7	6	31
CLO-MRE	-	0	2	0	0	438	1	1	2	0	0
MRE-PAT	-	0	3	0	0	516	7	10	17	6	10
FEL-LKF	-	1	0	0	0	70	14	16	30	6	6
FEL-CLO	-	10	0	0	0	622	2	7	9	6	12
FEL-CLO	SGT	14	0	0	0	884	1	1	2	2	8
FEL-MRE*	-	10	2	0	0	1064	8	2	10	4	7
FEL-MRE*	MCA	10	2	0	0	1064	0	6	6	1	2
FEL-MRE*	CLO	10	2	0	0	1064	1	2	3	0	0
FEL-MRE	LKF, CLO	10	0	0	1	815	0	1	1	0	0
FEL-SCH		2	0	0	0	97	4	8	12	2	3
		256	67	12	7	159	198	357	104	209	
<b>Totals 41</b>											

\*Routings, which are identical except for the location of baseband patch.

Table 2.2.2-2. Locations and Abbreviations

<u>Abbreviation</u>	<u>Location</u>	<u>Abbreviation</u>	<u>Location</u>
ABG	Augsburg, Germany	CHA	Chatham, North Carolina
ANK	Ankara, Turkey	CHE	Chesterfield, Massachusetts
ANU	Adenau, Germany	CHR	Christchurch, England
ANY	Alconbury, England	CHV	Charlottesville, Virginia
APA	Apache Junction, Arizona	CKS	Chicksands, England
ATH	Athens, Greece	CLK	Clark, Phillipines
AVO	Aviano, Italy	CLO	Coltano, Italy
BAH	Bahrain, Bahrain	CMC	C.M.C., Colorado
BAN	Bann, Germany	CRO	Croughton, England
BDK	Badkreuznach, Germany	DAG	Elmiadag, Turkey
BDM	Bad Muender, Germany	DIC	Dye 5, Iceland
BFM	Botleyhill, England	DIY	Diyarbakir, Turkey
BIG	Bitburg, Germany	DON	Donnersburg, Germany
BLN	Berlin, Germany	DOV	Dover-Foxcraft, Maine
BNT	Bentwaters, England	DRA	Dranesville, Virginia
BRE	Brewton, Alabama	DST	Darmstadt, Germany
BRN	Bremerhaven, Germany	ELE	Elevsis, Greece
BRY	Barkway, England	ELL	Ellisville, Florida
BTL	Brieitsol, Germany	EDZ	Edzell, Scotland
BUC	Ft. Buckner, Okinawa	FEL	Feldburg, Germany
CED	Cedar Brook, New Jersey	FIN	Finegayan, Guam

Table 2.2.2-2. Locations and Abbreviations (Continued)

<u>Abbreviation</u>	<u>Location</u>	<u>Abbreviation</u>	<u>Location</u>
FKT	Frankfurt, Germany	JUL	Julian, California
FLO	Flobecq, Belgium	KAD	Kadota, Japan
FRE	Fredericton, New Brunswick	KAR	Karamursel, Turkey
FTD	Ft. Dietrich, Maryland	KEF	Keflavik, Iceland
FUC	Fuchu, Japan	KEN	Kenitra, Morocco
FYL	Flying Dales Moor, Scotland	KLN	Kaiserauern, Germany
GAB	Gablingm, Germany	KRE	Karlsruhe, Germany
GSN	Giessen, Germany	KSL	Koenigstuhl, Germany
HAG	Hagerstown, Maryland	KTS	Karatas, Turkey
HAN	Hahn, Germany	LAH	Lakenheath, England
HDG	Heidelberg, Germany	LAM	Lamar, Colorado
HEL	Helena, Montana	LDL	Landstuhl, Germany
HIN	Hillingdon, England	LDN	London, England
HPG	Hohenpieissenberg, Germany	LDR	Londonderry, North Ireland
HST	Hohenstadt, Germany	LEE	Leesburg, Virginia
HUM	Humosa, Spain	LEG	Leghorn, Italy
HYE	High Wycombe, England	LKF	Landerkopf, Germany
INC	Incirlik, Turkey	LIT	Littleton, Massachusetts
IRK	Iraklion, Crete	LOD	Lodi, California
IZM	Izmir, Turkey	LUA	Lua-Lua-Lei, Hawaii
JAS	Jasper, Alabama	LSY	Lindsey, Georgia

Table 2.2.2-2. Locations and Abbreviations (Continued)

<u>Abbreviation</u>	<u>Location</u>	<u>Abbreviation</u>	<u>Location</u>
LYO	Lyons, Nebraska	MUL	Muhl, Germany
MAG	St. Mawgan, England	NBG	Nuernberg, Germany
MAM	Martlesham Heath, England	NMK	Nea Marri, Greece
MBA	Mount Limbara, Italy	NPS	Naples, Italy
MCA	Mount Corna, Italy	NTG	Netcong, New Jersey
MEL	Melbourne, Florida	OAK	Oakhanger, England
MEM	Memphis Junction, Arkansas	PAT	Mount Pateras, Greece
MHN	Manheim, Germany	PHR	Pearl Harbor, Hawaii
MIL	Mildenhall, England	PMS	Pirmasens, Germany
MIS	Misawa, Japan	POL	Polk City, Florida
MNH	Munich, Germany	POT	Pottstown, Pennsylvania
MOH	Mormond Hill, Scotland	PRU	Pruem, Germany
MOJ	Mojave, California	RAG	Reese-Augsburg, Germany
MOR	Moran, Spain	REG	Reggio, Italy
MOS	Mosely, Virginia	RMN	Rhein Main, Germany
MOU	Mounds, Oklahoma	RPS	Ruppertsweiller, Germany
MPR	Mount Parnis, Greece	RSN	Ramstein, Germany
MRA	Martina, France	RTA	Rota, Spain
MRE	Mount Vergine, Italy	SAH	Sahin Tepesi, Turkey
MSR	Massweiler Cave, Germany	SCH	Schoenfeld, Germany
MTE	Mount Venda, Italy	SEG	Seguin, Texas

Table 2.2.2-2. Locations and Abbreviations (Continued)

<u>Abbreviation</u>	<u>Location</u>	<u>Abbreviation</u>	<u>Location</u>
SEH	Sembach, Germany	TLY	Tully, New York
SEO	Seoul, Korea	TOL	Toledo Junction, Ohio
SGA	Sigon Ella, Italy	TPF	Tempelhof, Germany
SGT	Stuttgart, Germany	TUS	Thurso, Scotland
SHE	Sherbrooke, Quebec	UHD	Upper Heyford, England
SLO	San Luis Obispo, California	VCA	Vicenza, Italy
SMF	Smith Falls, Ontario	VHN	Vaihingen, Germany
SNP	Sinop, Turkey	WAH	Wahiawa, Hawaii
SNV	San Vito Dei Normanni, Italy	WBG	Wurzburg, Germany
SOC	Socorro, New Mexico	WIL	Williamsburg, Kentucky
SPB	Shape, Belgium	WMS	Worms, Germany
SPM	Spangdahlem, Germany	WSE	Wasserkuppe, Germany
STK	Stockton, California	WTH	Wethersfield, England
STN	Stanfield, North Carolina	WTL	Whitehall, England
STV	Stevens Point, Wisconsin	WYO	Wyoming, Minnesota
SWE	Sweetwater, Texas	YAM	Yamanlartropo, Turkey
SWN	Schwetzingen, Germany	YKS	Yokusuka, Japan
SYH	Sidi Yahia, Morocco	YOK	Yokahama, Japan
TAP	Taipei, Taiwan	ZBN	Zweibrucken, Germany
THL	Thule, Greenland	ZUG	Zugspitze, Germany
TJN	Torrejon, Spain		

When possible, access loops were established to the most remote access locations since the network coverage could not be as complete as that achieved with IST loops. Thus, Ankara, Turkey; Iraklion, Crete; Sidi Yahia, Morocco; Berlin, Germany; Londonderry, North Ireland and Dye 5 in Iceland were chosen for testing. In all, tests were conducted to 33 of the 122 different access locations involved in the network. Of the 77 microwave links used to supply access line channels (exclusive of microwave links in the IST network which also are used for access lines), 34 (46 percent) were transited during the access line tests. Of the 22 tropo links involved, 14 (64 percent) were transited. One of the four diffraction links, one of the five government owned land lines, and one of the two VHF/UHF LOS links were accessed. None of the three leased Telpak circuits were involved. In addition, two calls involved digital links in the FKV project even though these did not appear to be in use for access lines at the time of the tests. This was done since future digitization of the network may require operation over similar channels.

The Pacific IST network as discussed in Appendix A is made up almost exclusively of submarine cables, satellite links and tropo links.

The approach to conducting IST loops in the Pacific was similar to that used in Europe since the Pacific switches also have automatic loop-around capability. In this case secondary routing was accomplished by "busying out" rather than seizing trunks. The resulting set of calls utilized all of the basic links involved in the IST network with the exception of one DSCS hop from the Philippines to Okinawa. It is possible, however, that this link was not in operation at the time of the tests. Of the 16 possible circuit routings between switches, 13 (81 percent) were accessed. Two of the three not accessed involved the DSCS link from the Philippines to Okinawa.

Table 2.2.2-3 shows the 16 circuit routes involved with the Pacific IST network and the number of different circuits and calls placed on each during the testing. As can be seen, 24 of the 155 circuits (15 percent) were used.

Table 2.2.2-3. Pacific Interswitch Circuit Routes

	<u>Type of Link</u>	No. of V1 Circuits	No. of S3 Circuits	Total	No. of Circuits	No. of Calls
BUC-FUC	TROPO + MICROWAVE	2	26	28	-	3
BUC-WAH	DSCS	0	9	9	4	6
FUC-WAH	INTELSAT	0	14	14	6	9
FUC-WAH	TRANS PAC CABLE	0	6	6	1	1
FIN-FUC	TRANS PAC CABLE	0	8	8	-	2
FIN-WAH	TRANS PAC CABLE	0	6	6	2	2
FIN-WAH	INTELSAT	0	6	6	1	1
FIN-WAH	DSCS	0	12	12	4	4
CLA-BUC	TROPO + CABLE + MICR	0	14	14	-	2
CLA-WAH	INTELSAT	0	11	11	1	1
CLA-WAH	TRANS PAC CABLE	0	4	4	1	2
CLA-FUC	TROPO - CABLE - TROPO	0	6	6	0	0
CLA-WAH	DSCS	0	10	10	3	4
CLA-FIN	SUB CABLE	0	12	12	1	1
CLA-FUC	DSCS-TROPO	0	3	3	0	0
CLA-BUC	DSCS	<u>0</u>	<u>6</u>	<u>6</u>	<u>0</u>	<u>0</u>
Totals		2	153	155	24	38

Information on the number of access lines involved in the Pacific network was not available. However, the approach used to select access lines in the Pacific was to use those presently associated with secure voice manual switchboards (SECORDS). There are 18 such boards in the Pacific, and nine of the 18 were accessed. Loops to the remaining nine were attempted but problems either in the switchboard or in the verbal communications involved prevented the establishment of the loop-around. Taiwan and Korea were among the locations successfully accessed.

Coverage of the trans-Atlantic calls was as complete as it could be made from Hillingdon, England in that 26 of the 27 circuits from Hillingdon to CONUS were tested. The remaining circuit was down at the time of testing. The 26 circuits tested represents 30 percent of the total trans-Atlantic circuits from CONUS to Europe. The remaining 58 circuits not tested connect Feldberg and Mt. Vergine to the CONUS. At the time of the tests the Atlantic DSCS satellite was inoperative. It is assumed, but not confirmed, that calls normally routed through the DSCS were transmitted through the NATO satellite instead. In addition to the NATO satellite, INTELSAT circuits and four undersea cable circuits are used. In fact, 71 of the 85 trans-Atlantic circuits are routed commercially. The calls from Hillingdon transited all of the undersea cables and satellites used in the trans-Atlantic circuits. Table 2.2.2-4 shows the trans-Atlantic circuits and those accessed during the test. (TAT I, III, IV and V are submarine cables.)

The trans-Pacific tests were less complete than the trans-Atlantic tests partially due to the larger number of circuits from Hawaii to CONUS. Of the 55 circuits from Hawaii to CONUS, 19 (34 percent) of them were involved in the test. These circuits did transit all three undersea cables involved but did not access any of the DSCS channels. The routings not accessed carry 6 of the 55 circuits. In addition to the Hawaii-CONUS circuits, there are 13 circuits which connect CONUS to Japan and the Philippines. These circuits are all satellite circuits using either DSCS or INTELSAT satellites. The performance on these circuits should not differ from those from Hawaii using the same satellite. Table 2.2.2-5 shows all the trans-Pacific circuits, as well as

Table 2.2.2-4. Trans-Atlantic Circuits

<u>From</u>	<u>To</u>	<u>Trunk</u>	<u>V2</u>	<u>S3</u>	<u>TOT</u>	<u>No. of Circuits</u>	<u>No. of Calls</u>	<u>Type of Transmission</u>
HIN	PTN	14VS01	2	0	2	2	2	NATO SAT
HIN	CDB	14VS01	3	0	3	2	3	NATO SAT
HIN	PTN	134801	1	0	1	1	1	NATO SAT
HIN	CDB	134801	1	0	1	1	1	NATO SAT
HIN	PTN	137S02	0	4	4	4	5	INTELSAT
HIN	CDB	137S02	0	5	5	5	5	INTELSAT
HIN	PTN	137Q01	0	3	3	3	3	TAT III
HIN	CDB	137Q01	0	5	5	5	5	TAT III
HIN	PTN	157Q01	0	1	1	1	2	TAT V
HIN	CDB	157Q01	0	1	1	1	2	TAT V
HIN	PTD	237Q02	0	1	1	1	1	TAT I
FEL	PTN	14CS01	6	0	6	0	0	NATO SAT
FEL	CDB	14CS01	4	0	4	0	0	NATO SAT
FEL	PTN	147S03	0	14	14	0	0	INTELSAT
FEL	CDB	147S03	0	12	12	0	0	INTELSAT
FEL	PTN	144801	1	0	1	1	1	NATO SAT
FEL	PTN	140S01	1	0	1	0	0	NATO SAT

Table 2.2.2-4. Trans-Atlantic Circuits (Continued)

<u>From</u>	<u>To</u>	<u>Trunk</u>	<u>V2</u>	<u>S3</u>	<u>TOT</u>	<u>No.</u> <u>Circuits</u>	<u>No.</u> <u>Calls</u>	<u>Type of</u> <u>Transmission</u>
FEL	CDB	140S01	2	0	2	0	0	NATO SAT
FEL	CDB	14D	0	1	1	0	0	COM
FEL	PTN	137Q01	0	1	1	0	0	TAT III
FEL	CDB	137Q01	0	2	2	0	0	TAT III
FEL	PTN	157Q01	0	1	1	0	0	TAT V
FEL	CDB	144801	1	0	1	0	0	NATO SAT
FEL	CDB	157Q01	0	2	2	0	0	TAT V
FEL	PTN	147Q02	0	1	1	1	1	TAT IV
MRE	PTN	157Q01	0	1	1	0	0	TAT V
MRE	CDB	157S01	0	5	5	0	0	TAT V
MRE	CDB	157Q01	<u>0</u>	<u>3</u>	<u>3</u>	<u>0</u>	<u>0</u>	TAT V
			22	63	85	28	32	

**Table 2.2.2-5. Trans-Pacific Circuits**

<u>Location</u>	<u>Trunk</u>	<u>V2</u>	<u>S3</u>	<u>TOT</u>	<u>Circuits</u>	<u>Calls</u>	<u>Type of Transmission</u>
LOD-WAH	187Q03	0	6	6	2	2	Hawaii III Cable
SLO-WAH	187Q03	0	7	7	6	8	Hawaii III Cable
LOD-WAH	187Q01	2	1	3	2	2	Hawaii I Cable
LOD-WAH	187Q02	3	1	4	0	0	Hawaii II Cable
SLO-WAH	187Q02	0	3	3	2	2	Hawaii II Cable
LOD-WAH	18FS01	0	3	3	0	0	DSCS
SLO-WAH	18FS01	0	3	3	0	0	DSCS
LOD-WAH	18DV02	2	10	12	5	6	INTELSAT
SLO-WAH	18DV01	0	12	12	2	2	INTELSAT
LOD-WAH	187S01	0	2	2	0	0	INTELSAT
LOD-WAH	187S04	<u>0</u>	<u>1</u>	<u>1</u>	<u>0</u>	<u>0</u>	INTELSAT
Subtotal		7	49	56	19	22	
LOD-FUC	177S02	0	4	4	0	0	INTELSAT
SLO-FUC	177S02	0	2	2	0	0	INTELSAT
LOD-CLK	177S01	0	3	3	0	0	INTELSAT
SLO-CLK	177S01	0	2	2	0	0	INTELSAT
LOD-CLK	17CS02	0	1	1	0	0	DSCS
LOD-CLK	17CS02	<u>0</u>	<u>1</u>	<u>1</u>	<u>0</u>	<u>0</u>	DSCS
Subtotal		0	13	13	0	0	
Totals		7	62	69	19	22	

those accessed during the tests. The totals are shown for those circuits from Hawaii and those from Japan and the Philippines.

The coverage of CONUS was limited to loop-around calls made to 39 different CONUS AUTOVON switches from Melbourne, Florida. These calls were made from each of two AUTOVON phones which are connected to access lines from the Polk City, Florida switch. The 29 loop-around locations represented all of the loop-arounds that could be located in the CONUS network.

### 2.2.3      One-Way Versus Looped BER

To obtain the network coverage described in the previous section, it was necessary to rely heavily on loop around calls. In order to obtain a rough correlation between the bit error rates of a one-way call and a loop-around call, most of the circuits used for one way calls were also tested in a loop-around configuration immediately following the measurement of the one-way data. This data was taken on European IST, trans-Atlantic and trans-Pacific calls. In all, 17 European IST calls, 32 trans-Atlantic calls and 17 trans-Pacific calls fell in this category. Tables 2.2.3-1, 2.2.3-2, and 2.2.3-3 show the bit error rates obtained in the one-way and looped calls. Figure 2.2.3 is a plot of the one-way versus the looped error rates on calls where the looped error rate is  $10^{-3}$  or higher. The dotted line represents a boundary which all calls equaled or bettered; thus, it should represent a conservative conversion factor between looped and one-way error rates. As can be seen, a looped error rate of approximately 6 percent corresponds to 1 percent one-way error rate while a looped error rate of 8 percent and 11 percent correspond to a one-way error rate of 2 percent and 5 percent respectively. Although no guarantee exists that the ratio of one-way error rates to looped error rate will always be as high as that shown in the curve of Figure 2.2.3, there is strong evidence to indicate that the ratio will often be higher.

**Table 2.2.3-1. European IST One-Way Versus Looped BER**

<u>One-Way Call No.</u>	<u>Looped Call No.</u>	<u>One-Way BER</u>	<u>Looped BER</u>
38	39	7.00E-6	9.91E-4
135	136	0	3.75E-6
40	41	5.91E-3	5.37E-2
44	45	1.11E-4	1.89E-2
42	43	5.91E-4	5.52E-4
46	47	2.48E-3	1.32E-2
50	51	8.05E-4	8.07E-4
52	53	8.74E-4	8.47E-4
76	77	6.25E-6	0
78	79	5.25E-5	3.06E-4
129	130	1.01E-3	2.44E-3
80	81	1.08E-3	2.23E-2
133	134	6.96E-3	1.99E-2
153	154	2.96E-4	1.25E-2
151	152	1.07E-2	6.23E-2
131	132	4.51E-2	1.18E-1
155	156	4.56E-4	5.03E-3

**Table 2.2.3-2. Trans-Atlantic One-Way Versus Looped BER**

<u>One-Way Call No.</u>	<u>Looped Call No.</u>	<u>One-Way BER</u>	<u>Two-Way BER</u>
222	223	6.39E-3	2.04E-1
210	211	4.46E-3	1.92E-1
186	187	4.02E-3	2.37E-1
188	189	2.40E-2	1.87E-1
248	249	4.87E-3	2.44E-1
224	225	2.62E-3	2.66E-1
244	245	1.30E-2	2.44E-1
214	215	2.37E-2	1.51E-1
242	243	1.61E-2	1.02E-1
220	221	1.33E-2	1.34E-1
204	205	3.39E-3	8.99E-2
236	237	1.14E-2	9.34E-2
212	213	1.82E-3	3.71E-2
216	217	1.34E-2	1.29E-1
202	203	2.48E-3	7.49E-2
229	230	2.47E-4	3.67E-2
190	191	3.23E-4	3.22E-2
227	228	3.35E-4	4.13E-2
192	193	7.10E-4	3.82E-2
200	201	2.94E-3	4.08E-2

Table 2.2.3-2. Trans-Atlantic One-Way Versus Looped BER (Continued)

<u>One-Way Call No.</u>	<u>Looped Call No.</u>	<u>One-Way BER</u>	<u>Two-Way BER</u>
194	195	5.22E-3	4.80E-2
232	233	1.06E-2	1.11E-1
240	241	3.41E-2	1.40E-1
246	247	7.75E-3	1.84E-1
208	209	4.05E-3	5.28E-2
231	232	1.65E-3	1.06E-2
234	235	5.92E-3	8.50E-2
206	207	1.12E-3	3.48E-2
238	239	6.54E-4	3.39E-2
198	199	4.24E-4	1.97E-2
216	217	1.34E-2	1.29E-1
196	197	1.73E-3	4.25E-2

Table 2.2.3-3. Trans-Pacific One-Way Versus Looped BER

<u>One-Way Call No.</u>	<u>Looped Call No.</u>	<u>One-Way BER</u>	<u>Looped BER</u>
285	286	1.19E-4	8.76E-3
287	288	2.11E-4	3.02E-2
302	303	1.68E-3	6.29E-2
319	320	8.90E-4	5.74E-2
323	324	2.66E-4	1.05E-2
289	290	1.87E-5	4.47E-3
309	310	6.62E-4	5.39E-3
321	322	9.12E-5	9.38E-3
330	331	5.00E-6	4.97E-3
335	336	3.00E-5	8.81E-3
298	299	1.74E-4	1.45E-2
304	305	5.24E-4	5.04E-3
317	318	5.25E-5	3.60E-3
267	268	6.37E-5	4.38E-3
300	301	2.25E-5	3.78E-3
337	338	5.67E-3	2.01E-2
269	270	1.29E-4	1.53E-2

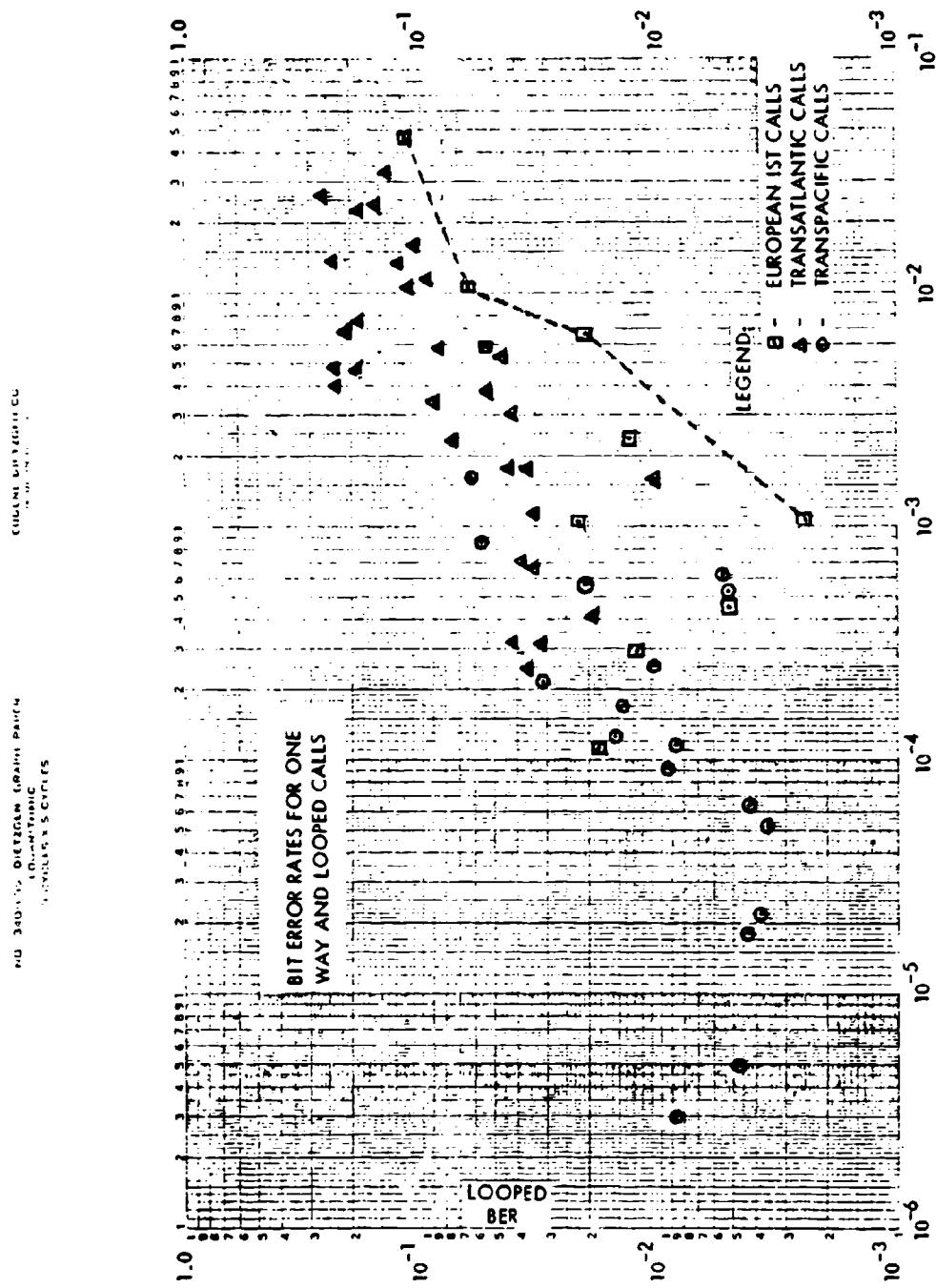


Figure 2.2.3. One-Way BER

It is interesting to note that in virtually all cases all of the line parameters associated with the loop-around calls were degraded over the same parameters associated with one-way calls. The exception to this was frequency offset which was inevitably zero for loop-arounds but generally non-zero for one-way calls. The modem BER, however, is reasonably insensitive to this parameter as long as it is less than 10 Hz. The largest frequency offset observed on a one-way call was 4 Hz. Phase jitter, which might be expected to be less for loop-around calls, usually increased for the loop-around configuration and was rarely less. Perhaps the explanation for this is that the rate of jitter is fast enough and the delay in the channel long enough to make the jitter in the receive and transmit channels of the multiplexer relatively independent.

#### 2.2.4 Composite Network Considerations

The tests were configured to obtain modem performance on each segment of the AUTOVON network rather than from Pacific network locations to Atlantic network locations. As discussed in Paragraph 2.2.5, loop-around calls were attempted from Italy to Hawaii and from Hawaii to England on voice grade lines with unsatisfactory results so far as the 16 kb operation was concerned. A one-way call, however, in these instances might have been quite satisfactory. On one of the Hawaii-England calls a 9.6 kb/s modem was placed on the same loop and was unable to operate even though the same type of modem was in operational use for European traffic.

The 2.4 kb modems used in the AUTOSEVOCOM system employ regenerators at the gateway locations. In the Pacific network the regenerators are not used at Wahiawa if the call originates in Oahu, but is employed otherwise. The CONUS regenerators also change the crypto key. Since the regenerators demodulate the line signal to the digital level only and remodulate at that level, the overall bit error rate associated with a call involving two segments connected by a regenerator will be very close to the sum of the bit error rates in each segment.

If regenerators were supplied at each gateway for the 16 kb/s modem a call from a Pacific location to an Atlantic location might involve five segments, Pacific, Trans-Pacific, CONUS, Trans-Atlantic and European. Thus the bit error rate involved in the total call would be the sum of the five individual bit error rates. If the looped error rates are converted to one-way error rates for the Pacific and CONUS segments it can be concluded that satisfactory error rates would likely be available on most worldwide calls on this basis. In consideration of this process, care must be taken not to add the error rates associated with 80 percent values for the individual segments if it is wished to obtain the error rate for 80 percent of the overall lines. The probability that each of five independent segments would have lines corresponding to the 20 percent worst-case lines is only 0.032 percent.

A legitimate question that was unanswered by the tests is whether satisfactory performance could be obtained without some, or perhaps all, of the regenerators. If key change is required in CONUS, regenerators at the CONUS gateways are a necessity regardless of the operational capability of the modem. Regenerators at the overseas gateways might not be necessary, however, and those in CONUS might not be if the key change were not required. Reduction or elimination of the regenerators could reduce the cost of network deployment of the 16 kb modem.

#### 2.2.5      Special Calls

A number of calls were placed that were not included in the data presented in Paragraph 2.2.1. The trans-Atlantic calls and trans-Pacific calls usually involved both one-way and looped measurements. Only the one-way data was presented in Paragraph 2.2.1 since the looped data appeared to be superfluous except for correlating one-way versus looped. The looped as well as the one-way data is included in the tables of Appendix C.

In addition, 30 calls have been included in Table C-10 of Appendix C which do not fit appropriately into one of the nine categories of calls reported upon in Paragraph 2.2.1. Call 257 in Table C-10 was a loop from Pearl Harbor to Wahiawa which ran error free at 16 kb. Since it was the only access call in the Pacific it did not appear to warrant a category of its own.

Call 1157 was a configuration arranged in Europe where two access lines and an IST were involved. A loop to Vicenza, Italy, was established in Coltano, Italy. An IST connection was established from Coltano to Hillingdon, England via Humosa and Rota in Spain. A second access loop over leased General Post Office (GPO) lines was established to London from Hillingdon. The transmitted signal was then sent from Coltano to Vicenza, and back to Coltano, to Hillingdon, to London, and back to Hillingdon. The 16 kb error rate of this configuration was  $4.25 \times 10^{-3}$ . A loop established from the modem at Hillingdon through this network produced a 16 kb error rate of  $3.80 \times 10^{-2}$ .

Call 333 in Table C-10 was a loop through a short HF hop on Oahu. The modem was located at Pearl Harbor. The transmitted signal was sent via a leased AUTOVON line to Wahiawa and then to Lua Lua Lei which is located about 15 miles over a mountain from Wahiawa. The signal was then sent via an HF link back to Wahiawa and then via AUTOVON back to Pearl Harbor. The 16 kb error rate was  $9.87 \times 10^{-3}$  over this configuration and the 8 kb configuration was error free. Almost no fading was observed on the signals during the tests. Although these results are interesting, caution should be used in extrapolating to long HF links where the effect of the medium might differ.

Calls 183A and 183B listed in the table involved tests from the Royal Signal and Radar Establishment in Christchurch, England to Whitehall and Oakhanger in England over leased 4-wire lines. This demonstration had been set up during the site survey trip. The 16 kb call to Oakhanger ran error free for the 50 second count and that to Whitehall provided a BER of  $5.00 \times 10^{-6}$ . The call to Oakhanger was left on for a 92 minute period with an average 16 kb error rate of  $3.85 \times 10^{-5}$ .

Calls 250, 217, 251, and 241 in Table C-10 were trans-Atlantic loops which indicated that the access line from the CONUS gateway to Ft. Dietrich, Maryland was a major contributor to the error rates in the trans-Atlantic calls. Loop-around calls to Ft. Dietrich from Hillingdon, England had been placed on known trans-Atlantic circuits through the Cedar Brook, N.J. and Pottstown, Pa. CONUS gateway switches. Loop-arounds to Cedar Brook and Pottstown were then placed using the same trans-Atlantic circuits. In the case of the Cedar Brook circuit, an error rate of 12.9 percent was obtained on the loop around to Ft. Dietrich while an error rate of 1.12 percent was achieved when the circuit was looped at Cedar Brook. A number of the line quality parameters were significantly degraded when the loop was extended to Ft. Dietrich. The harmonic distortion was 3.55 percent looped at Ft. Dietrich and 1.15 percent looped at Cedar Brook. In the case of the Pottstown circuit, an error rate of 14.0 percent was obtained looped at Ft. Dietrich while an error rate of 7.69 percent was obtained looped at Pottstown. The harmonic distortion was 7.24 percent looped at Ft. Dietrich and 4.28 percent looped at Pottstown. (This line was selected since it was the worst line to Pottstown from Hillingdon.)

Calls 129A and 129B in Table C-10 were loop-around calls to Pottstown from Feldburg, Germany. Call 129A was placed on a V2 conditioned circuit through the NATO satellite and provided a looped 16 kb error rate of 7.77 percent. The equalizer weights on this call were extremely active indicating that the equalizer was stressed in this configuration. This occurrence was also noted on trans-Atlantic loops from Hillington involving V2 conditioned lines. Call 129B was another loop to Pottstown from Feldberg on an S3 conditioned line. The 16 kb BER was  $2.52 \times 10^{-3}$  for this call.

Call 306 in Table C-10 was a loop-around call from Pearl Harbor to San Luis Obispo, CA which was placed in an attempt to obtain the same type of calibration of the Stockton, CA access lines as obtained for the Ft. Dietrich lines. Unfortunately, the trans-Pacific line obtained in this call was not used in any of the Stockton calls so that a direct comparison could not be made. A looped error rate of  $1.02 \times 10^{-3}$  was obtained, however, which was slightly better than the best looped error rate to Stockton. Calls 307 and 326 provide a slightly better comparison. Call 307 was a loop to the CONUS switch at Mojave, CA through a trans-Pacific circuit to San Luis Obispo on the Hawaii III cable. Call 326 was a loop to Stockton on the same trans-Pacific line. The loop to Mojave provided a 16 kb BER of  $1.93 \times 10^{-3}$  while the loop to Stockton on the same trans-Pacific circuit had a 16 kb BER of  $1.32 \times 10^{-2}$ . Thus it appears likely that the access lines to Stockton also may have adversely affected the BER measurements relative to measurements taken directly at the CONUS gateway switches. The BER values to Stockton, however, were good enough to make this conjecture academic in nature.

Calls 111 and 127 in Table C-10 are European IST loops from Feldberg, Germany which provided identical 16 kb BER values of 2.82 percent. These calls were supposed to have been placed to the Martlesham-Heath loop-around number from Feldberg through the switch at Donnersburg, Germany to provide measurements on the secondary routing from Feldberg to Martlesham-Heath. Patient tracing of the

connections, however, indicated that they were not looped at Martlesham-Heath. The second connection was traced as far as Mt. Vergine, Italy but was not observed leaving there which probably implies that the loop-around on both calls was made at Mt. Vergine through Donnersburg for some reason. Since the routing was felt to be somewhat in doubt due to these events these calls were relegated to Table C-10 rather than Table C-1 which contains the normal IST looped calls. The next day a legitimate loop to Martlesham Heath from Feldberg through Donnersburg was established which yielded a 16 kb BER of  $7.72 \times 10^{-4}$ . It is interesting to note that the secondary routing call from Feldberg to Mount Vergine does go through the Donnersburg switch and an error rate of 2.20 percent was obtained on that call.

Call 49 in Table C-10 was from Hillingdon to Coltano which provided a BER of  $1.50 \times 10^{-5}$  but the circuit was lost before any routing information was obtained.

Calls 11, 15, and 16 were placed from Coltano, Italy to evaluate the effect of establishing loop-around connections at access locations at a two-wire rather than four-wire point. The first of these to Leghorn was made on an automatic dialed basis. (This service is being established for several access locations from Coltano.) Although the 16 kb BER was  $7.50 \times 10^{-6}$  with the two wire loops, the four-wire loops at Leghorn had been error free. Calls 15 and 16 were two-wire loops established by the PBX operator in Ankara, Turkey. The 16 kb BER values for these calls were  $2.85 \times 10^{-1}$  and  $3.65 \times 10^{-2}$ . Four-wire loops to Ankara from Coltano provided BER values of  $5.36 \times 10^{-3}$  and  $1.26 \times 10^{-2}$ . Further, the equalizer weight patterns observed on the two-wire loops indicated considerable reflections on the line which were likely caused by mismatch at the looped connection point. These measurements indicated that even though two-wire loops might be somewhat easier to establish, four-wire loops should be used to obtain representative data.

Calls 334 and 69A were loops established from Pearl Harbor, Hawaii to Hillingdon, England and from Coltano, Italy to Wahiawa, Hawaii

respectively. The 16 kb BER values of these calls was 12.5 percent and 18.1 percent, which would be totally unacceptable from a user standpoint. Both calls were placed on voice grade circuits since data grade calls automatically inserted regenerators which could not operate with the 16 kb modem. Whether one way calls and/or the use of data grade lines would have provided acceptable error rates is a matter of conjecture. The calls were placed to obtain some rough feeling for worldwide performance since the overall test plan was not designed for direct measurement of this mode of operation. Had the looped values been better, the question in this direction would have been answered. However, the values obtained were such that no conclusions can be drawn. It is interesting to note that on the loop to England from Hawaii the 8 kb BER value was  $4.11 \times 10^{-4}$  while an operational 9.6 kb modem was unable to operate over the same loop. The 8 kb BER value on the loop from Italy to Hawaii was  $1.34 \times 10^{-2}$ .

The last seven calls in Table C-10 were calls in which the lines appeared to be degraded by in-band filters of some sort. The most common of these was a notch at 2.6 kHz which indicated the insertion of a single frequency (SF) filter used to handle the off hook signal. In addition, several lines indicated notches at 1600 Hz which apparently come from filters associated with a different signaling aspect. Some thought was given, in the course of preparing this report, as to whether these calls should be counted in the statistics given in Paragraph 2.2.1. Since the number of calls involved is small and the errors were not necessarily catastrophic, the effect on the statistics would not be very dramatic. However, it was reasoned that most, if not all, of these cases were either transient in nature (that is a line so bad that it would be complained about and fixed) or was due to the attempt to operate data signals over the voice grade network when no alignment of that network for this purpose had been done. Specifically the detection levels of the circuitry which inserts the SF filters was likely to be quite satisfactory to prevent their insertion due to normal voice traffic but not satisfactory for a data signal which has different spectral properties. They can be adjusted, as they undoubtedly are, for data grade lines, to also be satisfactory for data signals

but there has been no requirement to do so. If a decision were made that allowed data signals on voice grade lines on an operational basis the readjustments would be required as a matter of course and the problem would disappear. Hence, these calls were not considered representative of the network and were relegated to Table C-10.

For the purposes of completeness, it will be noted that 13 data sheets used during the test program contained some recorded data that is not included in the report. These sheets contained data for calls that involved setups that were discovered to be faulty in some manner such as; abnormal levels due to a mistake in patch locations, use of bad equipment to reach the transmitter or modem location from the switchboard, etc. To assure a fair presentation when the data was reduced, all data sheets containing any data were preserved during the tests and these sheets occupy a number in the chronological listing of the call numbers.

## 2.3

Line Test Results

Curves are presented in this section showing the percentage of channels providing specified line characteristics with values equal to or less than the ordinate or abscissa of the curve in question. The data is subdivided into the nine categories of calls presented in Paragraph 2.2.1 for the modem performance data. The three curves representing performance on the Pacific, European and CONUS IST loops are presented together. The one-way calls on the European, trans-Atlantic and trans-Pacific calls are also presented together as are the three categories of access line loops (European access loops, European remote access loops and Pacific remote access loops). In Appendix C the measured line characteristics for each call are listed along with the error rate performance.

Before presenting the data, several general comments are appropriate. All of the line data was obtained using a model 520 B Halcyon line tester. Details of the test procedure are given in Paragraph 2.4. The phase detector used in the Halcyon to provide measurements of peak-to-peak phase jitter does not respond to very low frequency jitter. In several instances large amounts of very low frequency phase jitter was observed on the tones appearing on the oscilloscope but the Halcyon indicated low phase jitter readings. Since the modem performance is relatively insensitive to low frequency phase jitter, this feature of the Halcyon is not too important. It can, however, account for some difference between values of phase jitter recorded on this test program and those which have been recorded in past programs where this parameter was measured with different equipment.

Differences between the data reported here and that previously gathered might also have occurred when tropo links were involved. In the tests reported herein, the line characteristic values reported were "average values" when a deep fade was not present. When deep fades occurred, all of the parameters varied widely. In some channels the variance of the values without deep fades was significant. If past data

values were obtained by reading "peak values" from recorder charts, they might be expected to vary significantly from those obtained on this test.

It should be noted that ordinary line test equipment is not set up to measure the pertinent parameters associated with the fading characteristics when tropo channels are present. Since these characteristics represented one of the two significant error contributors to the 16 kb modem, it would appear prudent to assure that future network models attempt to simulate these effects. No mention of these characteristics was found prior to this test in reports of past measurements.

Oscilloscope photographs of the envelope of a 1 kHz sinewave were made on many of the tropo transmissions and are included in Appendix D. Table 2.3-1 lists the peak-to-peak amplitude variation observed in these pictures as a percent of the peak-to-peak signal. The "period" shown in the table indicates roughly the time between successive fades and does not imply that fading is necessarily periodic. In many cases the period of fade was not clear from the photographs and is indicated with a dash in the table.

A third cause of difference in the line characteristics measured in this test and those measured previously is the difference in routing between test programs. In the present program much of the data is loop-around data, whereas most of the past data is one-way. Even in the case of one-way data, the routings involved in this test do not correspond exactly to those present in past tests. In the program which evaluated the Vodat modem, all of the IST calls were conducted from Mt. Pateras to Hillingdon which involved tropo on all calls.

Finally it is probable that the European network has been improved since the last tests were conducted. Several operational personnel who had been with the network for some time felt that the present quality control programs for assuring line quality have significantly improved the lines.

There were 14 different types of line measurements made, not counting those associated with the amplitude response and group delay of the channels. Figures

Table 2.3-1. Amplitude Variation

<u>Call No.</u>	<u>P-P Amplitude Variation - %</u>	<u>Period of Amplitude</u>
30	6	30 ms
31	6	20 ms
35	28	1.1 sec
37	4	0.45 sec
40	7	1.3 sec
41	9	0.8 sec
41-2	9	—
54	7	—
61	4	0.5 sec
64	6	0.6 sec
66	5	0.5 sec
71	17	2 sec
82	8	40 ms
86-1	7	1.2 sec
86-2	20	>4 sec
92	12	—
107	9	—
111	43	—
126	8	50 ms
127	31	—
129B	—	—

Table 2.3-1. Amplitude Variation (Continued)

<u>Call No.</u>	<u>P-P Amplitude Variation - %</u>	<u>Period of Amplitude</u>
144	20	6 sec
151	11	—
152	22	—
154	12	—
157	6	—
158	11	—
162	9	—
168	9	—
181	9	2 ms
240	21	Distortion
276	9	0.1 sec
292	3	1.5 sec
297	28	Distortion
313	6	20 ms

2.3-1, 2.3-2 and 2.3-3 present the percent of channels with line loss equal to or less than that shown in the abscissa. The line loss was measured both with the modem signal and with a 1 kHz tone and both types of loss are shown. The reason for including both types of measurement is that the modem performance is concerned principally in the loss associated with the modem signal while the standard techniques for determining this parameter is to use a 1 kHz tone. The two differ significantly for some channels due to variations in the amplitude response of the channel. In this report a positive line loss indicates that the received signal is smaller than the transmitted signal. Since all of the calls were essentially from one technical control facility to another, the nominal line loss should be zero.

Figures 2.3-4, 2.3-5, and 2.3-6 present receive S/N ratio data also measured separately with the data signal and with a 1 kHz tone. An additional difference between these two measurements is that in the case of the data S/N ratio, the quiet line noise was used in the ratio. In the case of the 1 kHz S/N ratio the noise level is obtained by notching the 1 kHz tone at the receive site. In this case harmonic distortion contributes to the degradation of the S/N ratio. This accounts for the noticeable difference of the two parameters in the CONUS IST loops. In both cases the noise was measured through a C-message weighted filter provided in the Halcyon.

Figures 2.3-7, 2.3-8, and 2.3-9 present data concerning peak-to-peak phase jitter. Some of the reasons that this data indicates less phase jitter for the E-6 network than that previously reported have already been given. In addition to this measurement the spectral characteristics of the phase jitter was obtained on many lines and is presented in Appendix D. The original test plan called for making spectral photographs of phase jitter whenever the peak-to-peak value exceeded  $15^{\circ}$ . However, so few channels had jitter this large that a number of spectral photographs were obtained for many channels with less than  $15^{\circ}$  jitter when periodic jitter appeared to be present. Table 2.3-2 shows the size of the periodic components on these photographs. Perhaps the most significant aspect of the phase jitter measurements is the fact that most channels

MA 11410 DICKSON GRAPH PAPER  
10 x 10 per inch

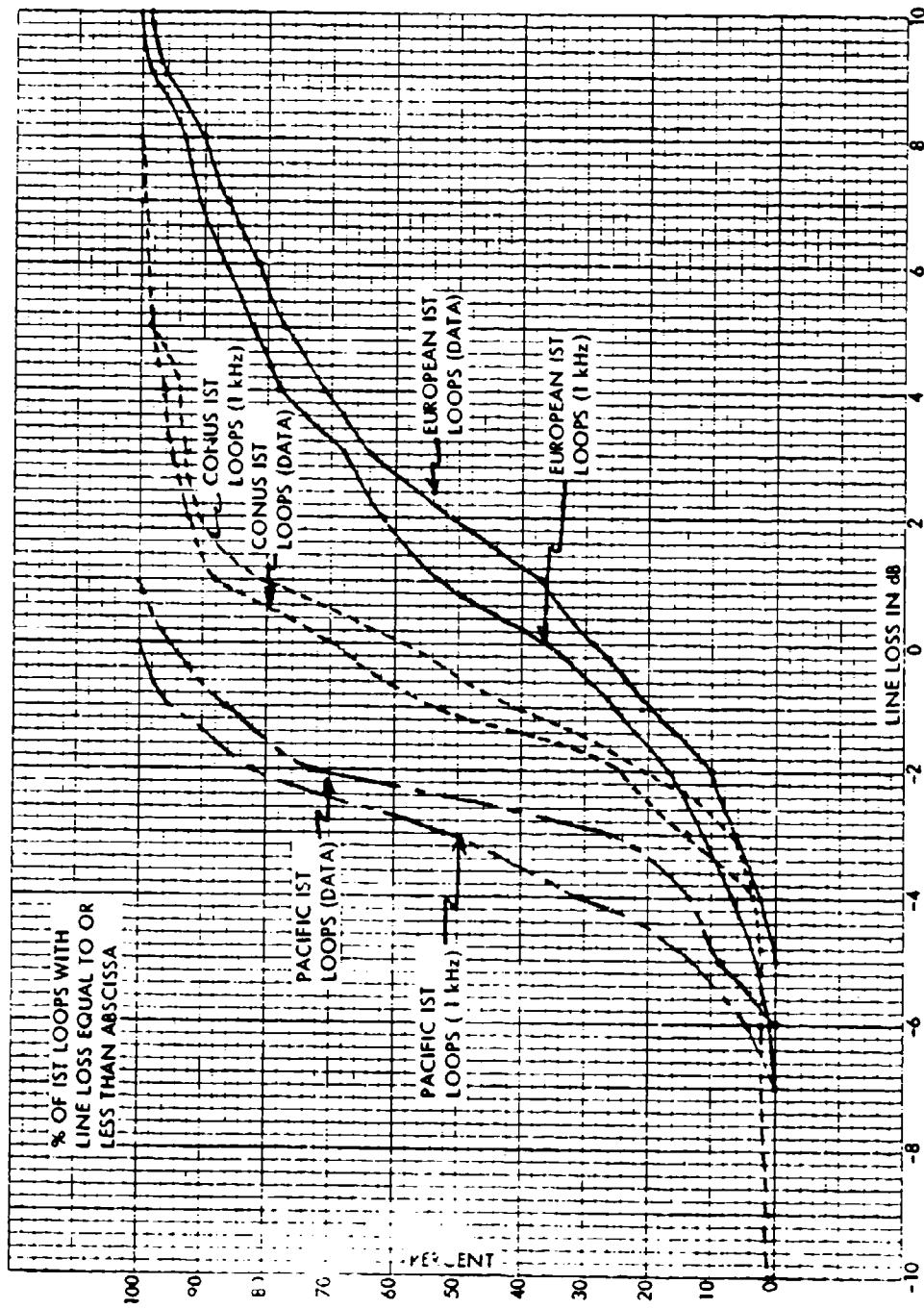


Figure 2.3-1

NO. 347-10 DIXIEGRAPH GRAPH PAPER  
10 X 10 PER INCH

EUROPE DIXIEGRAPH CO.

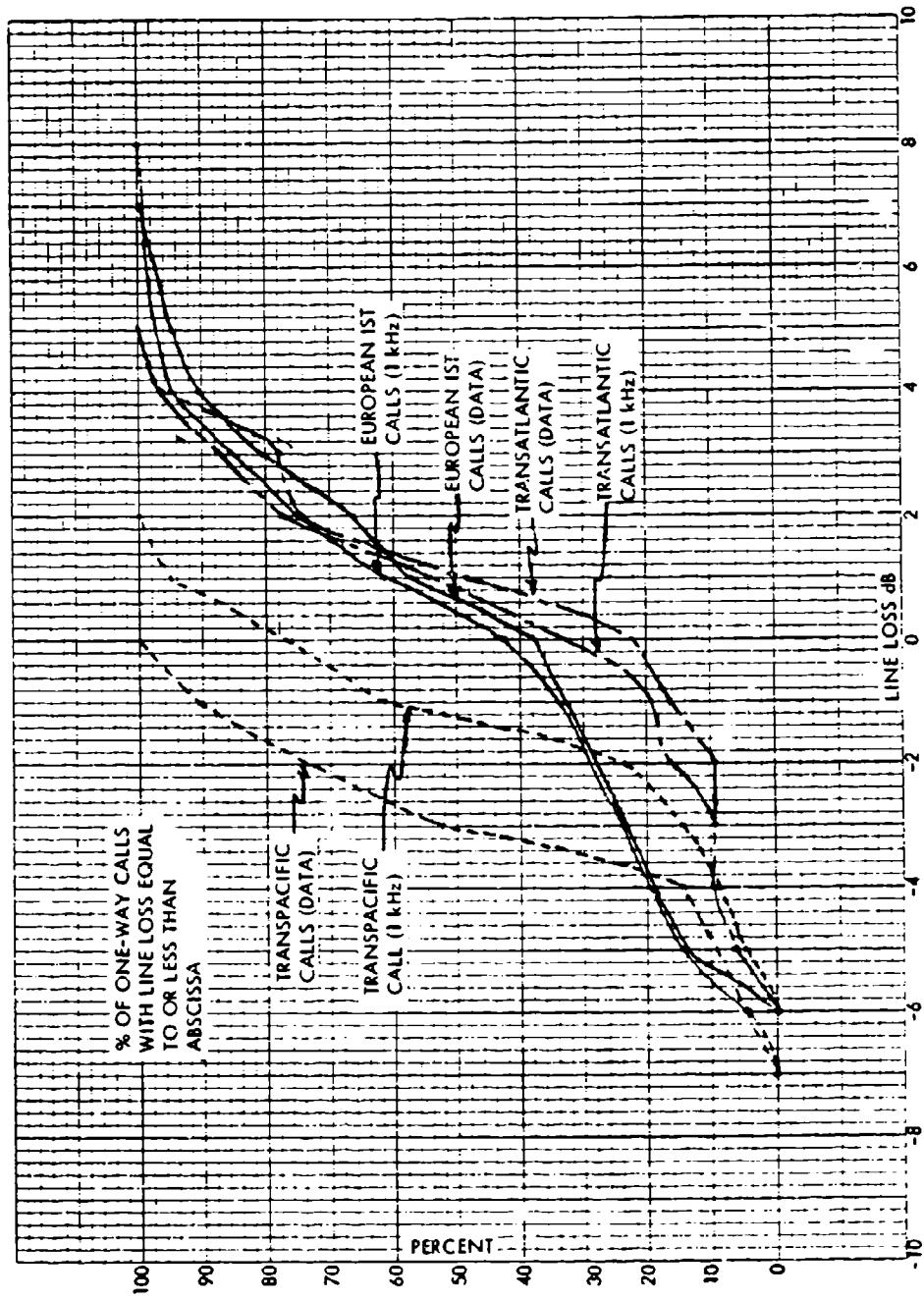


Figure 2.3-2

NO. 34010 DIAZINE GRAPH PAPER  
MADE IN U.S.A.

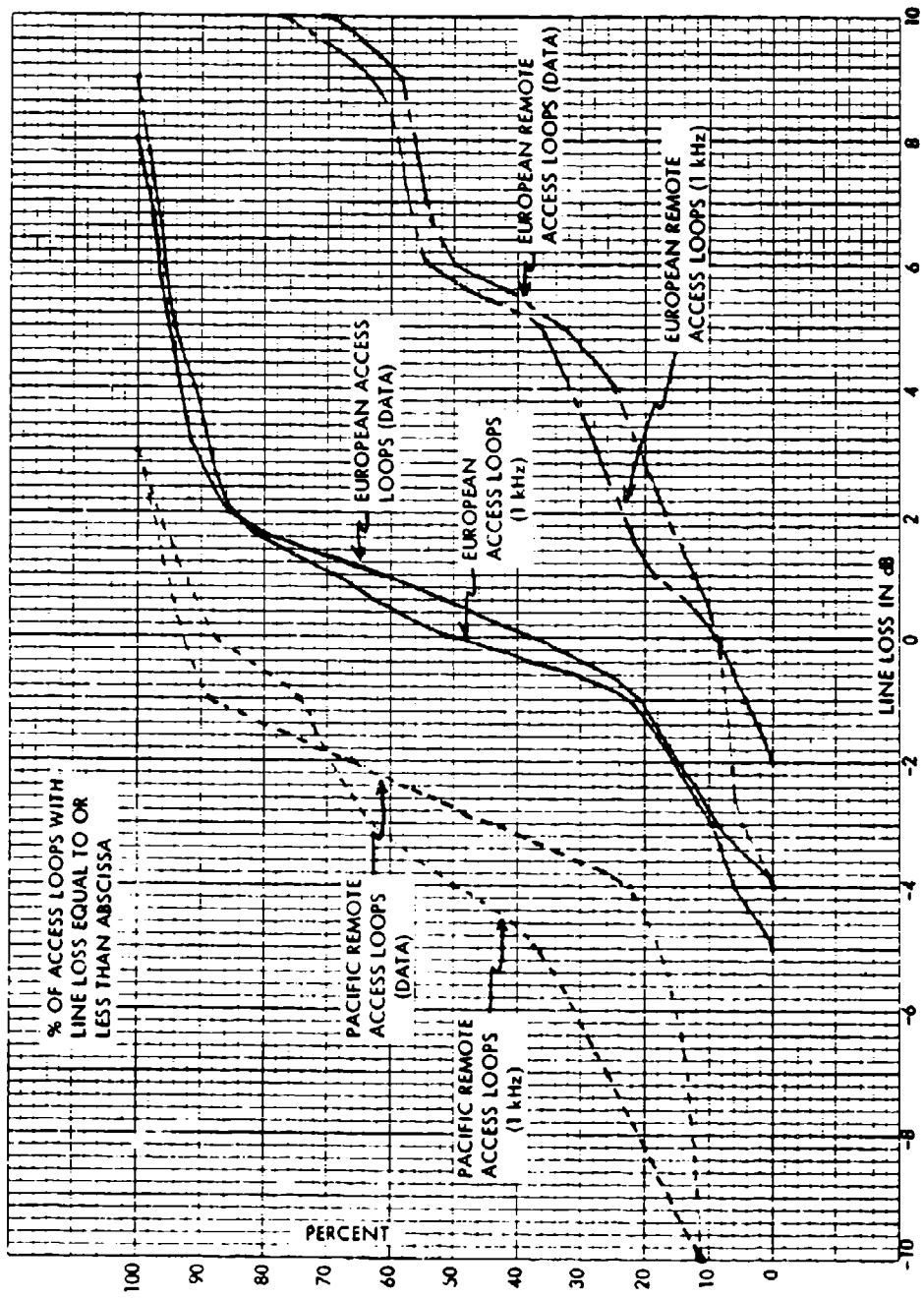


Figure 2.3-3

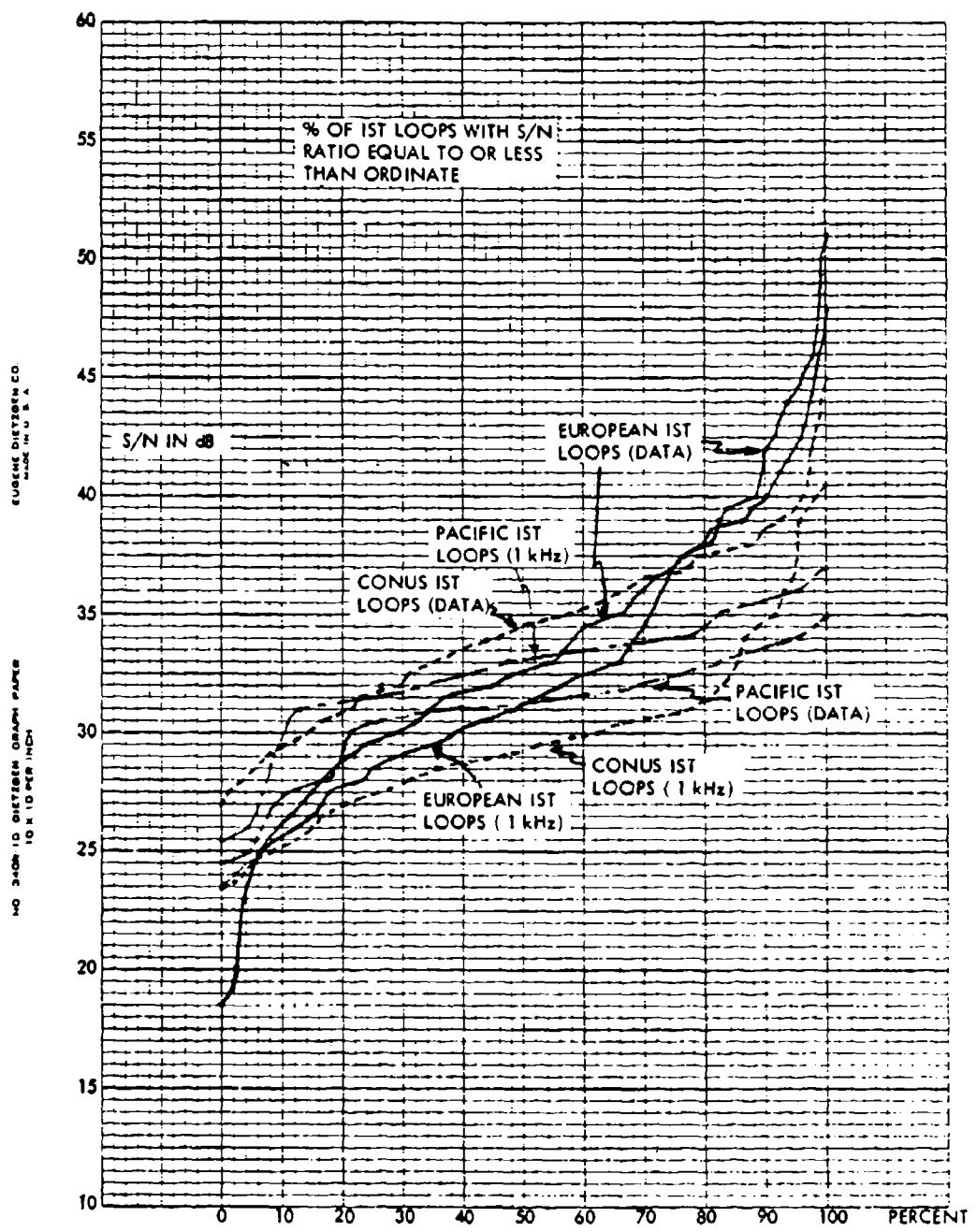


Figure 2.3-4

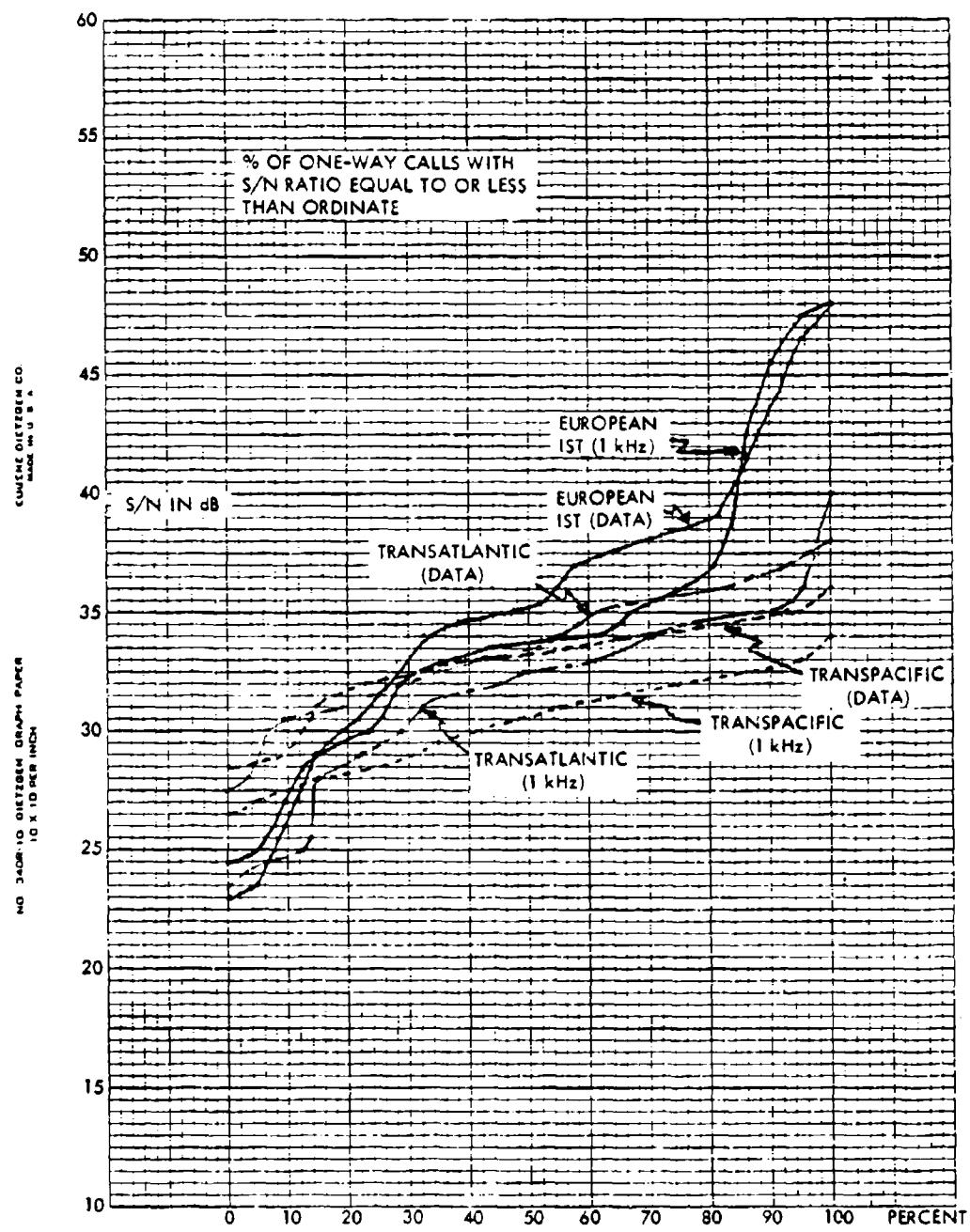


Figure 2.3-5

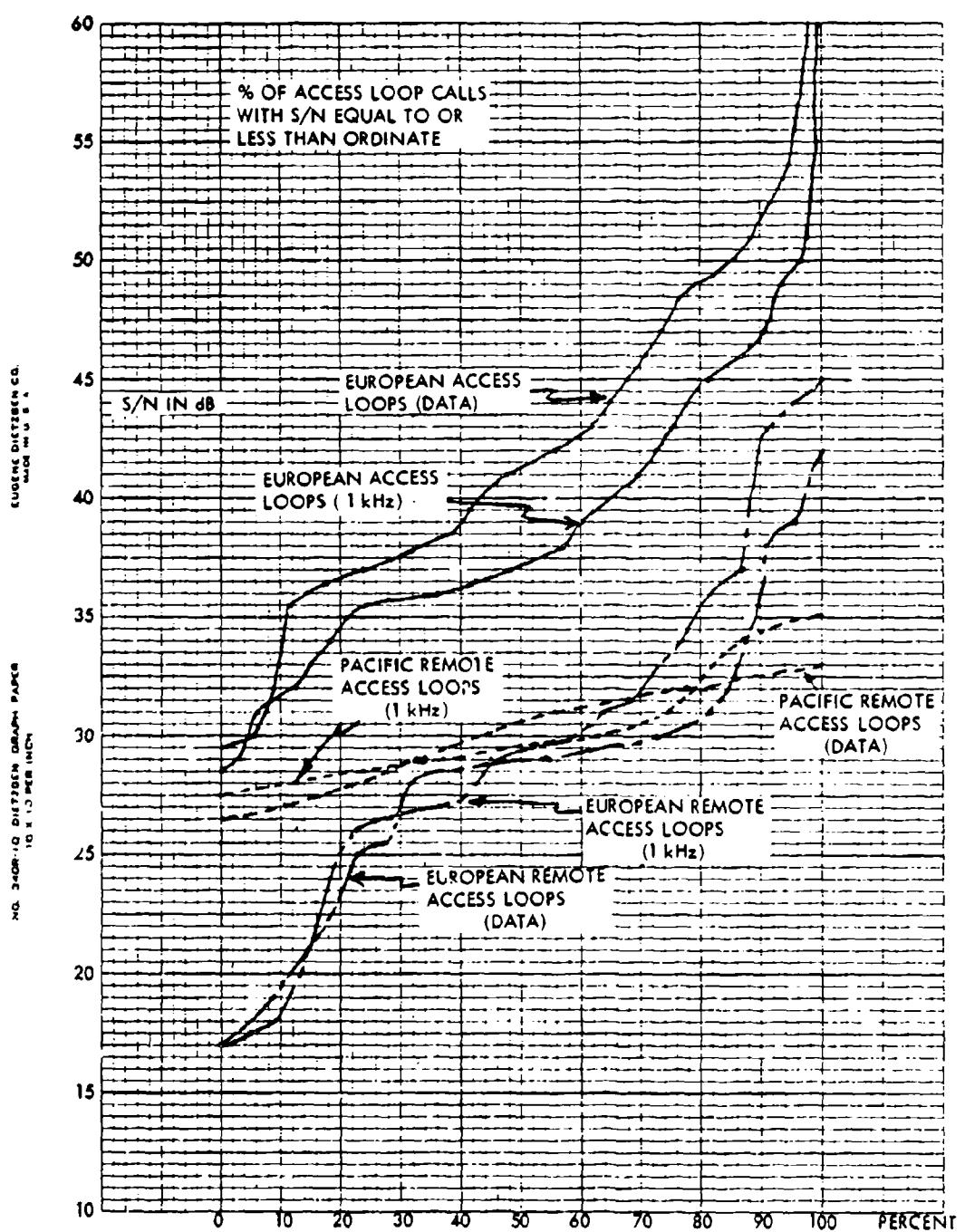


Figure 2.3-6

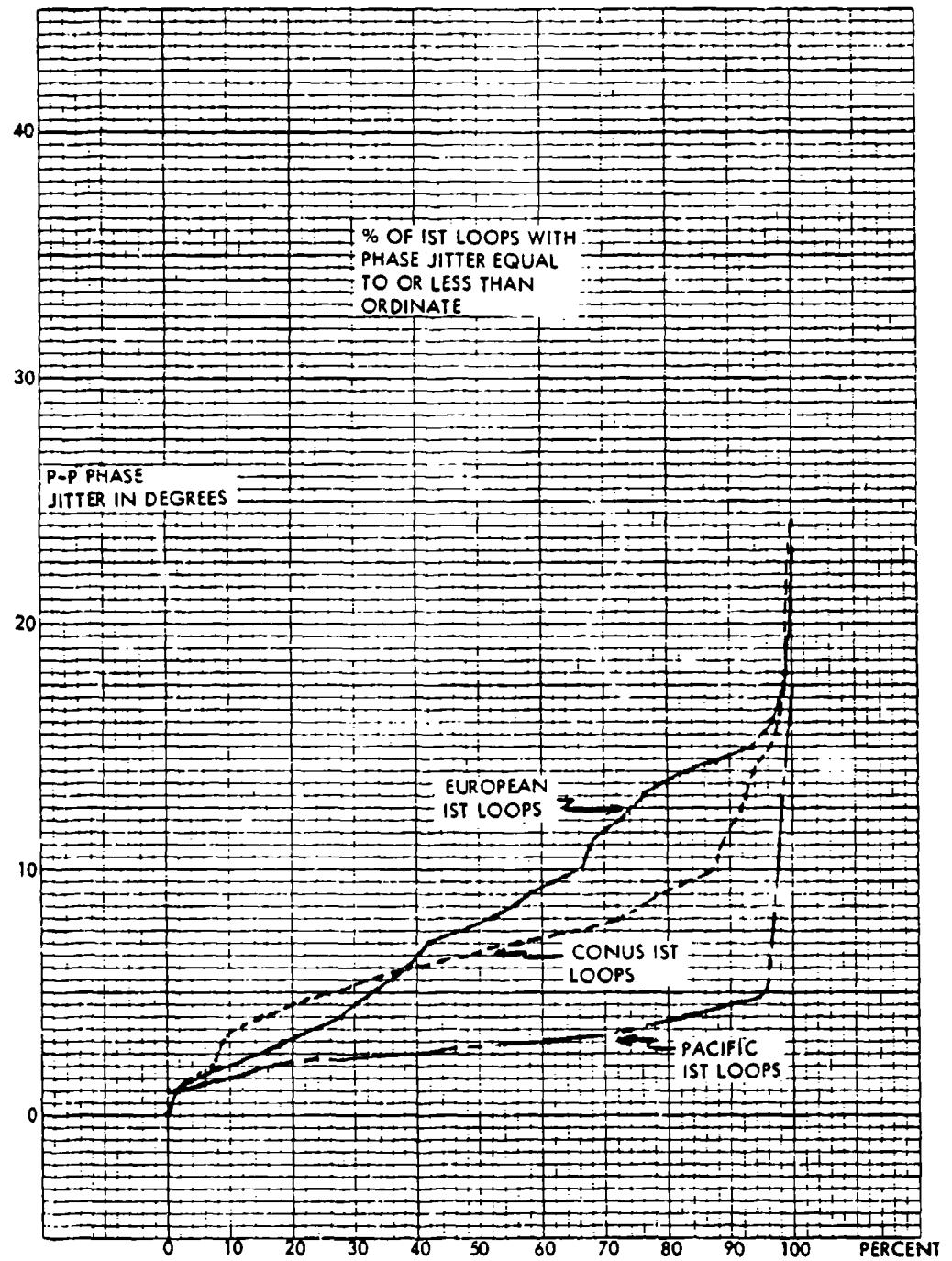


Figure 2.3-7

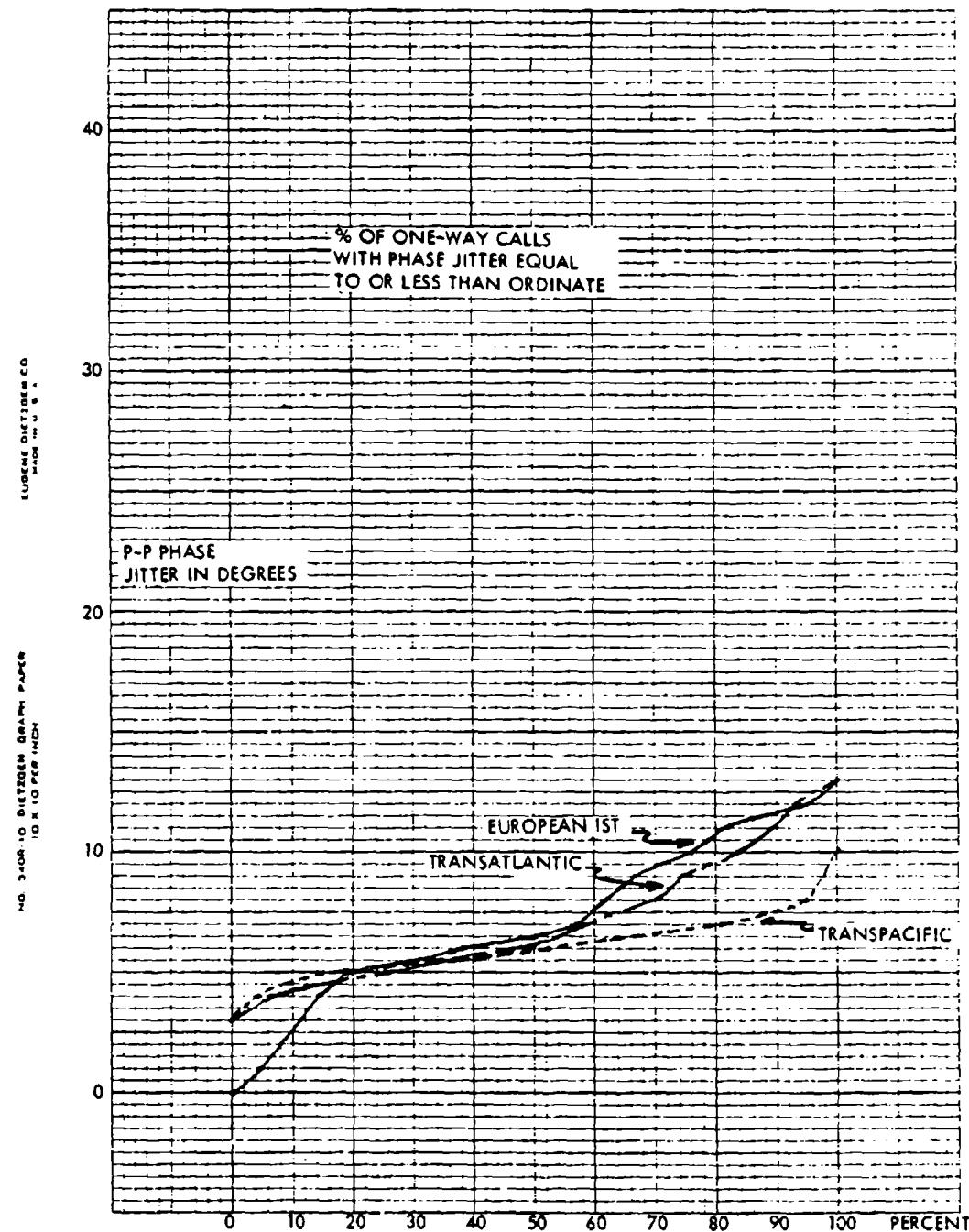


Figure 2.3-8

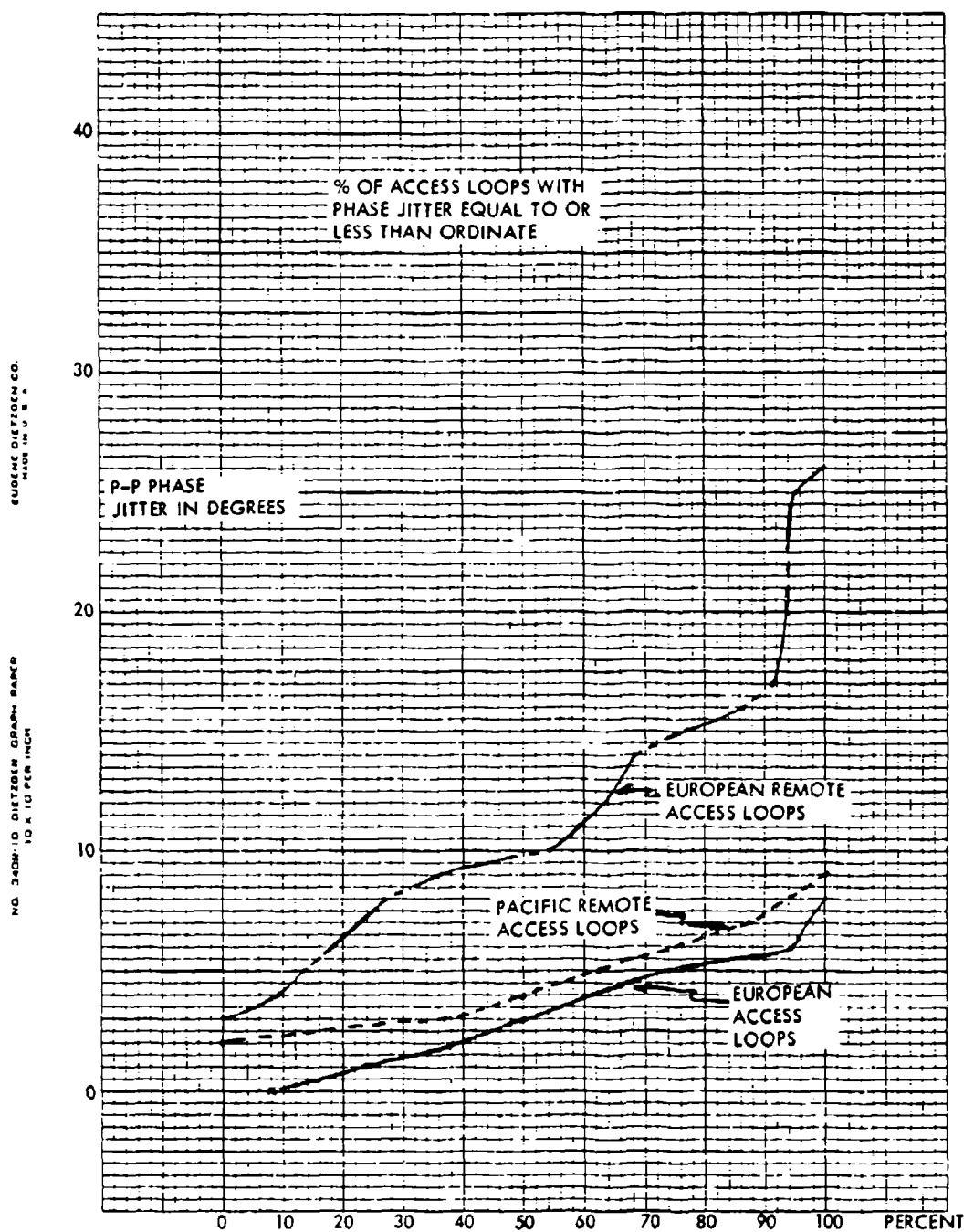


Figure 2.3-9

Table 2.3-2. Phase Jitter Spectrum

Call No.	<u>Highest Spectral Peak</u>		Overall Jitter Reading Degree P-P
	Approximate Frequency (Hz)	Approximate Magnitude Degree P-P	
18	50	3.8	6
20	100	1.9	4
21	130	3.8	25
22	50	11	15
23	20	7	15
24	50	7	23
27	130	2	8
30	100	2	11
31	100	2	10
37	100	2	7
38	100	4	10
39	100	4	10
46	20	3	12
47	50/100	5	14
51	50	1	14
52	50	1	12
53	20	3	16
55	-	1	13
58	50	1	13
60	20	2	9

Table 2.3-2. Phase Jitter Spectrum (Continued)

Call No.	Highest Spectral Peak		Overall Jitter Reading Degree P-P
	Approximate Frequency (Hz)	Approximate Magnitude Degree P-P	
61	100	4	10
62	120	8	10
66	—	4	10
67	50	7	12
82	50	7	15
88	100	7	14
95	100	4	10
99	100	12	15
102	50	5	—
126	0	5	6
156	100	12	15
162	100	9	12
169	200	7	15
172	—	5	18
182	—	6	16
206	0	11	12
207	0	20	29
226	50	20	16-22
276	—	2	15
313	60	9	9

contained relatively small amounts of periodic jitter at line frequencies and their harmonics. Spectrally shaped white noise would represent a better jitter model than sinusoidal jitter at line frequency harmonics. Modeling the jitter with a line frequency square wave would place an unrealistic burden on the modem.

Figures 2.3-10 through 2.3-18 present harmonic distortion information. The curves concerning second and third harmonic distortion present the size of these harmonics in decibels below the size of the signal tones transmitted during the harmonic distortion measurement. A more detailed description of the technique employed in the harmonic distortion measurement is given in Paragraph 2.4. Figures 2.3-16, 2.3-17, and 2.3-18 present the total harmonic distortion as a percent of the transmitted signal. It is interesting to note that on the calls where both one-way and looped data was obtained, the harmonic distortion on looped calls averaged 2.19 times that achieved on on-way calls. On this basis 80 percent of the CONUS IST lines tested would have a total harmonic distortion of 1.54 percent or less. With the exception of the Pacific remote access calls all of the types of overseas calls had 80 percent values in the vicinity of 1.5 percent or less. It is suspected that bad harmonic distortion observed on the Pacific remote access loops was due to the nature of the loop-around rather than the actual circuits. However, this was not substantiated. As previously discussed the high harmonic distortion associated with the trans-Atlantic calls was felt to be primarily due to the CONUS access lines rather than the trans-Atlantic lines.

Figures 2.3-19 through 2.3-30 present data on various hit activity in the channel. Figures 2.3-19, 2.3-20 and 2.3-21 show the distribution of the number of 3 dB amplitude hits in a 5-minute period. Figures 2.3-22, 2.3-23, and 2.3-24 show the distribution of 20° phase hits per 5-minute period. Figures 2.3-25, 2.3-26, and 2.3-27 give impulse noise distribution over a 5-minute period. The threshold settings for the impulse noise measurements were set at 67, 63, and 59 DBRNO. Figures 2.3-28, 2.3-29 and 2.3-30 show the distribution of dropouts. Paragraph 2.4 will describe the technique of measuring these channel hit phenomena.

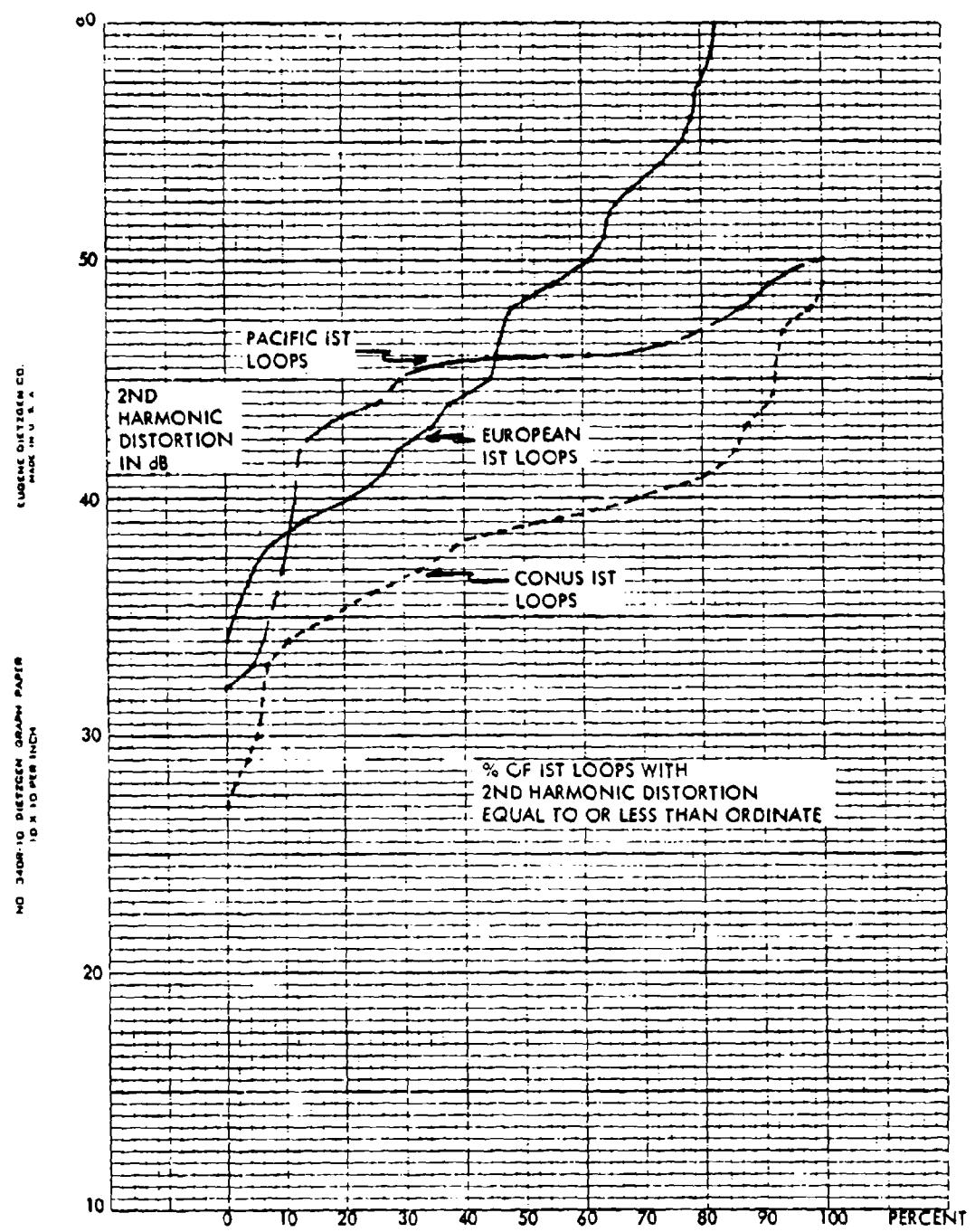


Figure 2.3-10

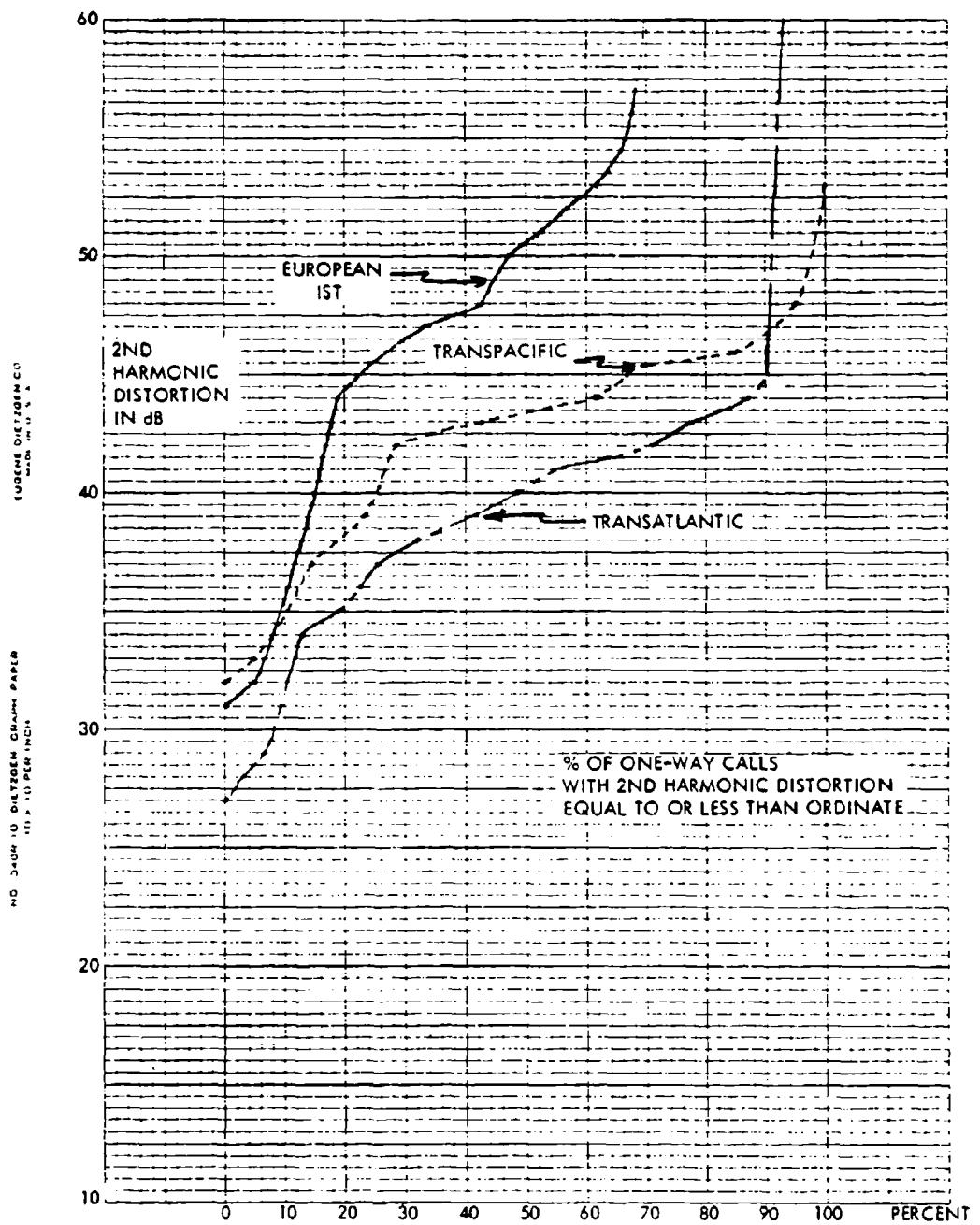


Figure 2.3-11

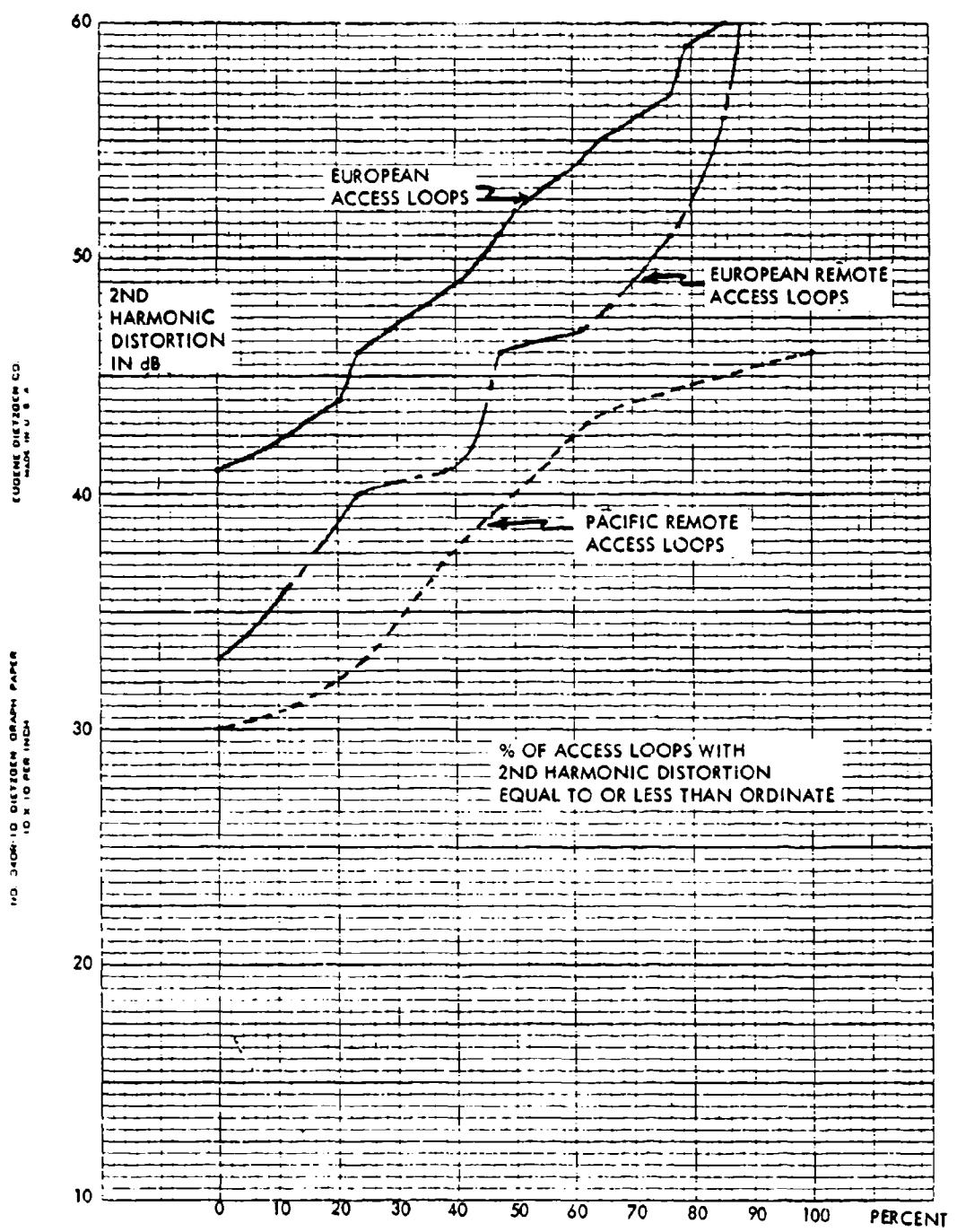


Figure 2.3-12

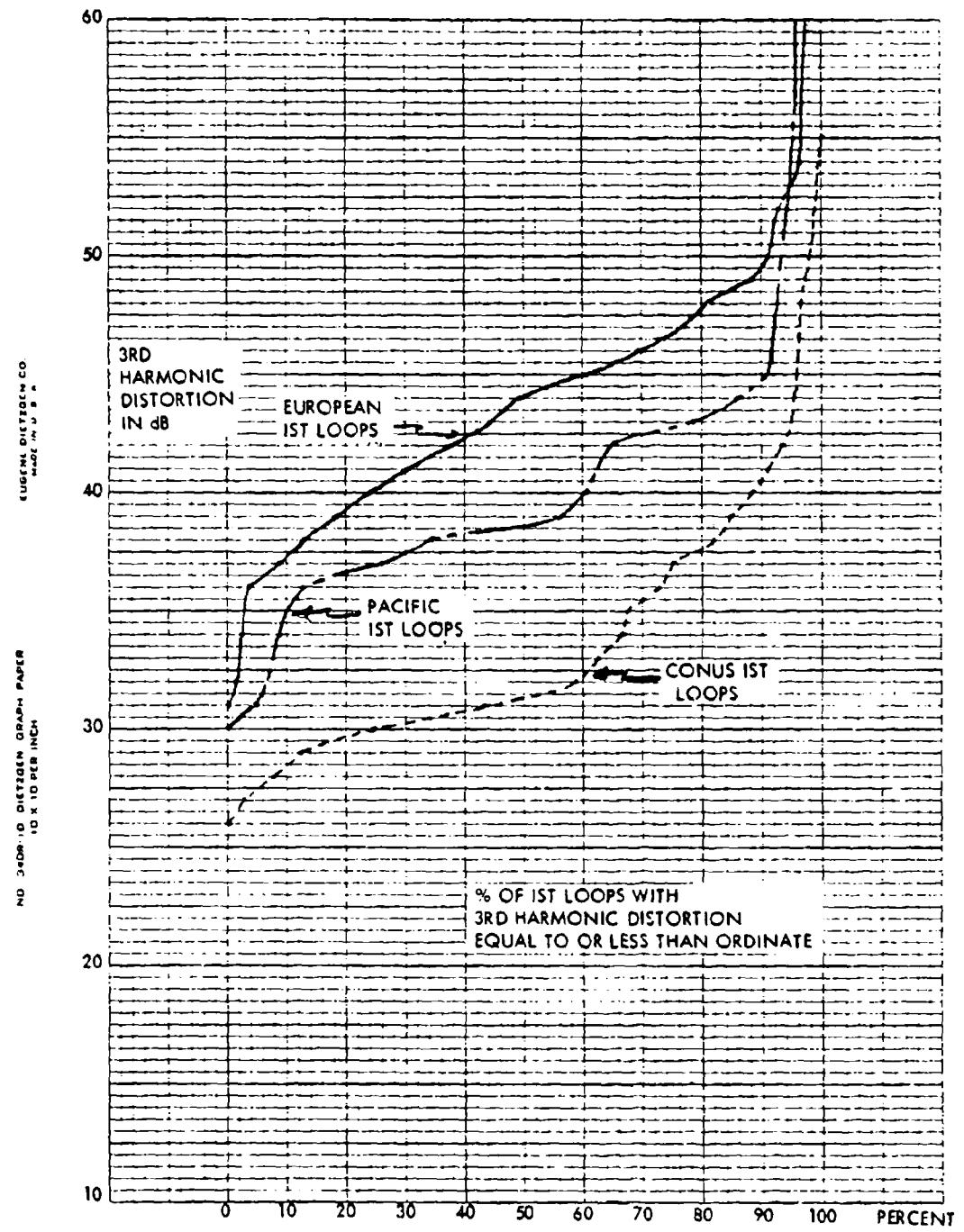


Figure 2.3-13

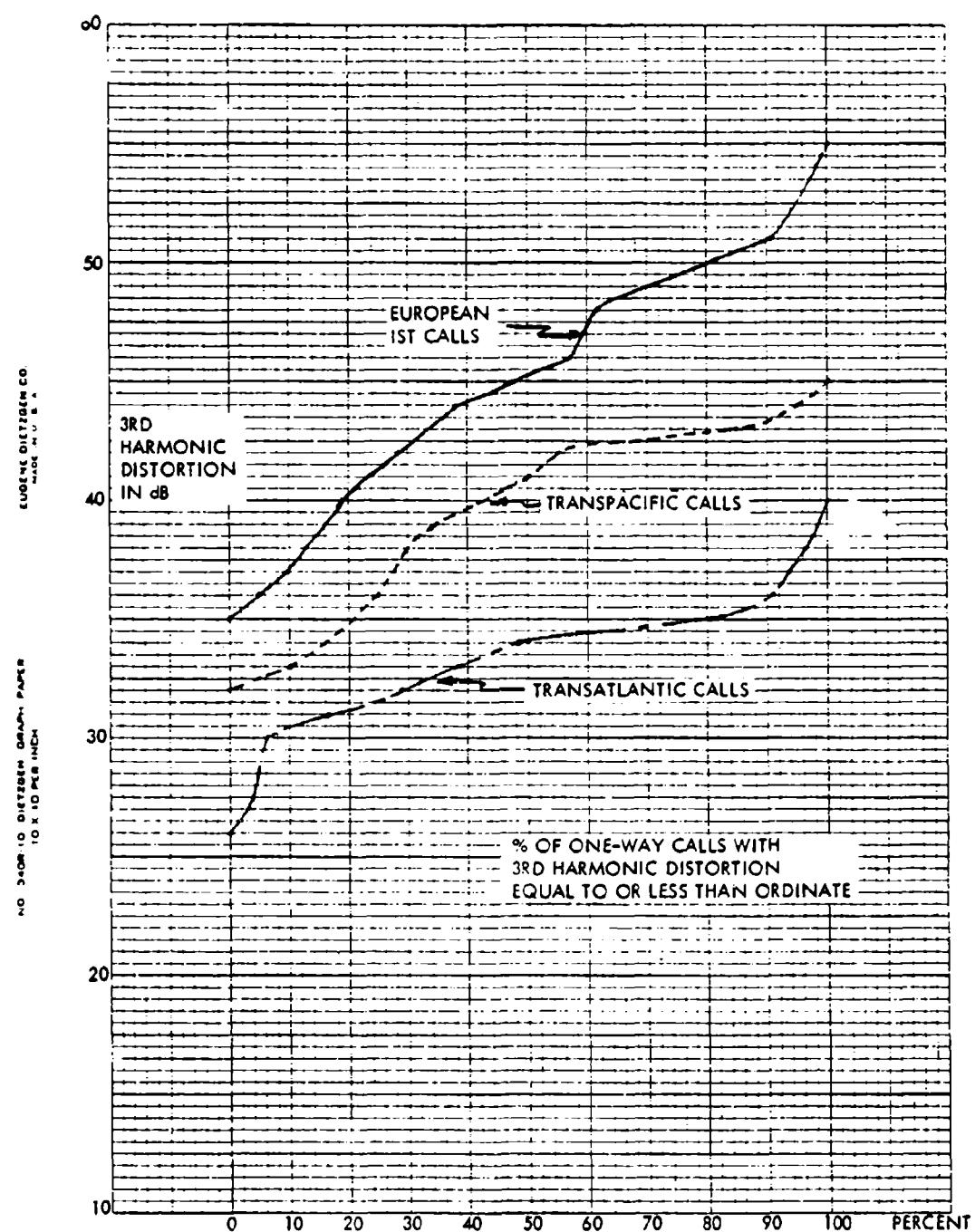


Figure 2.3-14

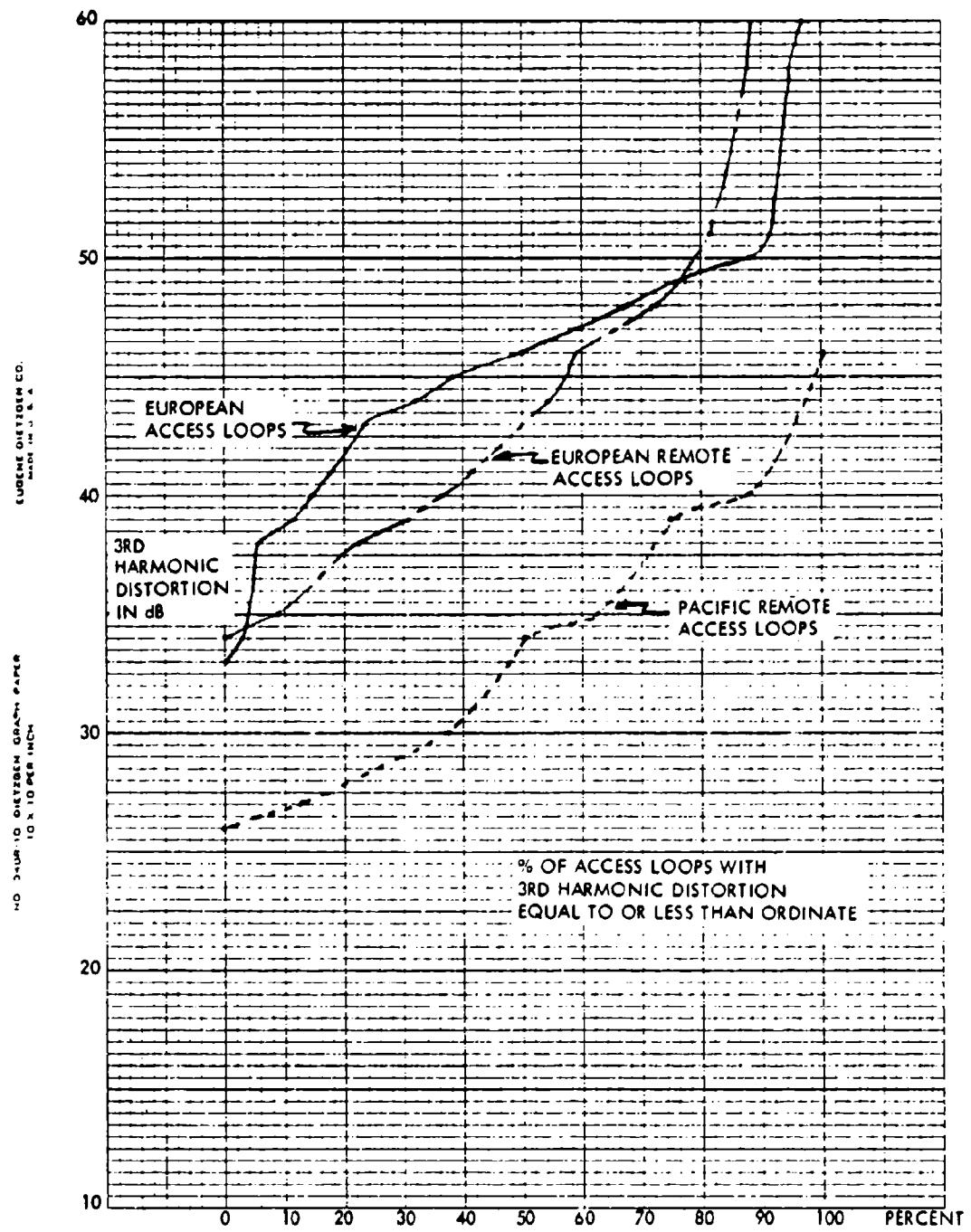


Figure 2.3-15

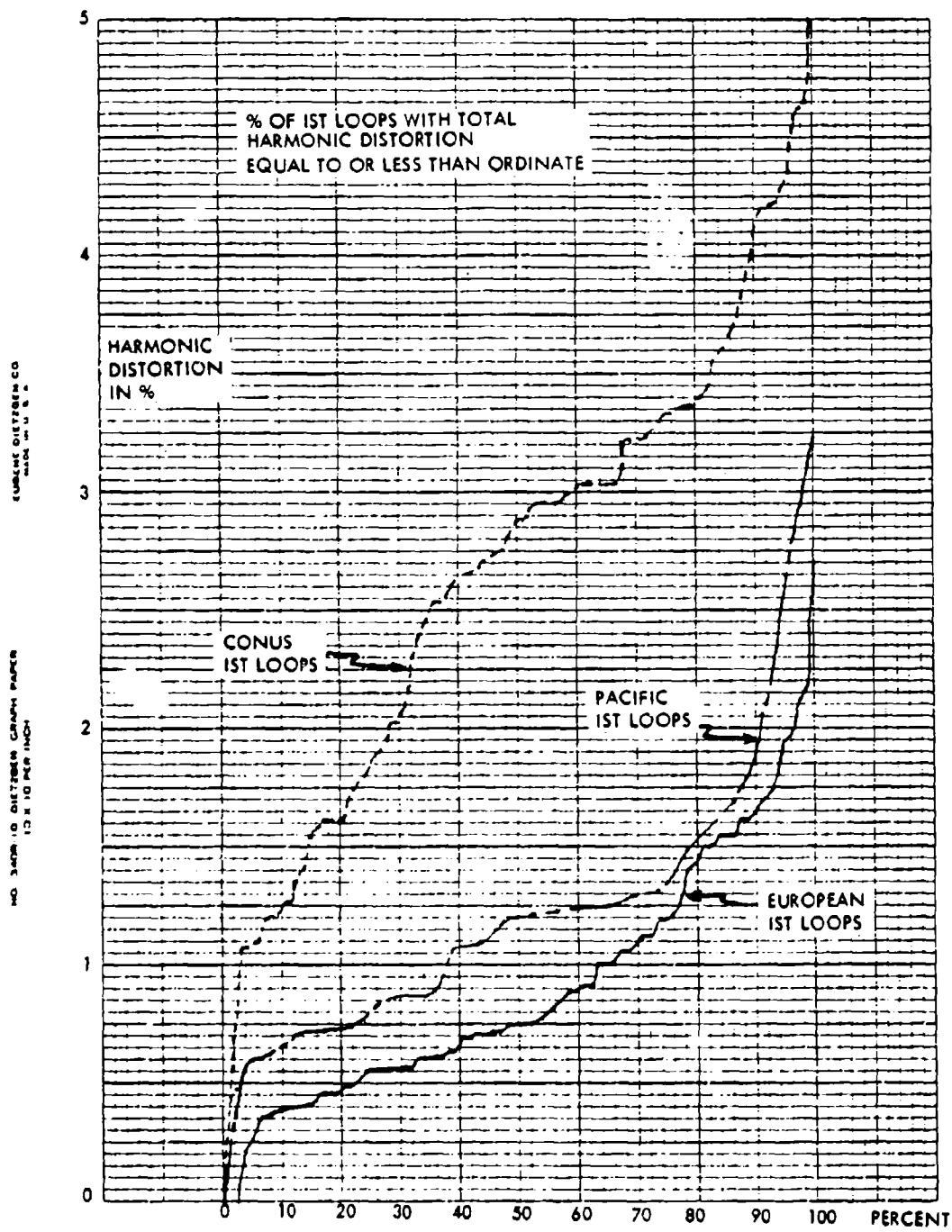


Figure 2.3-16

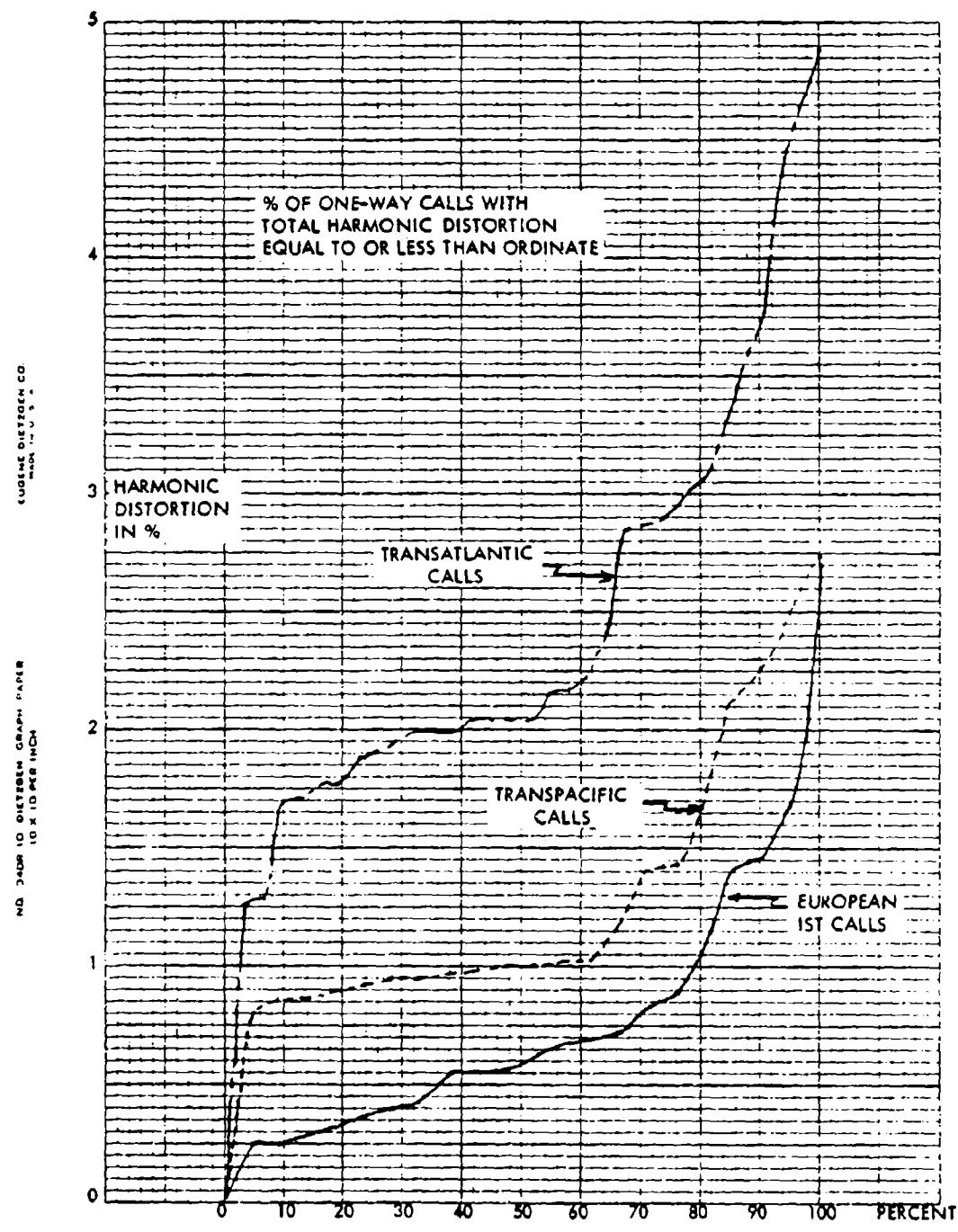


Figure 2.3-17

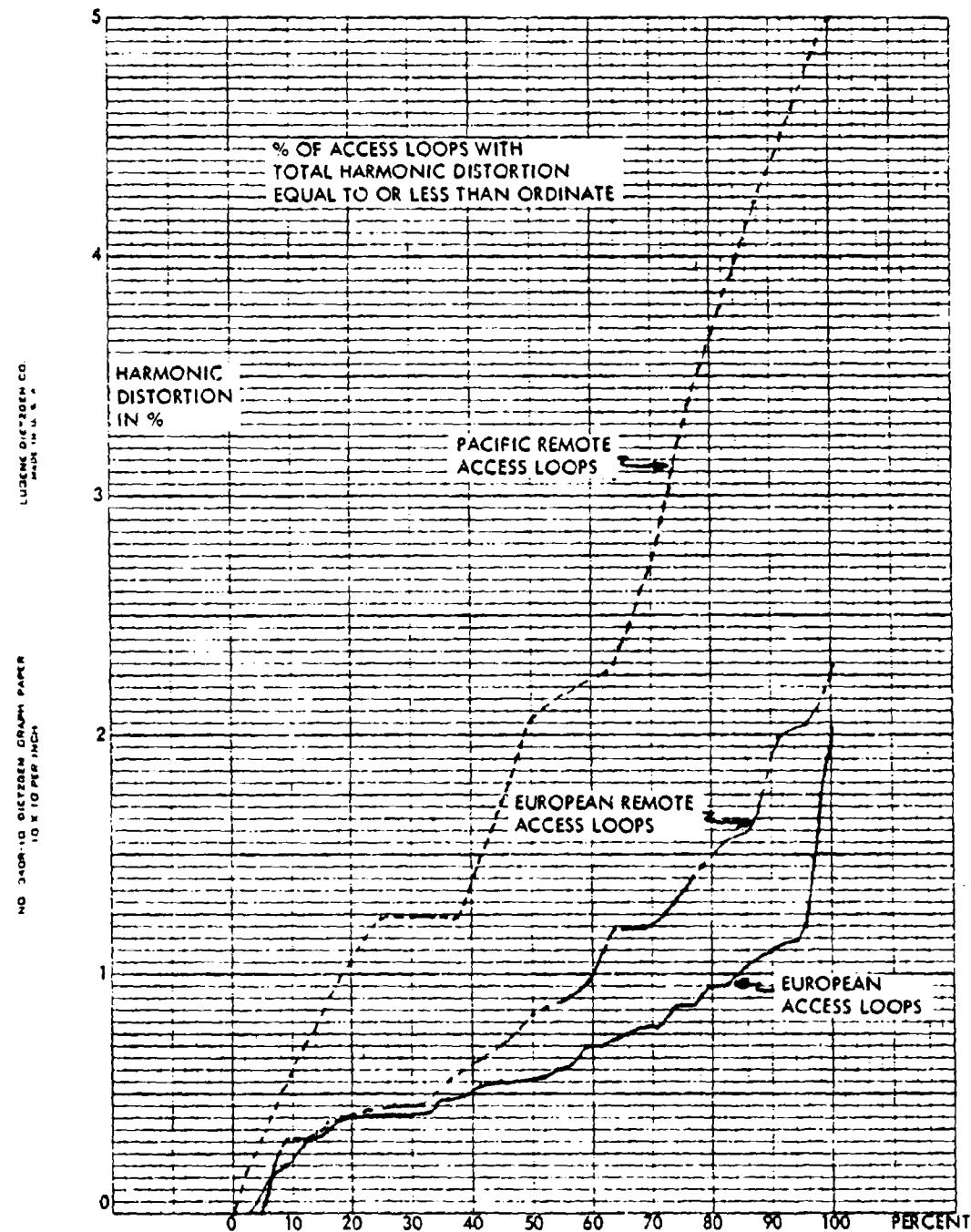


Figure 2.3-18

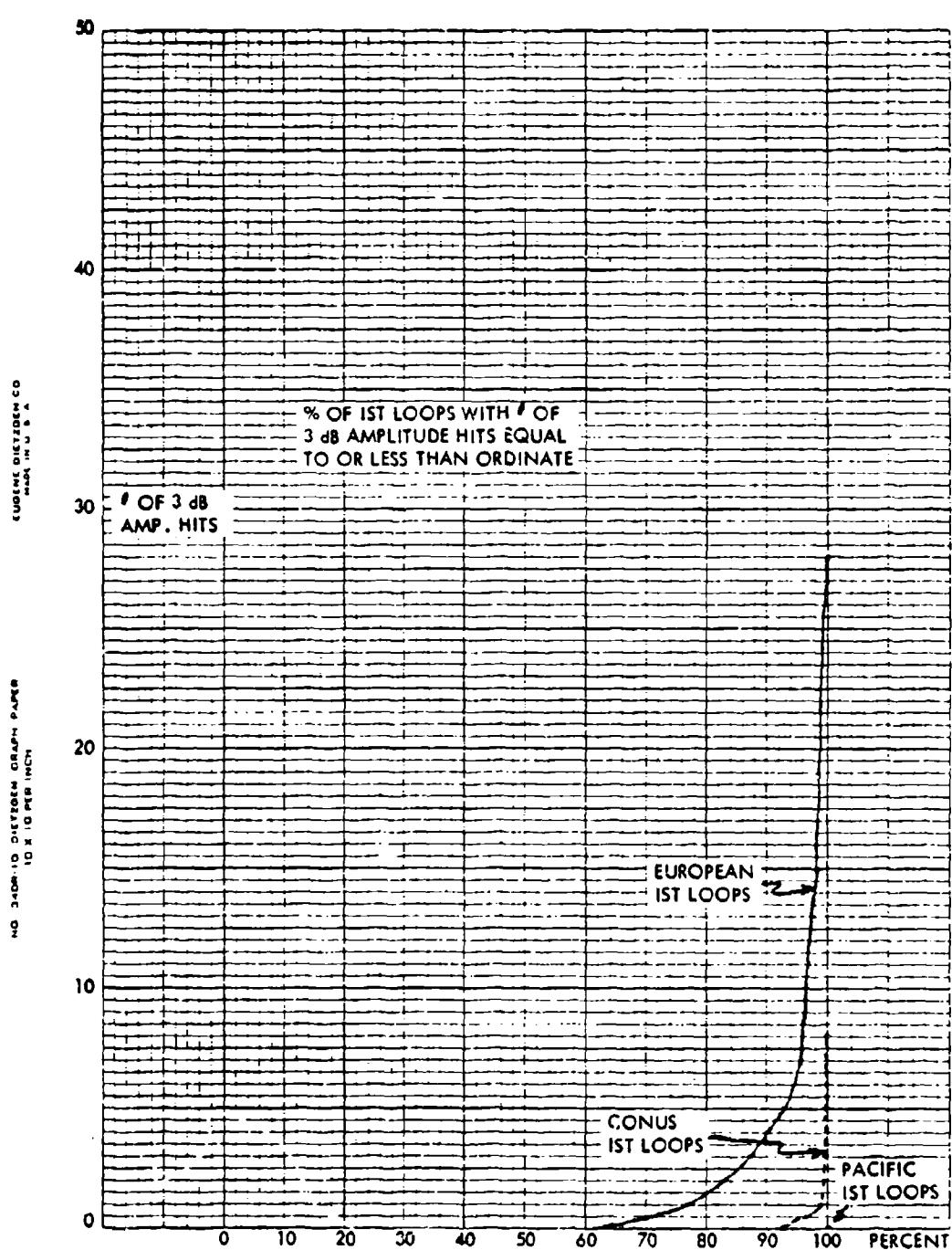


Figure 2.3-19

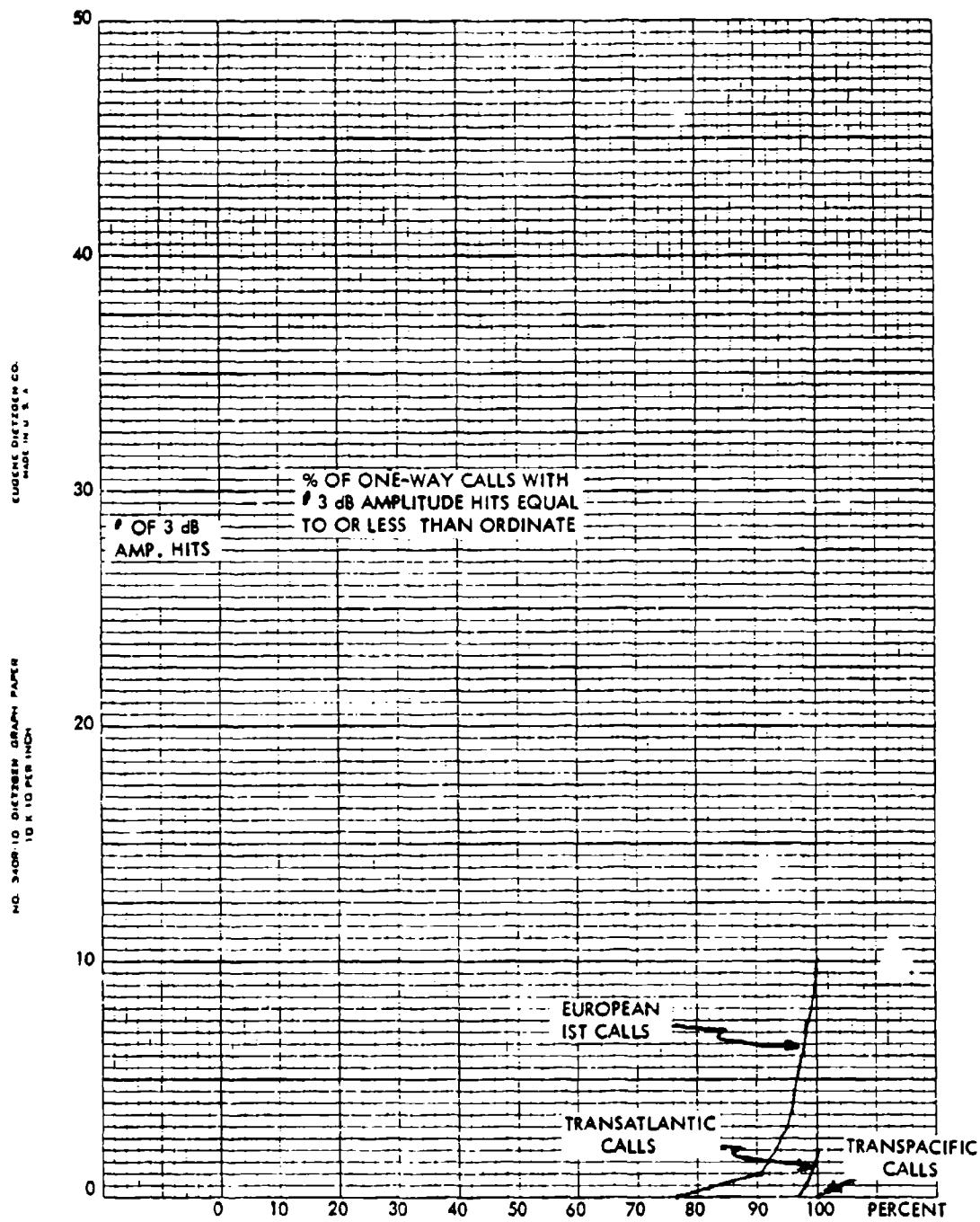


Figure 2.3-20

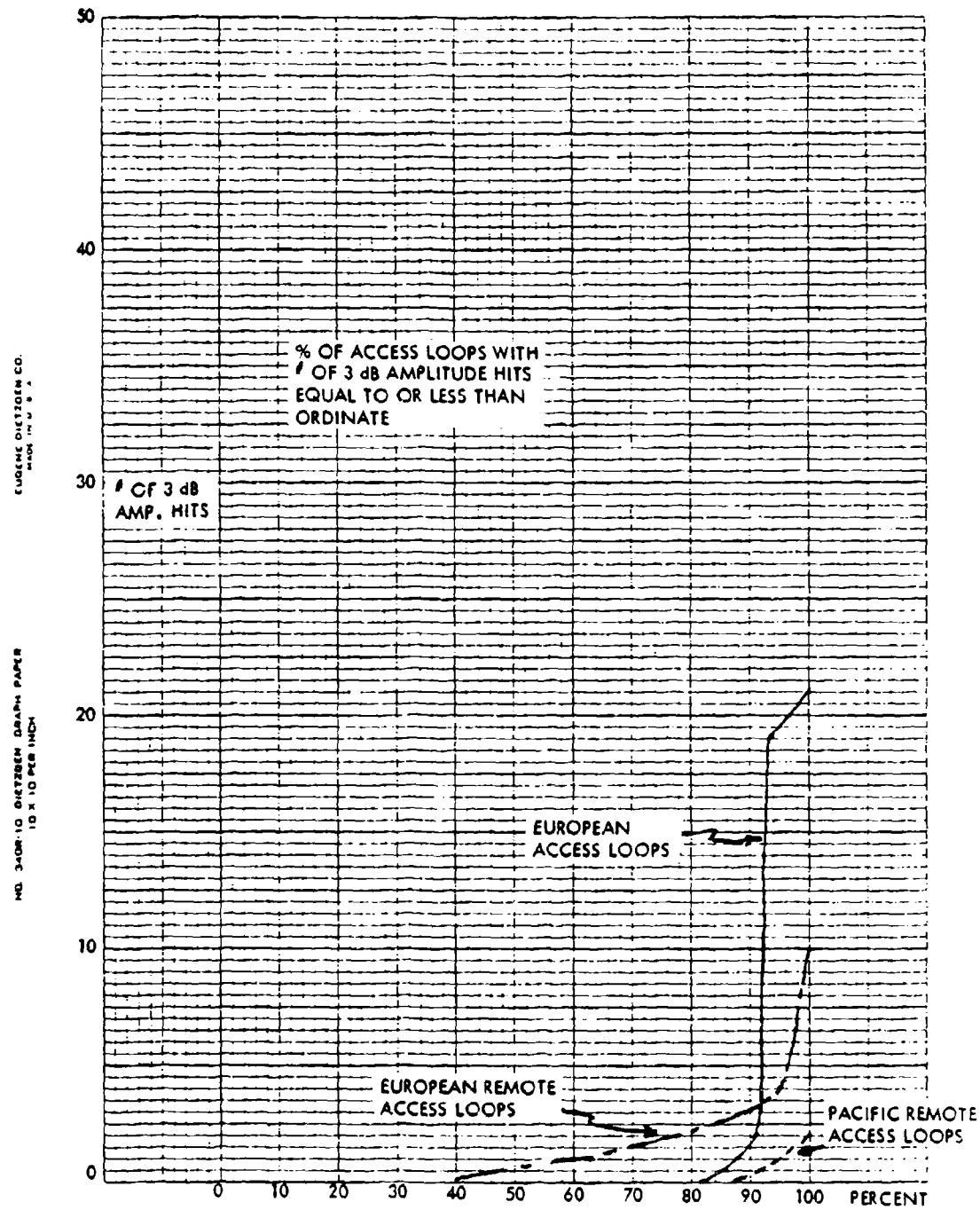


Figure 2.3-21

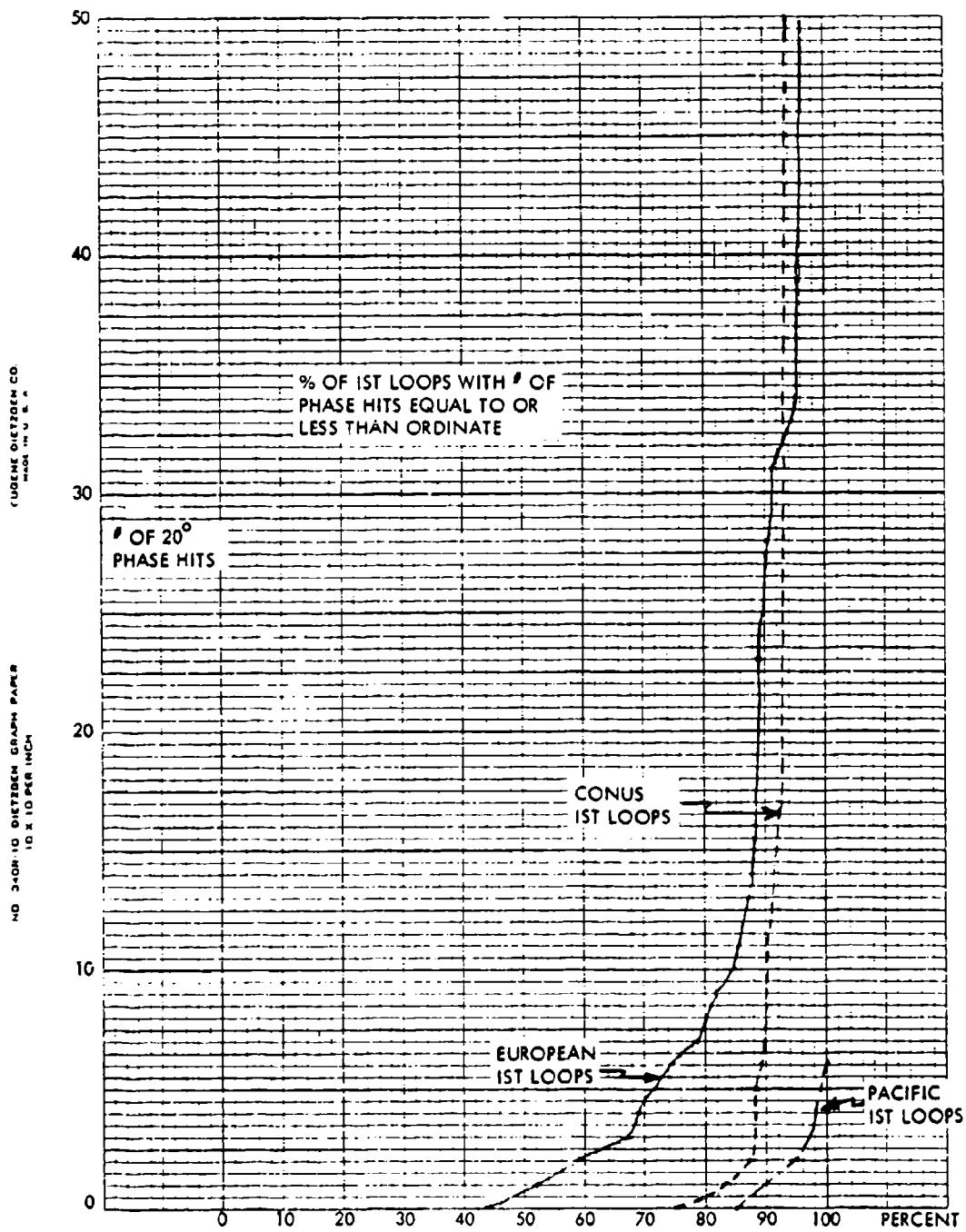


Figure 2.3-22

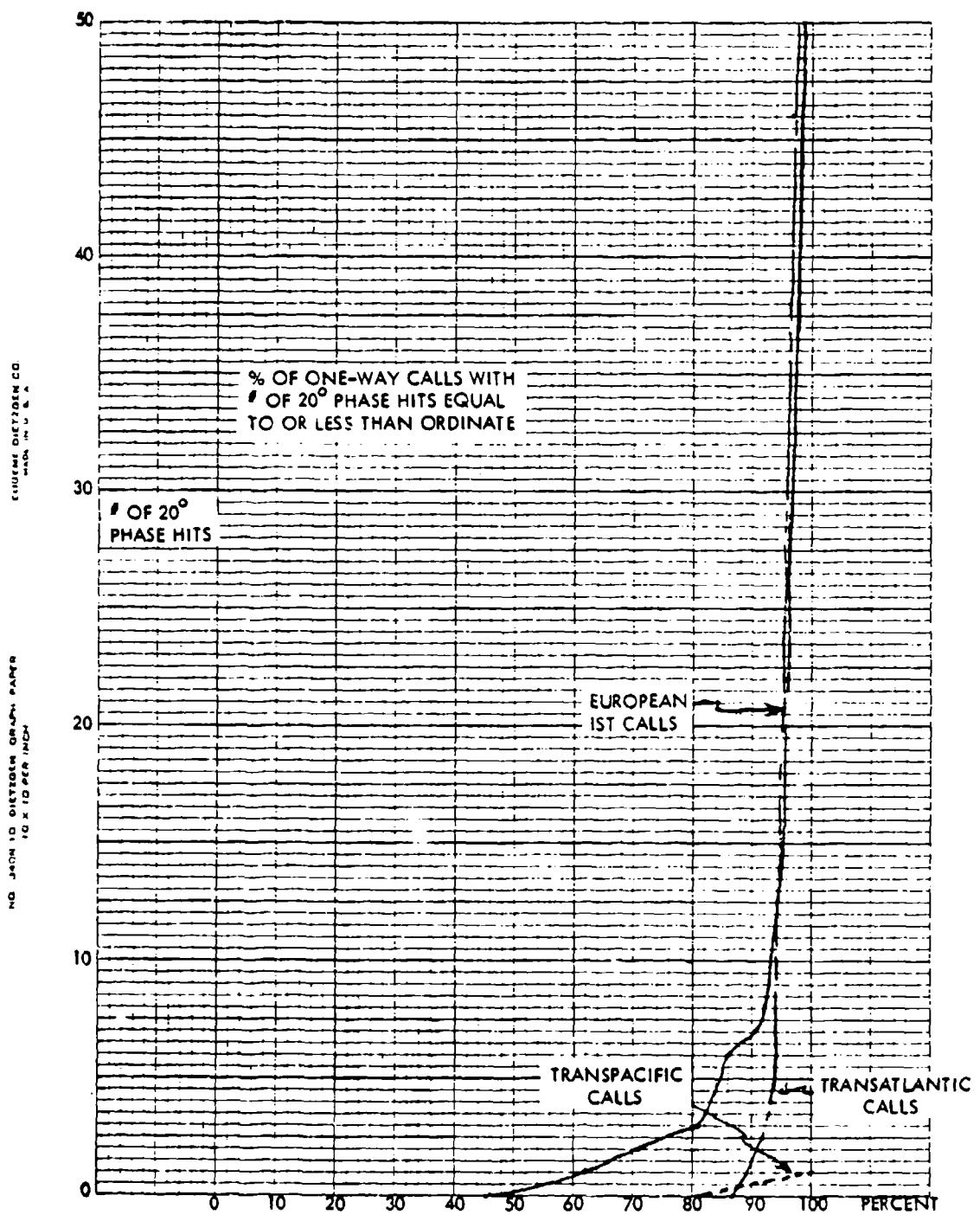


Figure 2.3-23

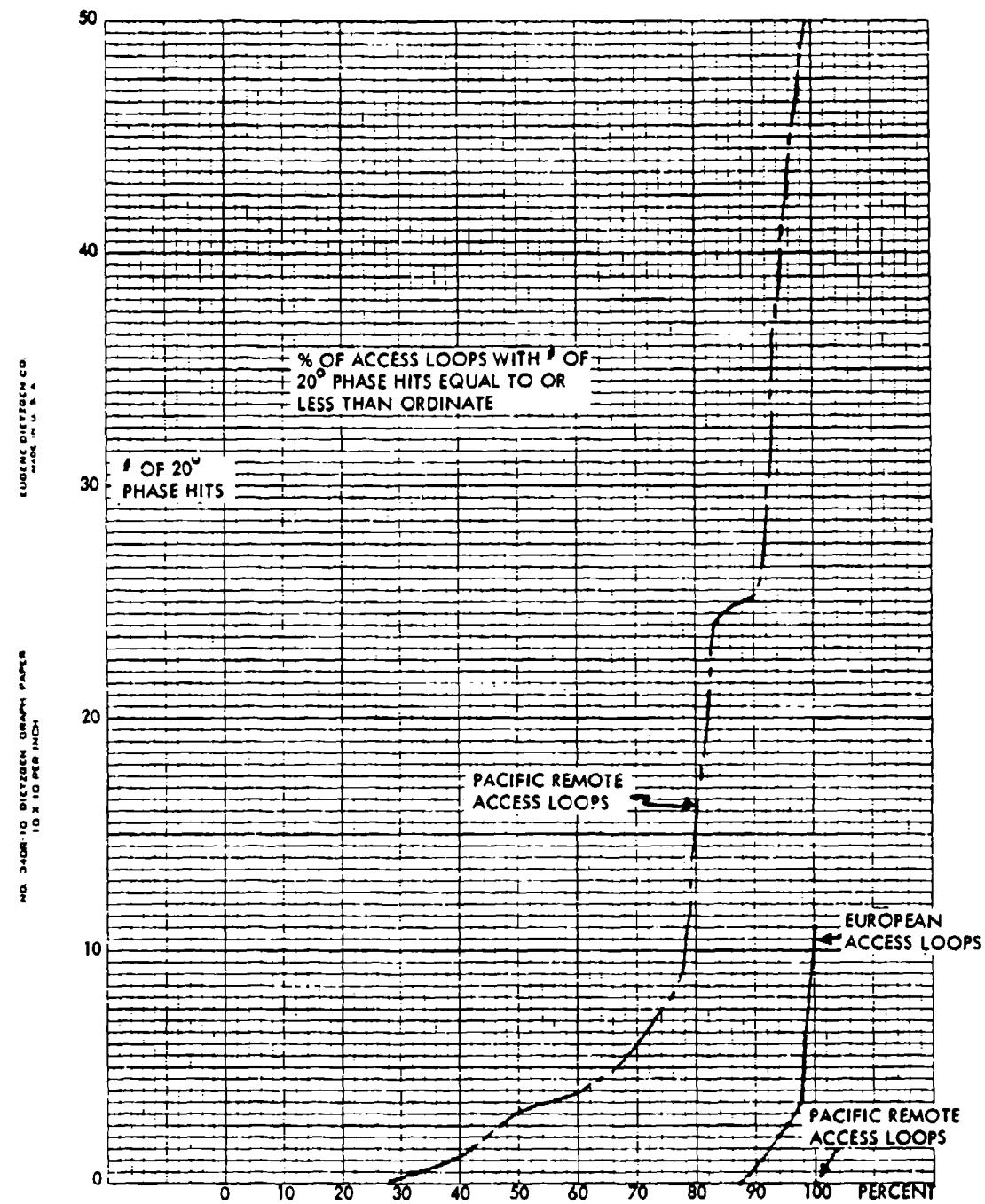


Figure 2.3-24

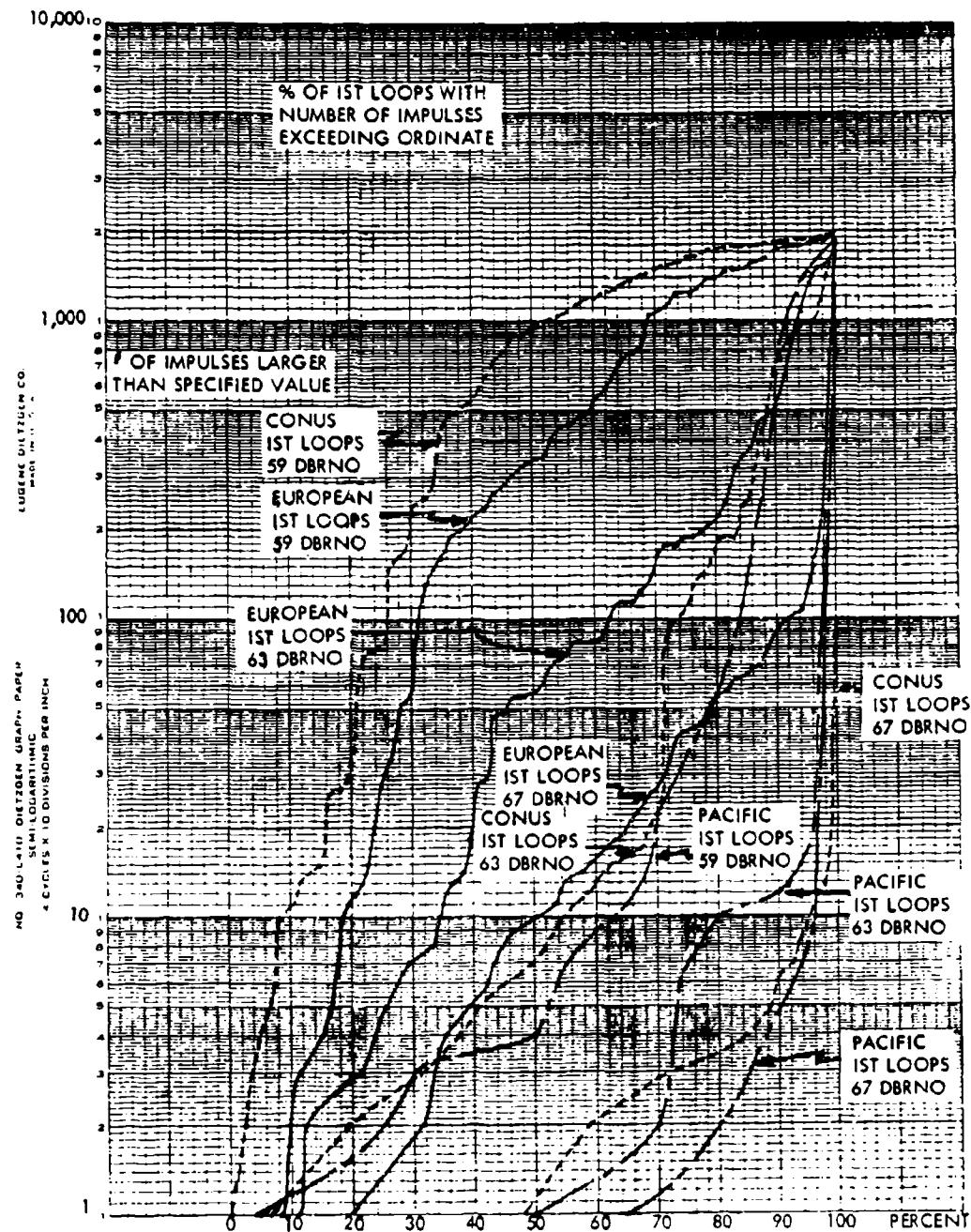


Figure 2.3-25

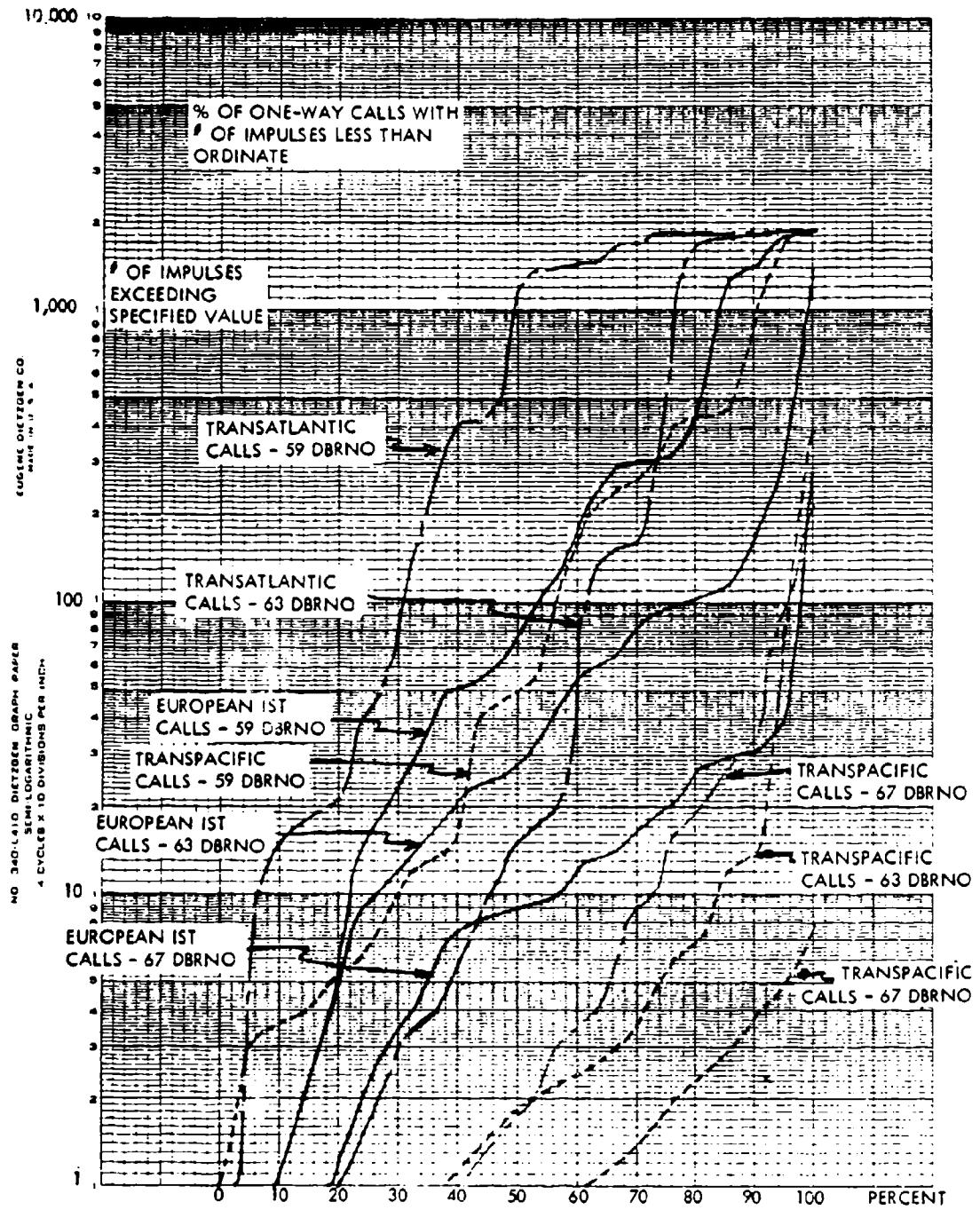


Figure 2.3-26

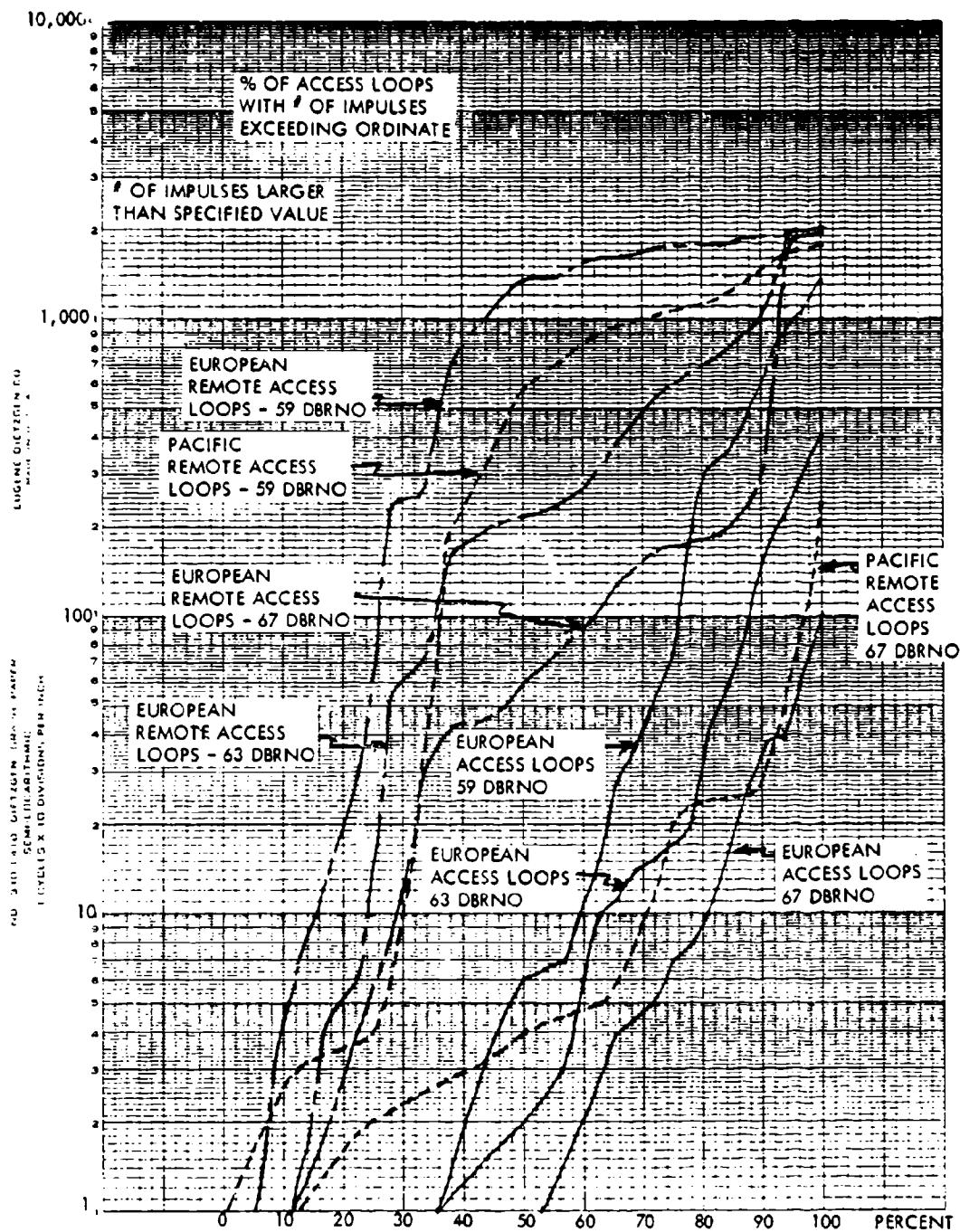


Figure 2.3-27

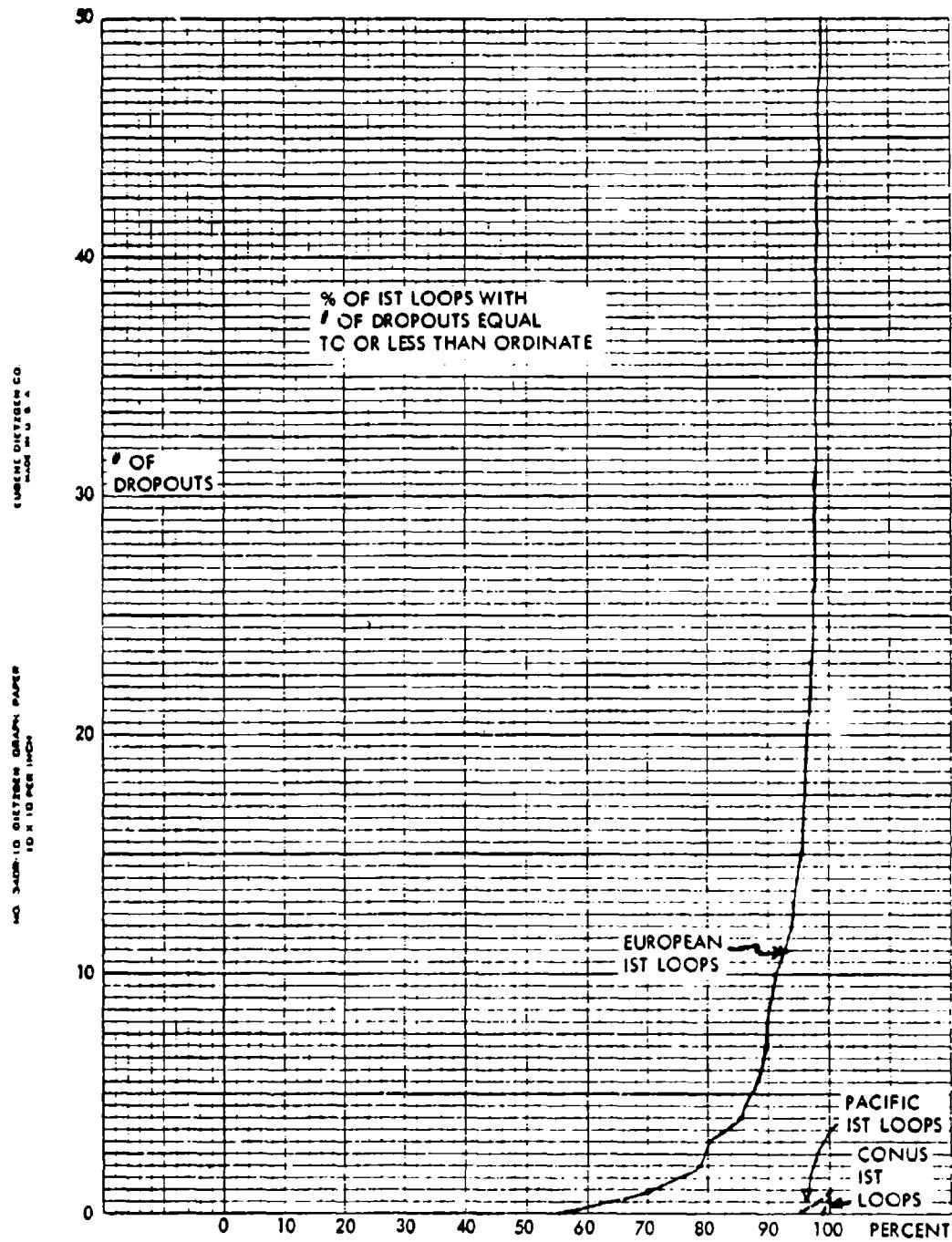


Figure 2.3-28

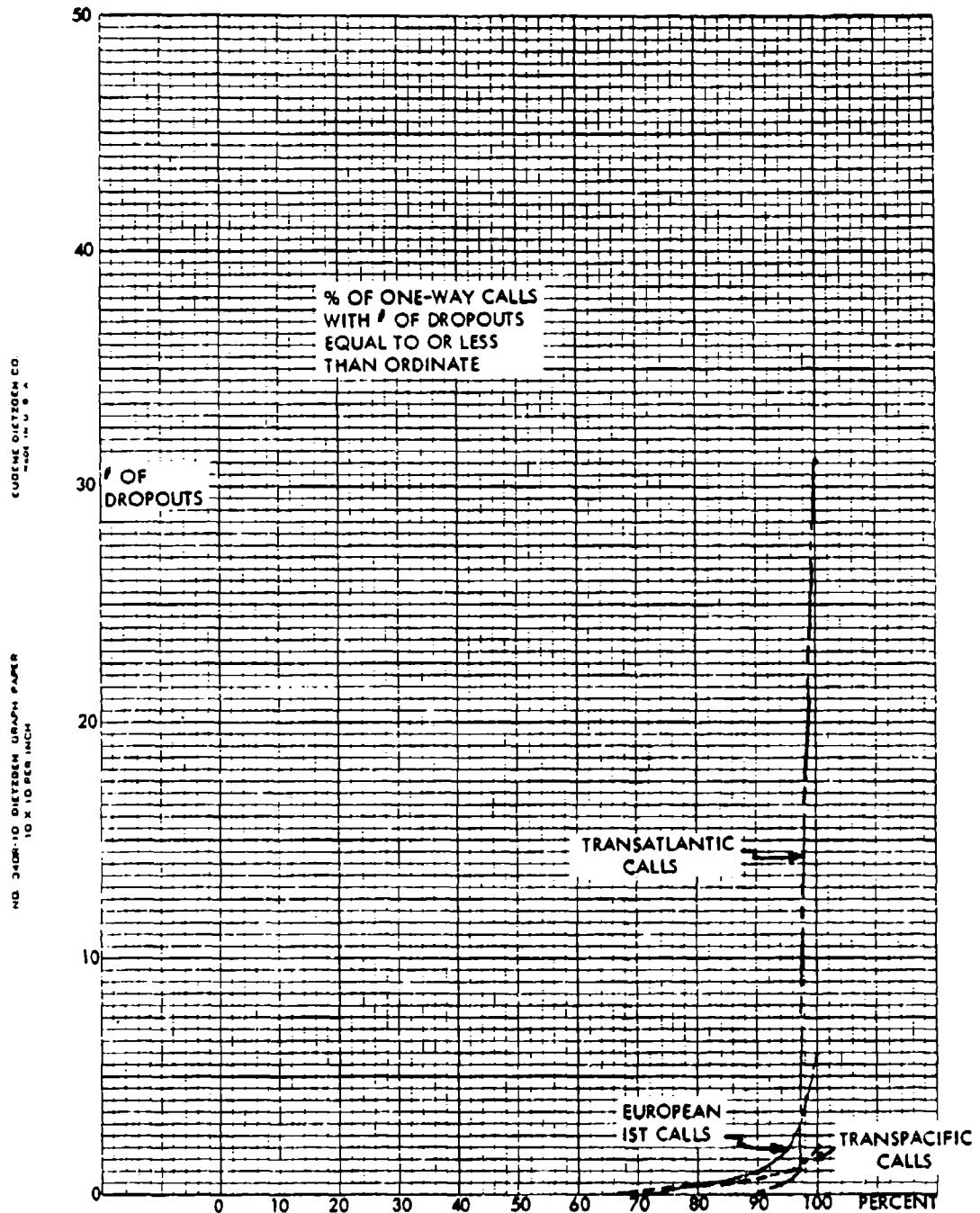


Figure 2.3-29

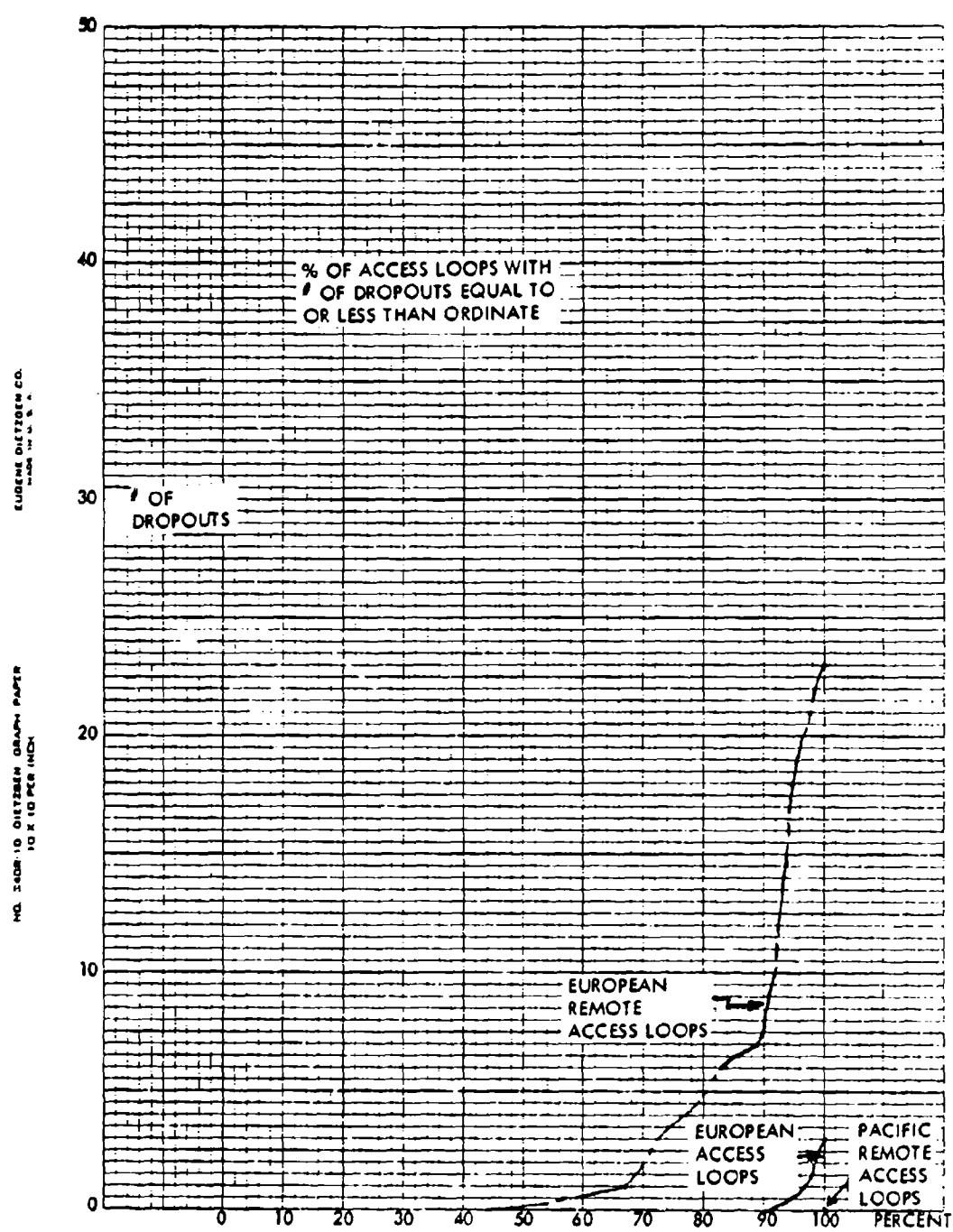


Figure 2.3-30

The data on amplitude response and group delay response of the lines was obtained by taking a photograph of the Halcyon display of these characteristics. These photographs are included in the report so that a comparison can be made with standard specification values. Each of the photographs was compared with V1, V2, S1, and S3 specifications and the tightest specification met was recorded for that call in the tables in Appendix C.

It should be noted that operation on data grade lines conditioned to S3 specifications will not necessarily yield a response meeting S3 specifications since the call may involve several circuits. This is emphasized in loop-around calls, and is also true of standard calls. The S1 specification is a user end-to-end specification for data grade lines and is supposed to take this into account; however, any attempt to specify end-to-end performance must imply a limitation in the number of sequential circuits involved. It is the individual circuits that are actually checked against the specified characteristics.

Tape recordings were made on virtually all calls. The recordings usually consisted of an introduction followed by a recitation of IEEE test sentences listed in Appendix E. The test sentences were normally played from a prerecorded tape but were sometimes read by the person at the transmitter site. The quality of the recordings from the prerecorded test tape was lower than that when the test sentences were read directly into the CVSD. This probably indicated a problem in the recorder - CVSD interface. Requests concerning these tapes should be addressed to RADC/DCLD, Griffiss AFB NY 13441.

## 2.4

### Test Procedures

This section describes the methods used for making connections to the lines, dialing the test connections, tracing the circuit routings, and also covers the equipment setup and measurement procedures.

#### 2.4.1

##### Connection Procedures

Connections were normally made to the network from either an AUTOVON or secure voice switch. The line access was by means of an extension from a secondary board or a test board. Connections for the testing were performed in several ways depending on the exact type of circuit to be established. For one-way calls the other location was simply dialed in the normal manner. For IST loops the switch loop-around numbers were utilized. For access line loops served by the originating switch, the loops were normally established by requesting a loop-around from Tech Control at the desired location. For remote access line loops, i.e., those served by a foreign switch, the procedure was slightly more complicated. Here it was necessary to patch around the echo suppressors at the switch serving the access line to be tested. Once this was done the loop at the remote access point was established at Tech Control or a test board in a similar manner to the local access line loops.

In order to establish the routing of the calls, a test tone was placed on the line and personnel at intermediate switches were requested to find the incoming and outgoing circuits with the tone. Normally the identification received was in the form of a Command Communications Service Designator (CCSD) number or equivalent, although in some cases group and channel number information was obtained directly.

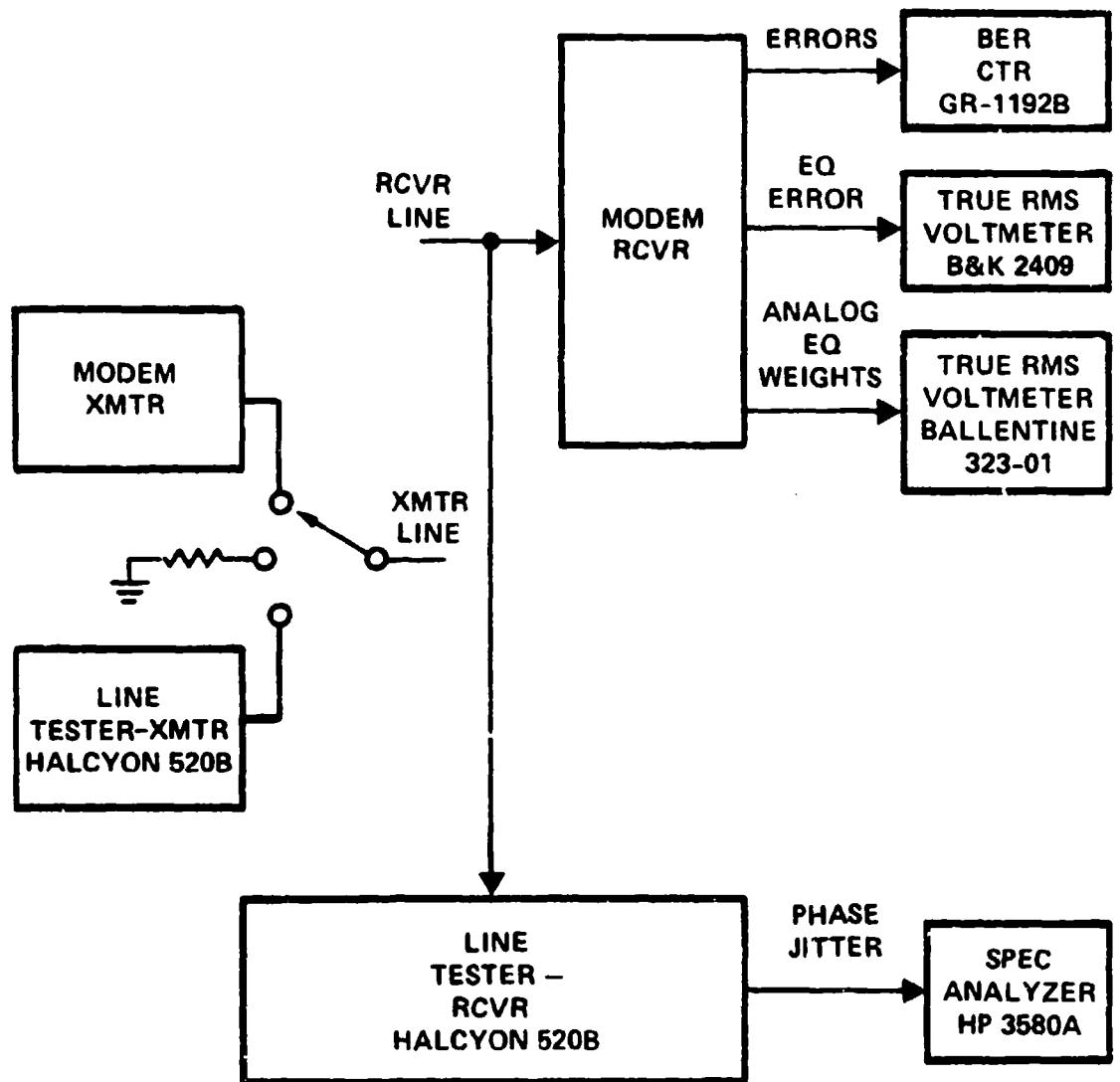
## 2.4.2      Equipment Setup

A block diagram of the test setup is shown in Figure 2.4.2. The transmit line was arranged so that it could be switched to either the mcdem transmitter, the line tester transmitter port, or a quiet termination. The receive line was connected in parallel to the modem receiver and to the line tester receive port. The modem included a terminating resistor, but the line tester was operated in a bridged mode so that only a single termination was presented to the line.

The modem includes a pseudorandom pattern generator in the transmitter and a second identical pattern generator in the receiver. The receiver sequence generator was automatically synchronized during the modem training process. Subsequently, a bit-by-bit comparison was made between the receive data and the receive sequence generator, with mismatches indicated by error pulses. These bit error pulses were brought out of the modem and applied to the bit error rate counter. The modem also produced two other signals used for analyzing performance. The analog error at the equalizer output was brought out and monitored on a true rms voltmeter. Also, the equalizer weights were converted to analog form and brought out for monitoring on a second true rms voltmeter. It was hoped that the equalizer weight measurement would provide an overall measure of line filtering, but no strong correlation was observed.

The analog line parameters were measured with a Halcyon Universal Test System, Model 520B. This unit provided test of the standard analog parameters in the manner described in the next paragraph. In addition, the unit was modified to bring out the phase jitter signal. This phase jitter signal from the internal phase detector was routed to a low frequency spectrum analyzer to provide data on the spectrum of the jitter components.

For the transmit end of the one-way tests, only the transmit portion of the modem and the line tester were utilized.



SIGNAL LEVEL  
 IDLE NOISE  
 NOISE WITH TONE  
 PHASE JITTER  
 NONLINEAR DIST  
 AMP. RESPONSE }  
 ENV. DELAY }  
 HITS } PHOTOS

89597-13

Figure 2.4.2. Modem Line Test Setup

### **2.4.3      Measurement Procedures**

This section describes the methods used for reading and recording the various modem performance and line parameters.

#### **2.4.3.1    Bit Error Rate**

The bit error rate was measured using the internal pattern generators in the modems as described above. Normally, error rate at 16 kilobits was measured by recording the count in 10-second periods. Usually five of these 10-second error counts were made in each mode. At 8 kilobits the bit error rate was recorded in a manner that provided an estimate of block throughput. This was done by reading the error count in 1-second counting periods. Normally a total of 100 1-second counts was observed and all nonzero counts were recorded. With this set of measurements, the overall bit error rate as well as the block error rate (for 8000 bit blocks) could be calculated from the same data.

#### **2.4.3.2    Signal-to-Noise Ratio**

Several different measures of line signal-to-noise ratio were made. The first was on the modem line signal in which the receive level and the idle noise measurements were recorded and their ratio calculated to provide the signal-to-noise ratio. The noise with tone was measured by transmitting a 1 kHz tone and recording the signal level. The noise level was measured with the tone notched out.

#### **2.4.3.3    Phase Jitter**

The phase jitter was measured with the Halcyon by transmitting a 1 kHz tone and phase locking a second 1 kHz signal to the receive signal at the receiver. The phase detector output is filtered to produce the spectral components from 20 Hz to 300 Hz and this value displayed on the Halcyon's digital display. In addition this

phase detector output was brought out to an external connection so that it could be displayed and photographed on the low frequency spectrum analyzer. A calibration of this setup was performed by providing a known amount of phase jitter to the system (using an Axel line simulator).

#### 2.4.3.4     Amplitude Response and Envelope Delay

These measurements are performed in the Halcyon by sweeping appropriate signals across the band and displaying the resultant amplitude or envelope delay measurements on a cathode-ray tube (CRT) display. The CRT display was photographed for record purposes.

#### 2.4.3.5     Nonlinear Distortion

Nonlinear distortion is measured in the Halcyon by transmitting two pairs of test tones, one centered at 860 Hz (Frequency A) and the second centered at 1,380 Hz (Frequency B), with a total power equal to the data level. The second order distortion products are measured by observing the power in the two bands of B + A and B - A. The third order distortion products are measured by observing the power at the frequency 2B - A. As a test for the effect of noise on these readings the B tone pair is removed and the power of the A tone pair is increased by 3 dB. An additional set of second and third order harmonic product readings are made and a correction factor is applied to minimize the effect of signal-to-noise ratio on the measured nonlinear distortion.

This nonlinear distortion measurement technique is an industry standard, and is felt to give a more representative measurement than total harmonic distortion of a single tone.

#### 2.4.3.6 Transient Measurements

The Halcyon performs transient measurements by transmitting a 1 kHz tone at the data level. Simultaneous measurement of gain hits, phase hits, impulse noise above three thresholds, and dropouts are performed. Gain and phase "hits" are "rapid" gain or phase changes which last 4 milliseconds or longer. The impulse noise counter is inhibited when a gain or phase hit occurs. A dropout is defined as a reduction of 12 dB or more in level, lasting for longer than 4 milliseconds. All other counters are inhibited when a dropout is detected. The normal thresholds utilized for these transient measurements were  $\pm 3$  dB for the gain hit threshold,  $20^\circ$  for the phase hit threshold and 59 dBRNO for the "O" impulse threshold. The other two impulse noise thresholds were 4 dB and 8 dB respectively above the reference setting. The transient counters are capable of counting at rates of up to seven events per second. The transient measurements were counted over a 5-minute period.

Comparison of Modes

One of the major objectives of the test program was to evaluate several modes of the modem on the actual networks to establish the optimum mode for operational purposes if satisfactory performance was achieved. Paragraph 3.3 discusses some of the process which led to the selection of the four modes that were tested. Paragraph 3.4 describes the four modes. In this section the comparative results obtained from the modes are presented. The modes are designated as 16-110, 16-130, 16-111, and 16-C. The first two modes (16-110 and 16-130) represent hardware of the same complexity as that involved in the original breadboard. The last two modes would require slightly less hardware to implement.

Figures 2.5-1 through 2.5-9 present the 16 kb BER performance of the four modes in the nine different categories of calls presented in Paragraph 2.2.1. In all cases, anomalous error counts have been disregarded in calculating the error rate. Mode 16-110 (the normal mode) was used for all of the curves in Paragraph 2.2.1.

With the exception of the European IST loops the BER performance can be seen to be very similar for all four modes. Actually the largest performance difference noted between modes was in the area of sync misses. On some channels where very poor 16 kb error rate existed, mode 16-C could not achieve sync although 16-110 and 16-130 provided reliable sync. As a whole it was felt that 16-110 did provide the best overall performance although all modes were acceptable.

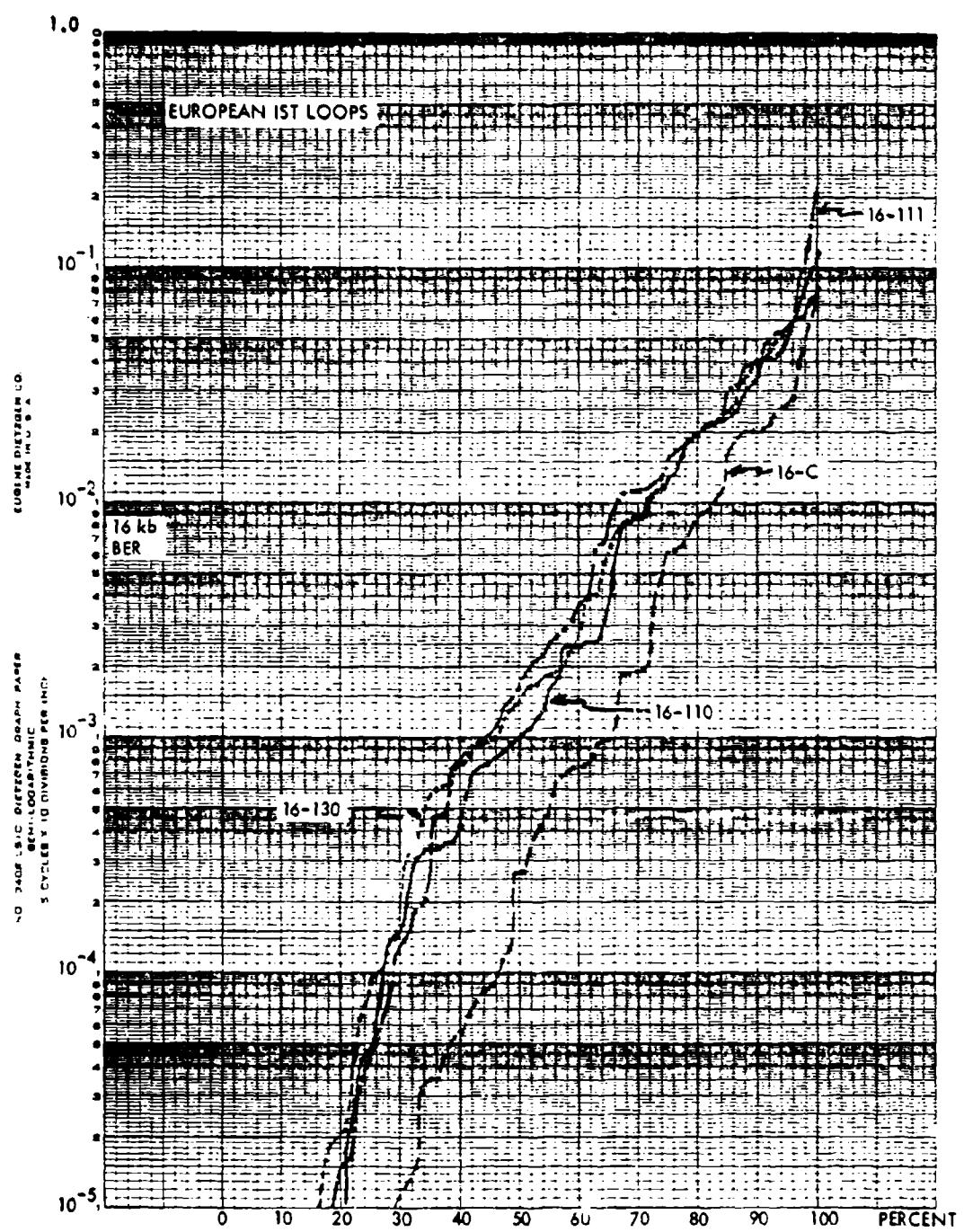


Figure 2.5-1

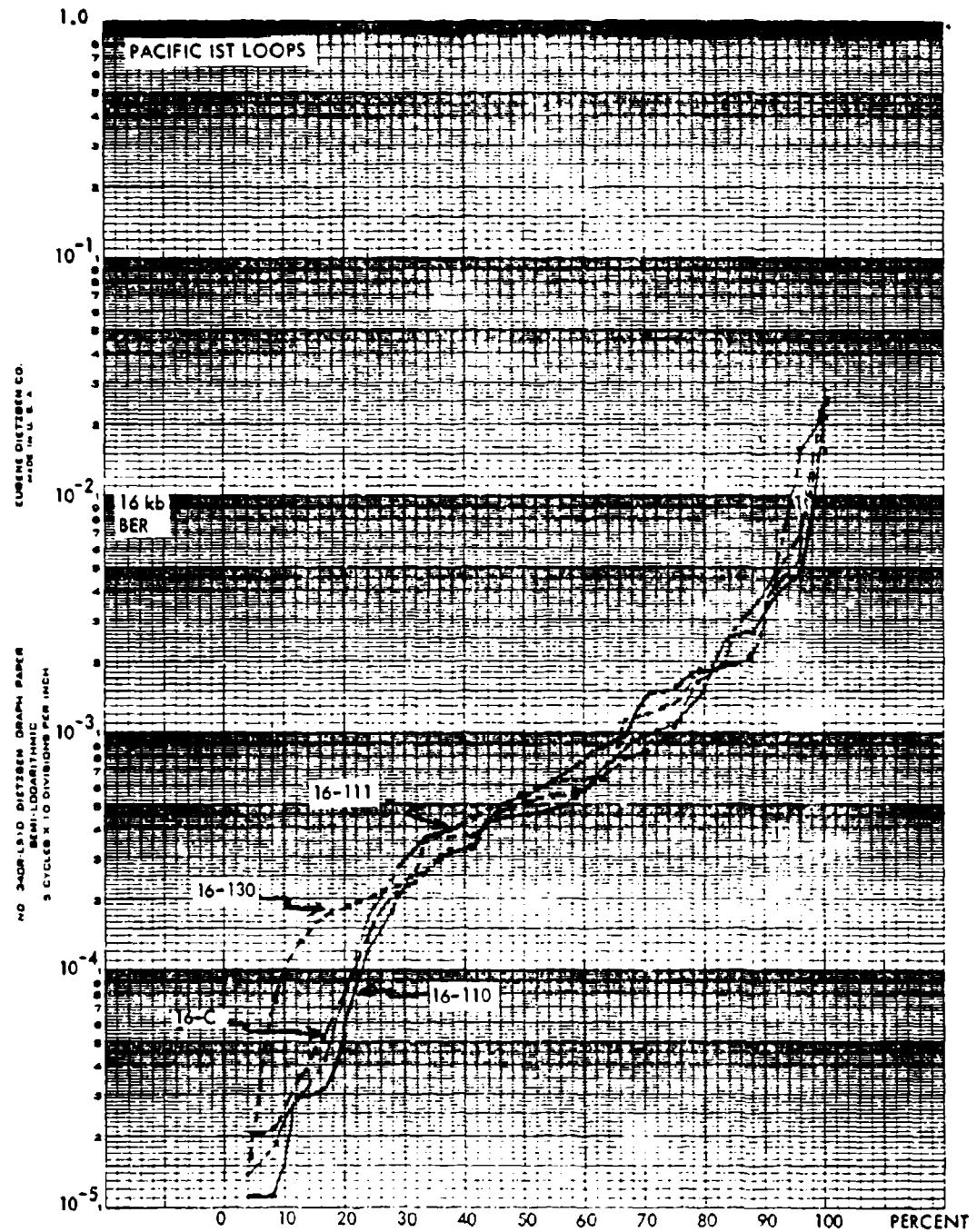


Figure 2.5-2

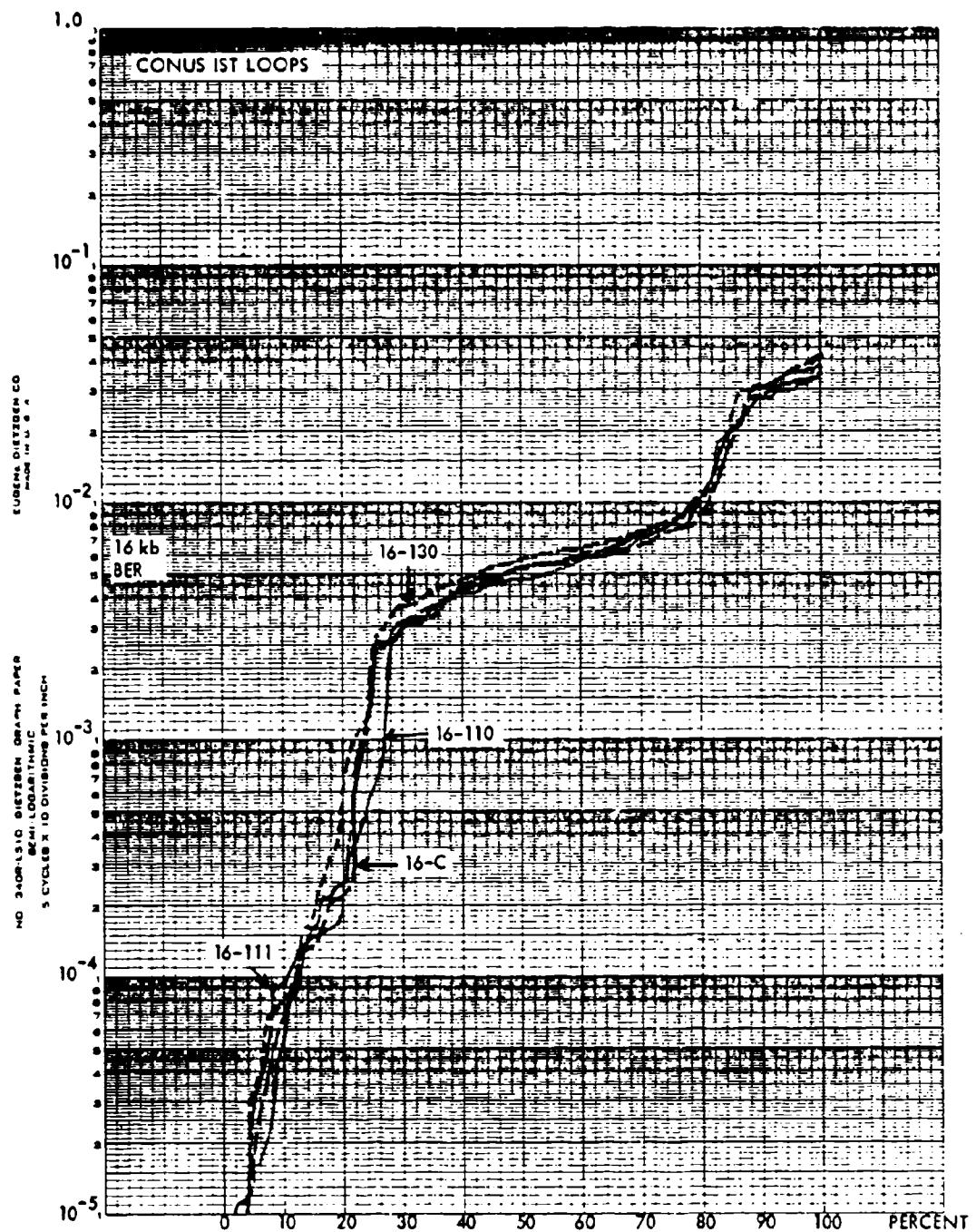


Figure 2.5-3

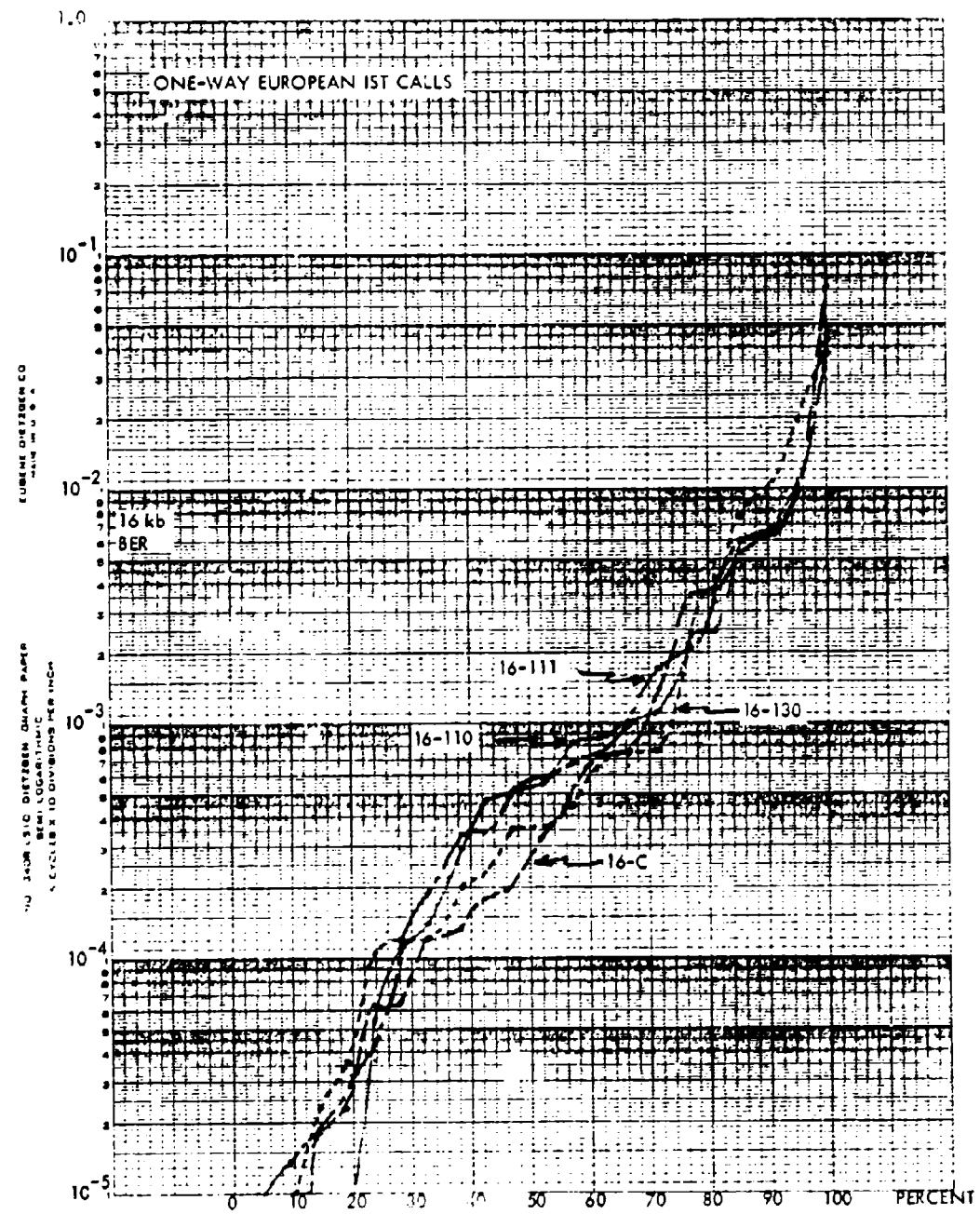


Figure 2.5-4

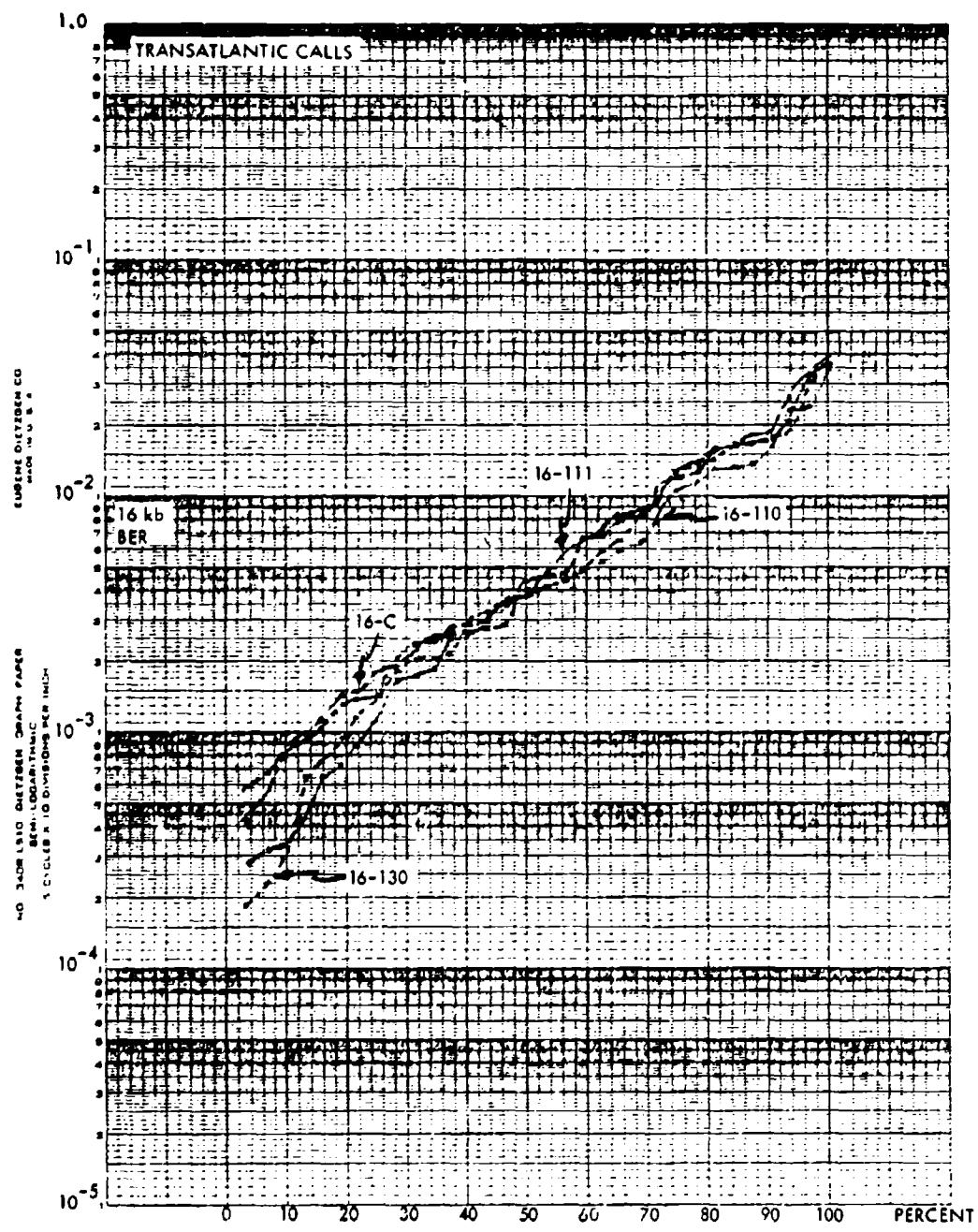


Figure 2.5-5

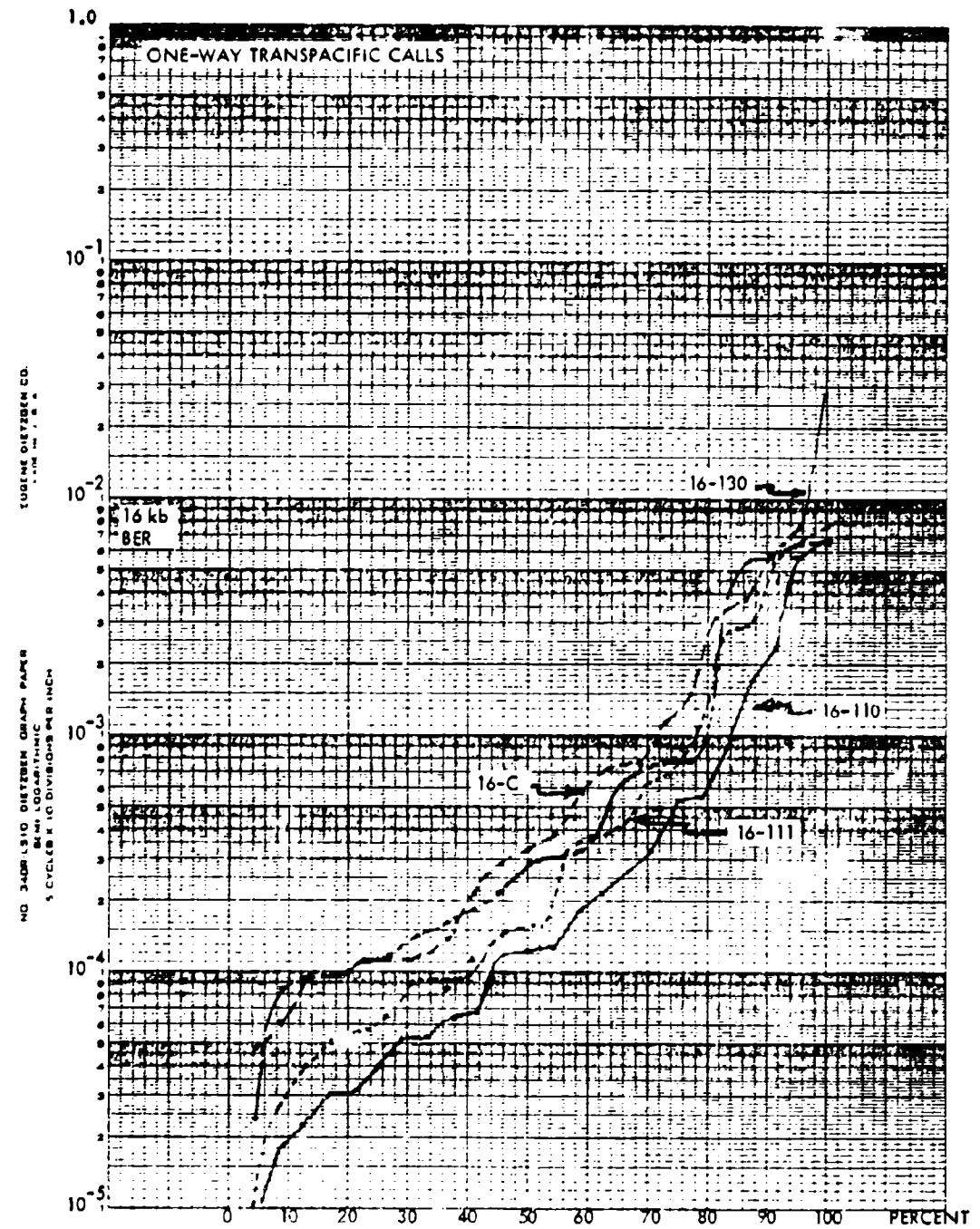


Figure 2.5-6

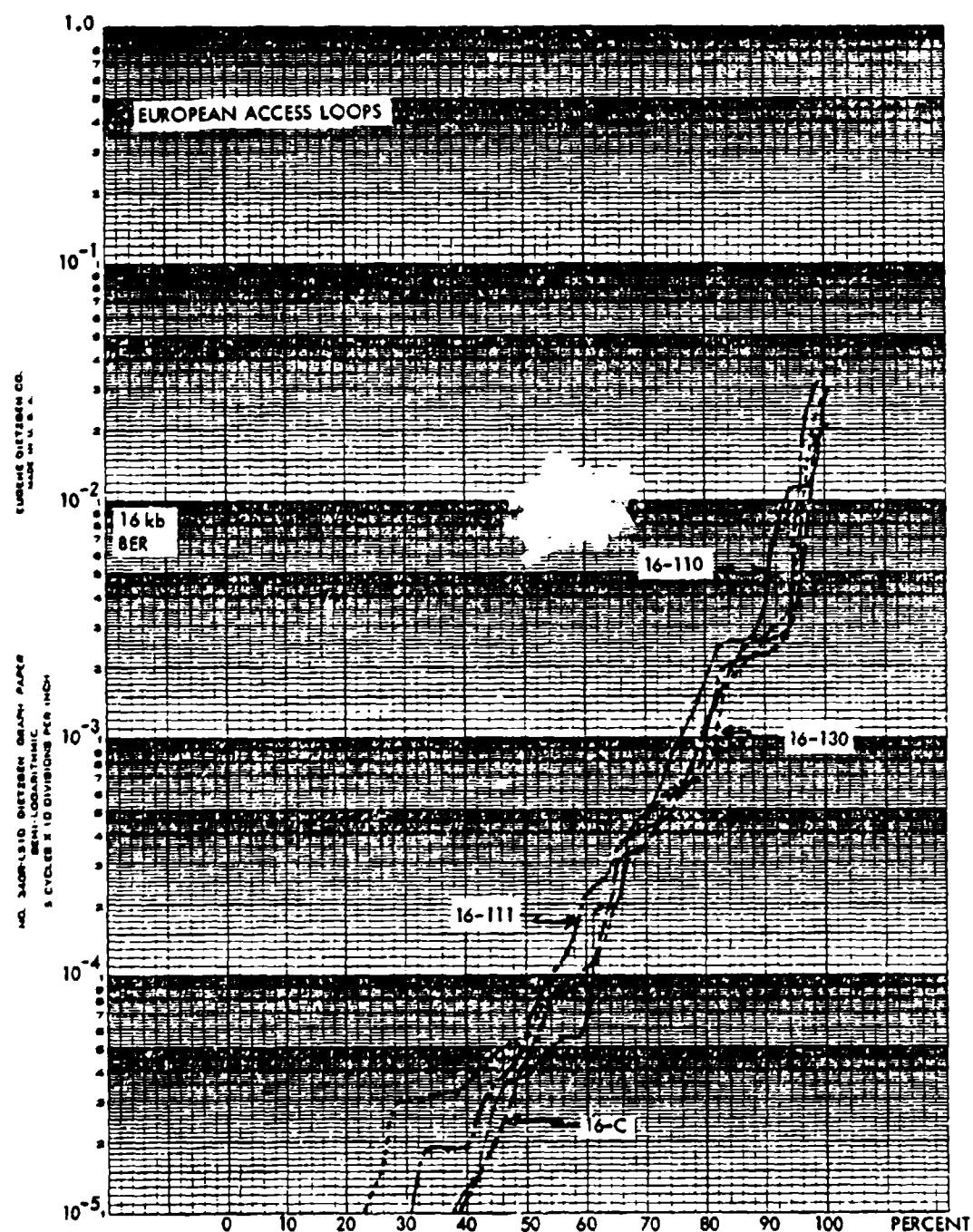


Figure 2.5-7

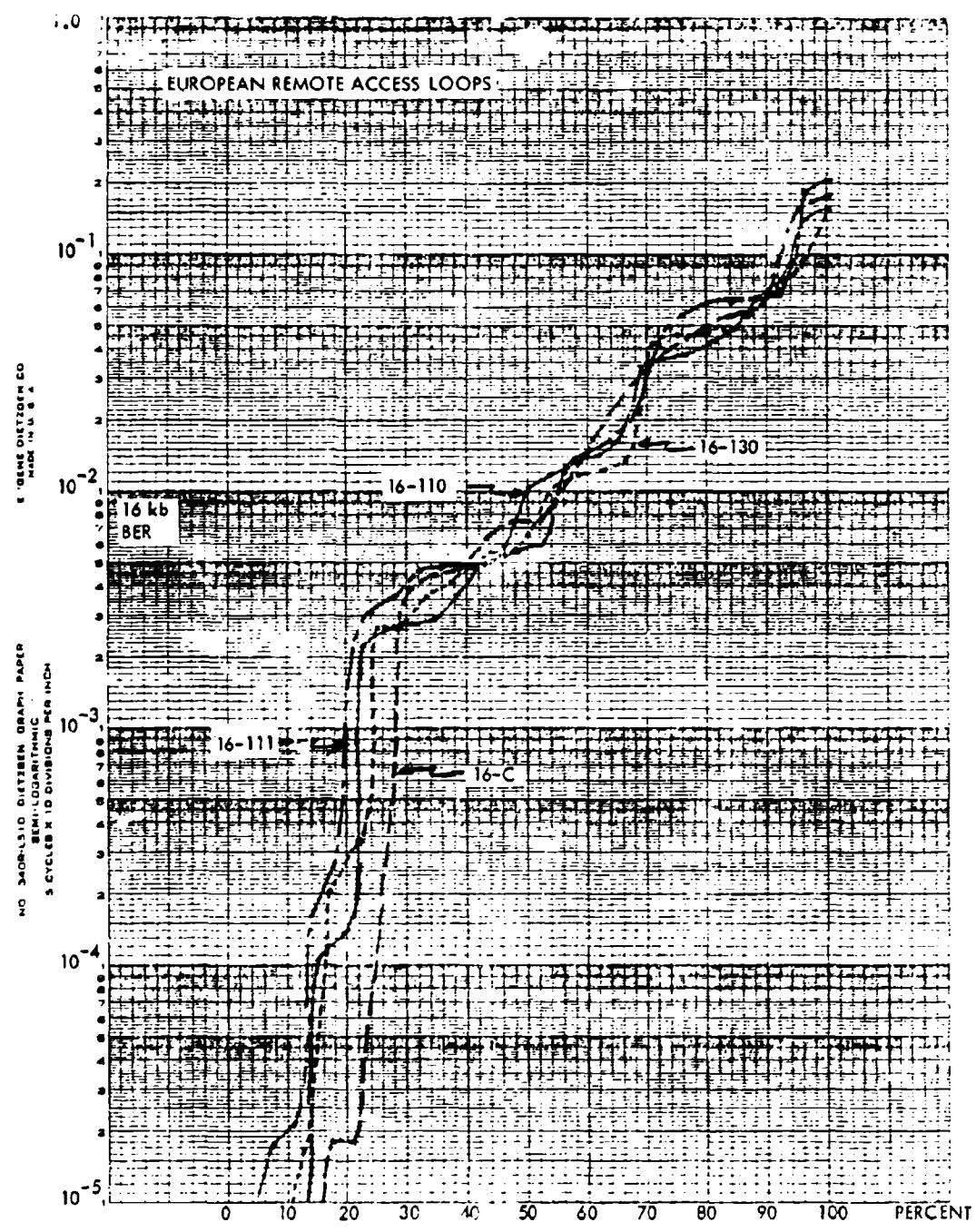


Figure 2.5-8

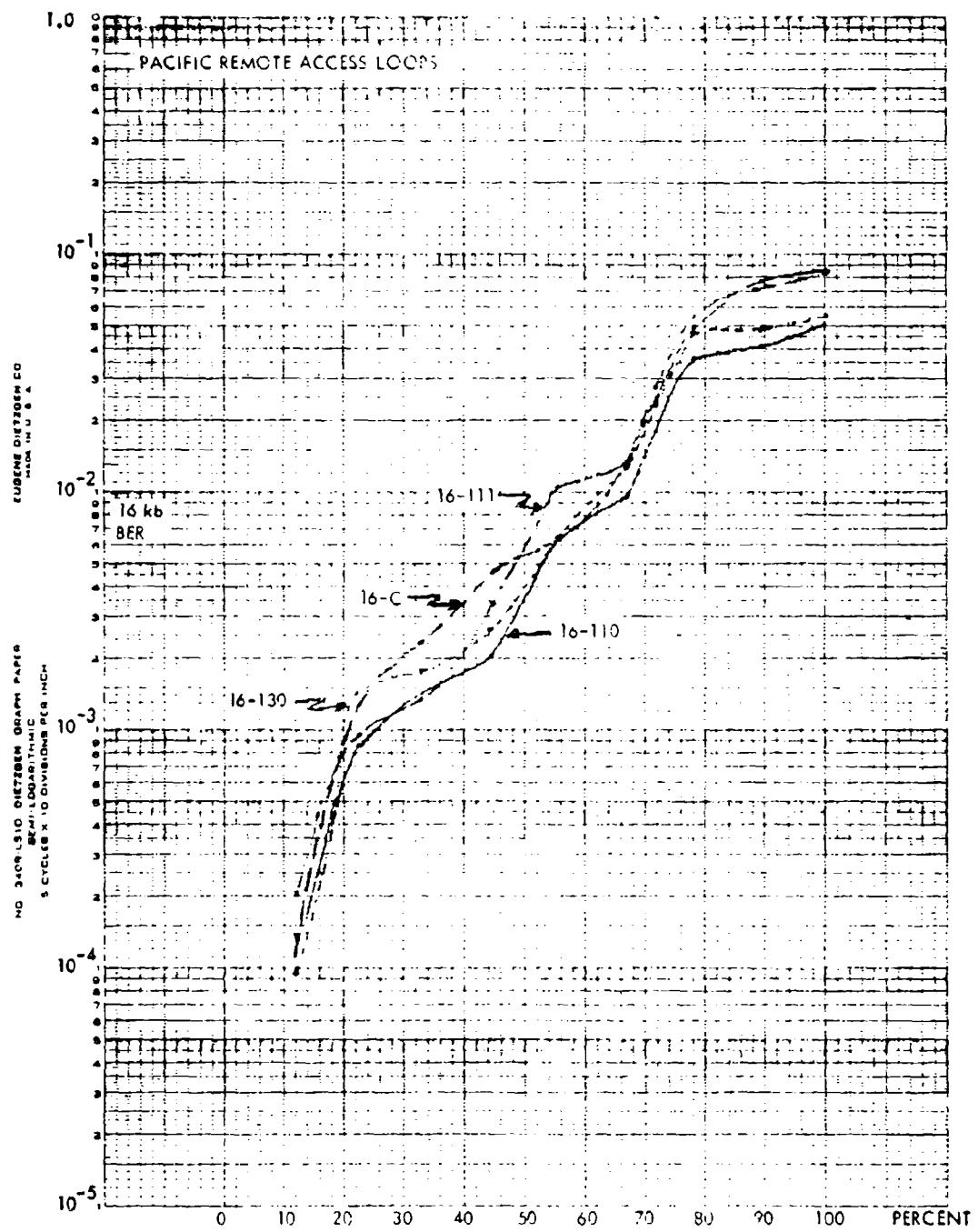


Figure 2.5-9

### 3.0 MODEM MODIFICATIONS

This section describes a set of modem hardware and firmware modifications made prior to the tests. These modifications were designed to package the Breadboard for the rigors of travel and field testing, and to improve performance in certain areas identified by previous tests.

#### 3.1 Repackaging

Prior to European testing, the modem and modem transmitter were repackaged to permit the equipment to be easily and reliably transported as well as set up and operated with a minimum of effort. The basic modem was encased in a 7 by 19 by 30.5 (H X W X D) inch chassis. The modem processor along with the power supplies for both the modem and processor were encased in a 7 by 19 by 16 inch chassis. The separate transmitter and its power supply was encased in a 7 by 19 by 16 inch chassis. All controls and input/output connections necessary for operational testing were installed on the front panels of the units. Blowers were installed in each of the three units to provide adequate cooling. The repackaging effort resulted in a complete modem (receiver, transmitter, processor) being housed in two chassis. The separate transmitter was encased in one self-contained unit. After repackaging, the units were tested to ensure that the overall performance had not been adversely affected by the change in mechanical configuration.

#### 3.2 Look-Up Table Investigation

In the original study program a technique for combating memoryful nonlinearities was devised which employed a memory which was trained to provide appropriate corrections for each transmitted pattern. A detailed description of this approach is given in the Bibliography Reference 1, and will not be repeated here. Although computer predictions for this technique indicated a noticeable improvement in performance for this approach when nonlinearities were present in the channel, the actual

equipment had produced no gain in performance when the look-up table was employed. It was an objective of this program to investigate this discrepancy and determine whether the look-up table approach could be modified to provide a performance advantage prior to the European testing.

Analysis of the difference between the assumptions present in the computer prediction and the actual hardware operation indicated that the likely problem was that the look-up table in the hardware used actual symbol decisions to provide the address while training, whereas the computer analysis had presumed perfect decisions. Since the bulk of the errors in channels with nonlinearity problems are irreducible errors it can be deduced that the table could not be expected to train properly when operating upon decisions rather than the actual transmitted signal as the basis for the table address. Consequently, the modem was modified to allow look-up table training during the normal training mode and an ideal reference, available in the hardware, was supplied to the processor so that it could be used as a basis for the address.

No perceptible performance improvement was noted in this case even when extended periods of time (30 minutes) were used to train the look-up table. Close examination of the received data (on an oscilloscope) during the training mode indicated that the errors for a fixed pattern had very little bias relative to their variance even when nonlinearity was the only disturbance present on the simulator. Thus, it appeared that the favorable predictions predicted by the computer model were due to a difference in the exact modeling and were not available to the hardware. Hence the look-up table approach was dropped. None of the tests reported in this document employed the look-up table.

### 3.3 Other Processor Modifications

Several other modifications to the processor were incorporated in the modem between the initial contract and the test results reported in this document.

During the initial study effort eight phase measurements were used in the phase-tracking algorithm. Although the computer prediction indicated that this was the best choice, this prediction was based upon a model of phase jitter that was felt to be questionable. Hence an attempt was made to provide the processor with the capability of switching manually between eight and four phase measurements. Time, however, did not allow completion of this activity prior to completion of the initial contract. This effort was completed prior to the testing reported herein and accounts for two of the modes that were tested as is discussed in Paragraph 3.5.

Although the phase tracking algorithm had worked quite adequately in the tests conducted at the end of the initial contract, it was anticipated that the phase jitter present in the European tests would be more severe than that existing on the CONUS lines. Specifically it was anticipated that lines with a large amount of low frequency jitter might be present. In this case the differential nature of the data would make the bit error-rate insensitive to this jitter. However, the initial equalizer training might be affected since the phase tracking loop used during equalization is very slow and would likely not be able to track this jitter. Simulation in the laboratory of large quantities of low frequency jitter indicated that this might be a problem.

Several approaches to using the processor to supply the equalization error signals during training were investigated. None of them solved the problem completely but the best approach located was one which switched modes half way through the eight frames of equalizer training. The training mode for the first four frames was that previously used except that the phase loop external to the processor to track the incoming signal phase was disconnected. At the end of four frames the phase loop was switched to utilize the X-Y reference algorithm in the processor as the basis for the equalizer error signal. The switching between modes was set up to be accomplished manually from a front panel sense switch since the modification required in the processor to automate this activity was too extensive to be done prior to the European tests. This switched mode

was one of the four tested.

Since modes which did not employ the external phase tracking loop could potentially reduce the amount of hardware, a switch was incorporated to allow disabling of this loop. The fourth mode tested was one in which all of the operations were the same as that developed in the previous program except that the external phase loop was disconnected.

### 3.4 Training Sequence Modifications

The receiver training sequence was modified to increase synchronization reliability. It was observed during line tests that the receiver would occasionally fail to recognize the sync pattern in the eight-frame training sequence. This caused the receiver to prematurely terminate the training sequence, resulting in the inability to pass data. The first sync, however, was detected whenever the receiver recognized the carrier burst at the beginning of the training sequence. Therefore, a means to prevent the synchronization logic from missing intermediate sync patterns was needed.

The present configuration of the synchronization logic contains circuitry which prevents the receiver from prematurely terminating the training sequence. This modification is implemented by the addition of a frame counter to the synchronization logic. The frame counter is initialized by the recognition of the first sync pattern. The frame length timer outputs a carry pulse to the frame counter at the end of each received frame of sync and training. After seven frames have been received, the frame counter releases the end of sync detect circuit. This enables the end of sync detect circuit to sense the absence of sync at the end of the eighth frame. The receiver then goes through the original freeze-weight and data modes. The modified synchronization logic will still permit training sequences longer than eight frames. When the receiver is in the continuous sync and training mode, the end of sync detect circuit is disabled. When the receiver is switched back to the normal mode, the end of sync detect circuit is reenabled after seven frame times. A modified block-diagram is shown in Figure 3.4.

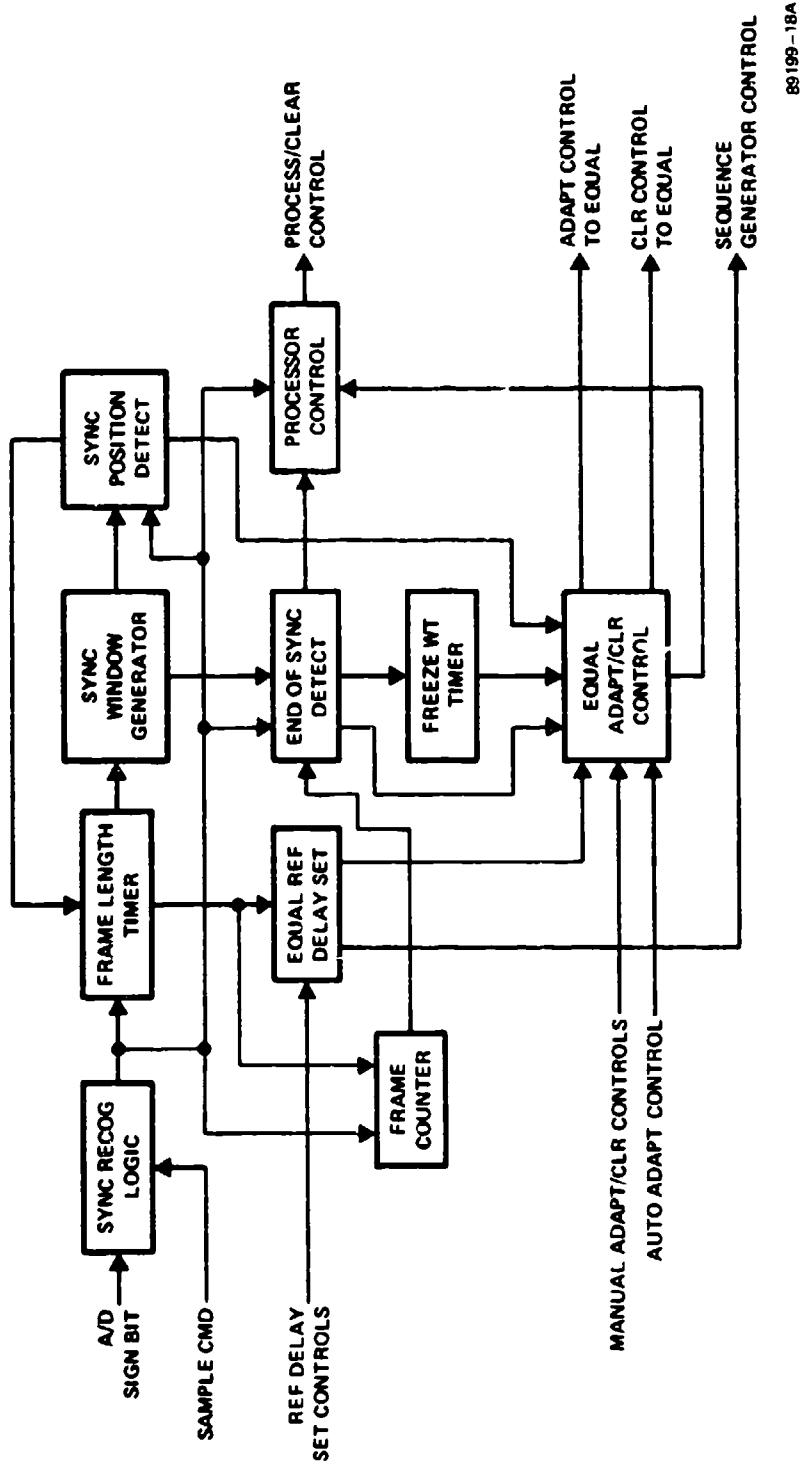


Figure 3.4. Modified Synchronization Logic.

### 3.5 Description of Modes

The four modes tested on the AUTOVON network will be briefly described in this section. The basic differences between the modes lies in three areas. These are:

- a. The use of either four or eight samples in the processor phase tracking algorithm during the data operation. This does not affect operation during the normal training operation.
- b. Use of the external phase tracking loop. This applies to both the training and data operations.
- c. Source of the X-Y errors for the equalizer during the training operation selected from the normal subtraction of the estimate from the reference or whether they are obtained from the processor algorithm used during data transmission. The four modes tested are shown in Table 3.5 along with the configuration in these three respects.

Table 3.5. Mode Configurations

<u>Mode</u>	<u>8 or 4 Samples</u>	<u>External Phase Loop</u>	<u>Source of X-Y Error for Equalizer During Training</u>
16-110	8	Connected	Normal Subtraction
16-130	4	Connected	Normal Subtraction
16-111	8	Disconnected	Normal Subtraction
16-C	8	Disconnected	Normal Subtraction for First Four Frames Processor Algorithm Last Four Frames

## 4.0 KEY GENERATOR TESTS

This section describes a series of interface tests with the modem and two types of encryption/decryption key generators, TSEC/KG-13 and TSEC/KG-34. The purpose of these tests was to determine at what point key generator synchronization would become a problem. This is an important consideration since the modem is able to synchronize and operate at high bit error rate conditions, and CVSD equipment such as the HY-11 is able to provide intelligible, albeit noisy, speech at high bit error rates. It should be noted that the use of "self synchronizing" key generators, with the attendant error multiplication, would significantly reduce the percentage of lines providing usable voice quality.

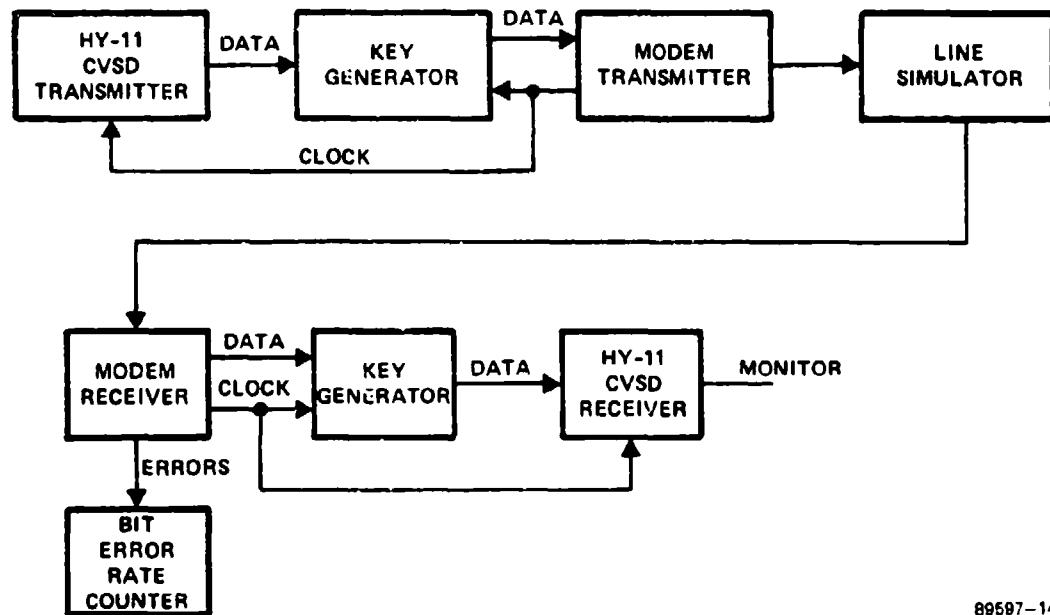
### 4.1 Test Setup

The test setup was as shown in Figure 4.1. The transmit portion of the key generator under test was connected between the HY-11 CVSD transmitter and the modem transmitter data input port. Similarly, the receive port of the key generator was connected between the modem receiver data output port and the HY-11 data input port.

The line simulator signal-to-noise ratio was adjusted to obtain the desired bit error rate from the modem. Then a series of keyer synchronization attempts was made, using the controls on the key generator. Synchronization was verified by monitoring the output of the receive portion of the HY-11. In the absence of synchronization, this output consists of a high level noise. Normally, 20 synchronization attempts were made at each bit error rate.

### 4.2 Results

The results for the KG-13 are shown in Figure 4.2-1, in the form of curves of sync probability vs bit error rate. The "modes" (4,8,16,32) have to do with the length of synchronization pattern employed by the key generators. The numerically



89597-14

Figure 4.1. Key Generator Test Setup

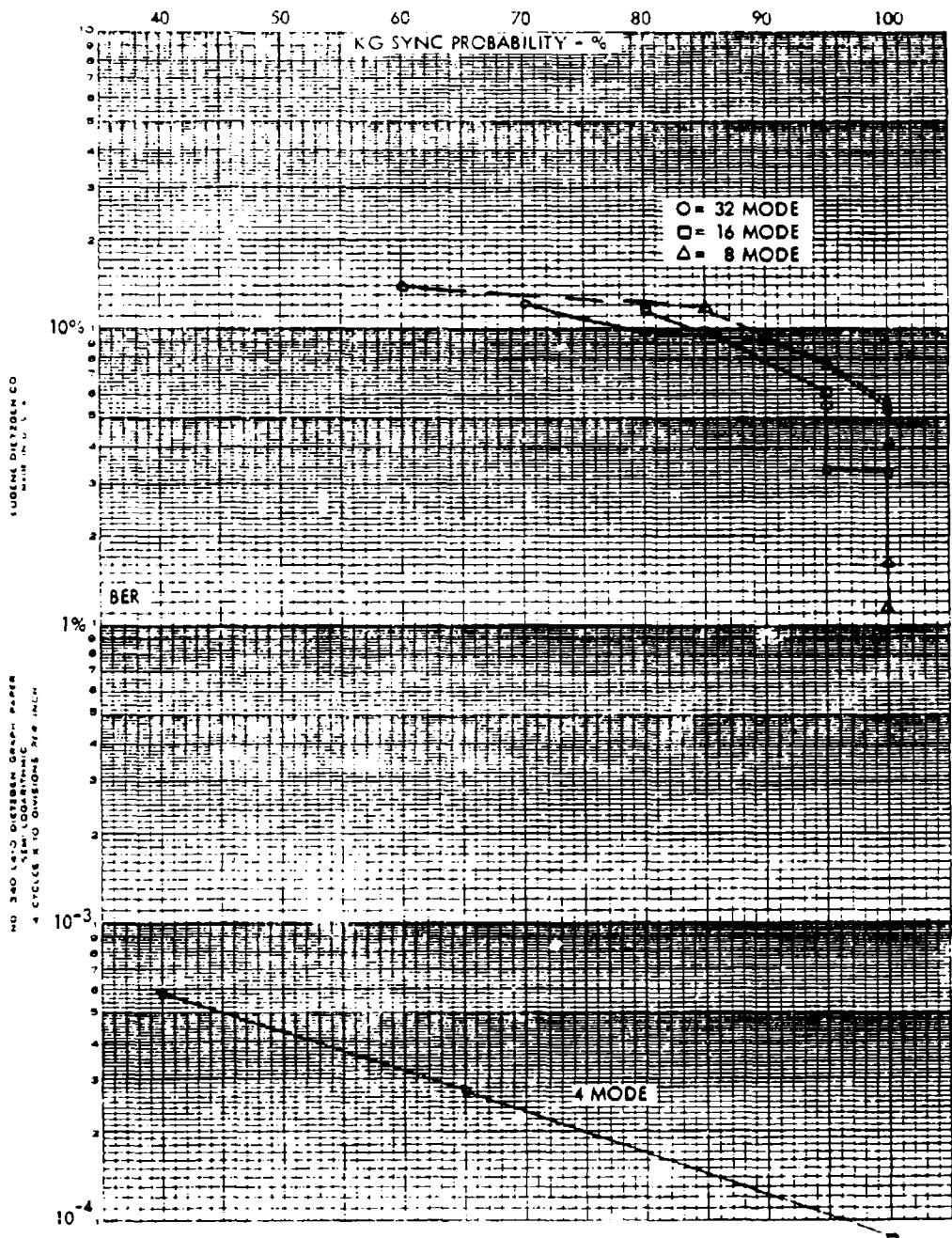


Figure 4.2-i. Sync Probability Versus Bit Error Rate KG-13

larger modes require longer synchronization time, but at 16 kb/s the longest sync time is less than 1 second, and is not significant relative to modem training time. As seen in the figure, all modes but "4" are similar in performance and provide 90 percent sync probability with bit error rates up to 8 or 10 percent. This is a virtually unusable bit error rate for CVSD voice, so the KG-13 would not limit system performance if the "4" mode was avoided.

The results for the KG-34 are shown in Figure 4.2-2. The performance is similar or slightly better, so the same conclusion would hold.

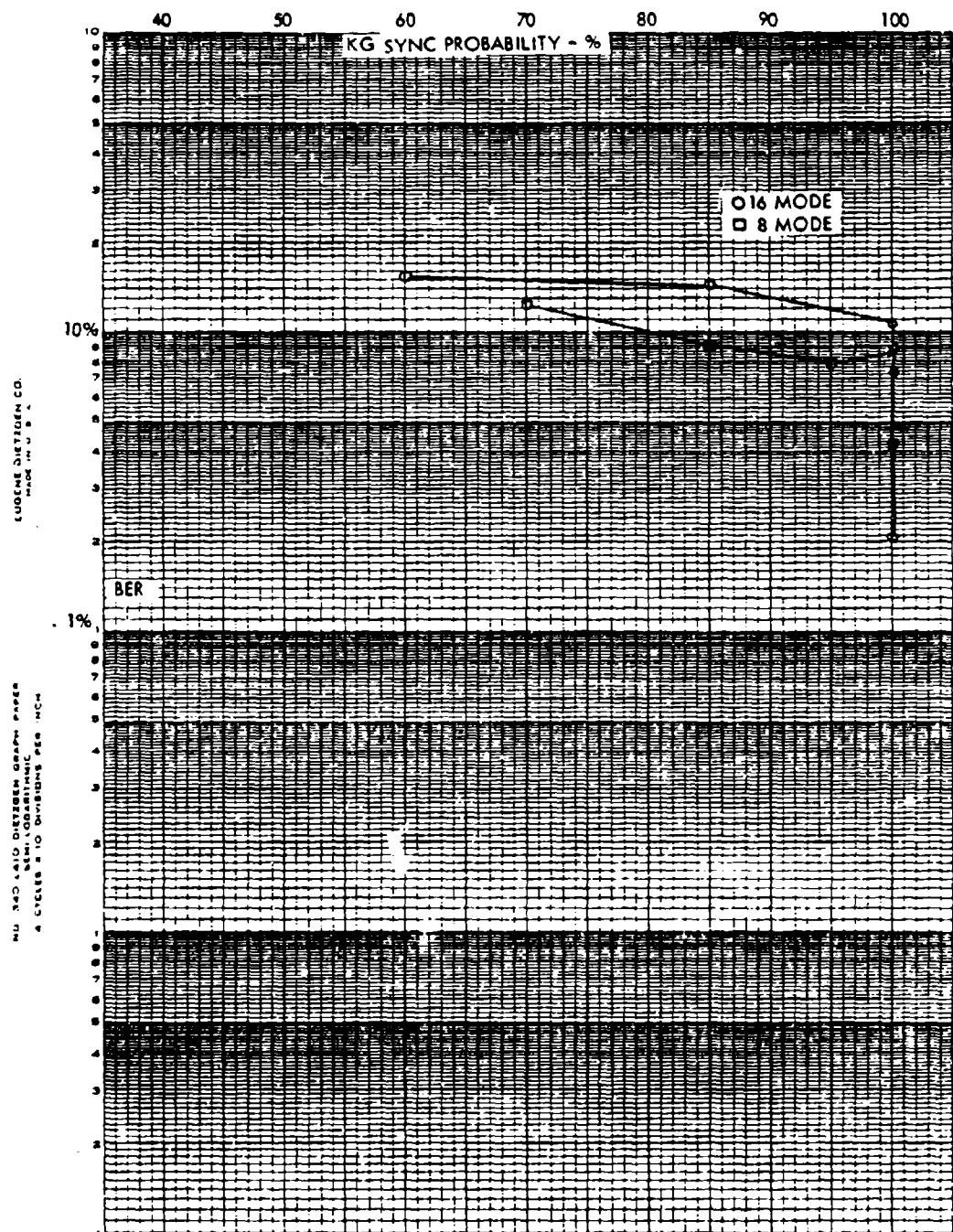


Figure 4.2-2. Sync Probability Versus Bit Error Rate KG-34

## 5.0

## CONCLUSIONS AND RECOMMENDATIONS

The following conclusions can be drawn from the results of the efforts described in this report:

- a. The design of the 16 kb modem is sufficient to provide for adequate voice quality over the existing AUTOVON network in any of the uses envisioned presented in Section 2.0 of this report.
- b. Digitization of segments of the network are not likely to degrade the voice service supplied.
- c. All four modem modes tested provide good performance. Mode 16-110 provided slightly better results than the other three.
- d. The only type of line disturbances observed in the testing which caused significant performance disturbances were fades of tropo links (predominantly in Europe) and harmonic distortion (in CONUS).

The following recommendations are made:

- a. Research, development, test, and evaluation units should be procured.
- b. These units should be tested in an operational configuration associated with AUTOSEVOCOM switches to provide service similar to that presently available with the 9.6 kb/s modem.
- c. Further investigation should take place to determine modem algorithms which would improve performance in the presence of fades and harmonic distortion.
- d. The use of D conditioned lines should be considered in cases where access lines have severe harmonic distortion.
- e. Line models for the European network should include the effect of fades.

## APPENDIX A

### NETWORK DESCRIPTION

#### A.0      General

A good deal of effort was expended during the initial phases of the program to understand the AUTOVON network as it presently exists as well as its anticipated configuration after the planned conversion to digital traffic. It was felt that an understanding of these facts would allow a better test plan to be created and would result in a better interpretation of the test results. This appendix presents a brief description of the "picture" of the network which was obtained from these efforts. The principal documents used in this effort are listed in the Bibliography References 2-11.

Reference 12 was used to verify CCSD numbers in connection with circuits tested.

It should be emphasized that it is not the intent of this appendix to present the reader with a complete description of the AUTOVON network. Rather it is intended to present the aspects of the network that appeared to be significant relative to the 16 kb modem test program and its potential use in the future network.

A number of the documents used to extract the detailed data on the European and Pacific networks were not consistent in all matters. This is undoubtedly due, at least in part, to the dynamic nature of the network. Hence data presented relating to quantities of circuits of different categories should be taken as approximately correct for the time period of the test, and not as an exact indication of the network at the time this report is being read.

This appendix first presents an overall discussion of the world-wide AUTOVON network, the plans for change, and roles that the 16 kb modem might play in the future network. This is presented in Paragraph A.1. Paragraph A.2 provides detailed data on the European network which was used to determine the network coverage. Paragraph A.3 presents similar data for the Pacific AUTOVON network.

## A.1

The World-Wide AUTOVON Network

The present network can be thought of as a composite of four different telephone networks. These are the networks in Europe, Asia, the Caribbean and the Continental U.S. Each of the three overseas networks are connected to the CONUS network through trunks between gateway switches. Within a particular network there are a number of AUTOVON switches (10 in Europe, five in Asia, one in the Caribbean and 70 in the CONUS). A connection between these switches will be referred to in this document as an IST. These switches serve a large number of subscribers who are connected to the AUTOVON switches by access lines. Many of the AUTOVON subscriber lines go to a secondary switch (PBX) located at a particular military installation. Thus, individual telephone subscribers at a base are tied into the PBX and can dial an AUTOVON switch through the PBX. In addition to the PBX access lines there are a number of access lines which go directly to a subscriber. These lines generally share the transmission facilities that are used to provide PBX access lines to the location of the subscriber, but these access lines are not switched by the PBX. The access lines presently used for AUTOSEVOCOM are of this nature.

All of the IST and access lines are four wire circuits. It appears that most of the subscriber lines off PBX switches are two wire connections since most PBX switches are two wire switches. Thus, the conversion between four and two wire circuits normally takes place on the AUTOVON side of the PBX switch.

The circuits are conditioned as voice grade (V1 and V2) or data grade (S3) circuits. The IST's contain circuits of both categories which are selected by the switch based upon a dialed prefix to the number. A data grade prefix will cause the switch to select a data grade circuit or provide a busy signal. A voice grade prefix (no prefix) will cause the switch to first search the voice grade circuits and if the voice grade

circuits are busy, the switch may select a data grade line. In Europe all of the AUTOVON access lines are data grade and most, if not all of the PBX access lines are voice grade.

At present the 2.4 kb AUTOSEVOCOM signals are passed through regenerators at each gateway switch when the signals are to be sent from one of the four networks to another of the four networks. The regenerators convert the analog signal to a bit stream which is then used to produce a new analog signal. Consequentially, final bit error rate is the sum of the bit error rates obtained in each of the segments. This provides less overall degradation than that which would occur if the signal were not regenerated. In addition the crypto key is changed at the CONUS gateway locations which would necessitate the regeneration even if the signal degradation would not. The exact configuration of the 9.6 kb AUTOSEVOCOM signals was not determined with certainty. At present there are relatively few 9.6 kb modems in use.

The present network is almost exclusively an analog network. In Europe the only digital links are those that were installed in the "FKV" project which provide digitized trunks between Hiedelburg, Vaihingen, Swetzengen, Koenigstuhl, and Stuttgart. No IST circuits transit these trunks at present; and since none of these locations are AUTOVON switches, no access lines use exclusively digital trunks. The conversion of the European network planned in the DEB Phase I project will tie the FKV trunks into trunks coming from Coltano, an AUTOVON switch, and hence will result in a number of IST's which will transit the digital segment. However, since a second switch is not involved, all IST circuits will still transit portions of analog trunks. Later phases of DEB will extend the digital network to England and result in a large number of IST circuits and access lines which transit the digital trunks. The present projections for the time frame of DEB Phase I would provide completion in the next few years. The succeeding phases of DEB will be implemented in the 1980's.

It should be noted that the plans, of necessity, involve digitization of the transmission facilities first, followed by installation of digital switches. No end-to-end digital service can be provided until digital switches are installed. Even then end-to-

end digital service will be available only when all switches and transmission links between the subscribers involved are digitized. This also needs to include all routings between these subscribers since means of obtaining alternate routing must be preserved. It would appear that the time frame associated with providing this type of service throughout the network is quite long although some subscribers may have this service in the reasonably near future.

The plans associated with AUTOSEVOCOM II are consistent with interfacing the digital network with secure digital signals. Again, however, the subscriber locations with this service available will be limited to those which can be connected by completely digital AUTOVON service.

Unquestionably, the conversion of a vast operational network such as the AUTOVON network in a manner that does not disrupt service during the conversion will be a complex and lengthy process. Therefore, interim measures aimed at either upgrading the secure voice quality during the conversion or easing the task of conversion should be considered as potential roles of a 16 kb/s modem. Permanent roles in cases where conversion is not possible, or where the cost of digitization is too great, should also be considered.

Three general categories of usage appear consistent with the existing network and the plans for conversion. These are:

- a. Upgrading the voice quality compared to that presently available from the existing 2.4 kb/s vocoders and the 9.6 kb/s CVSD units in present use in the AUTOSEVOCOM network. This implies that the modem signal is treated as analog by all of the switches in the network whether or not specific trunks may have been digitized.

- b. Interfacing subscriber locations which do not have digital service with the digital network. This implies that the modem signal is treated as an analog signal only on the access lines connecting the subscriber to the digital switch, and at that point is converted to a digital signal for transmission over the digital network. This presupposes the existence of digital switches as well as digital trunks.
- c. Handling 16 kb/s digital traffic over interswitch trunks which either cannot be digitized or which will not be digitized in the earlier phases of the digital conversion. Specific examples of this are under-sea cables and other leased Telpak service. However, it would appear that on an interim basis, interswitch trunks requiring tropo hops and commercial satellite links also fall in this category.

#### A.2 The European Network

The 10 AUTOVON switches in the European network are connected by 22 link segments shown in Figure A-1. All of the interswitch traffic transits these links on circuits that may be patched at one of the locations shown. The circles in Figure A-1 indicate switch locations and the squares indicate nonswitch locations where at least one of the interswitch circuits is baseband patched. The segments are generally made up of several transmission links. The link designators are shown on Figure A-1. Segments involving only microwave LOS links are shown as solid and those involving tropo, diffraction or leased circuits are shown as dotted. Ten of the 22 segments require links that are not microwave LOS links. If these segments were taken out of the network, some switches could not be accessed and the flexibility of routing to the switches that can be accessed would be greatly impaired. Consideration of the geography associated with the tropo, diffraction and leased segments leads one to the conclusion that they cannot be reasonably replaced with LOS links. Hence the digitization of the

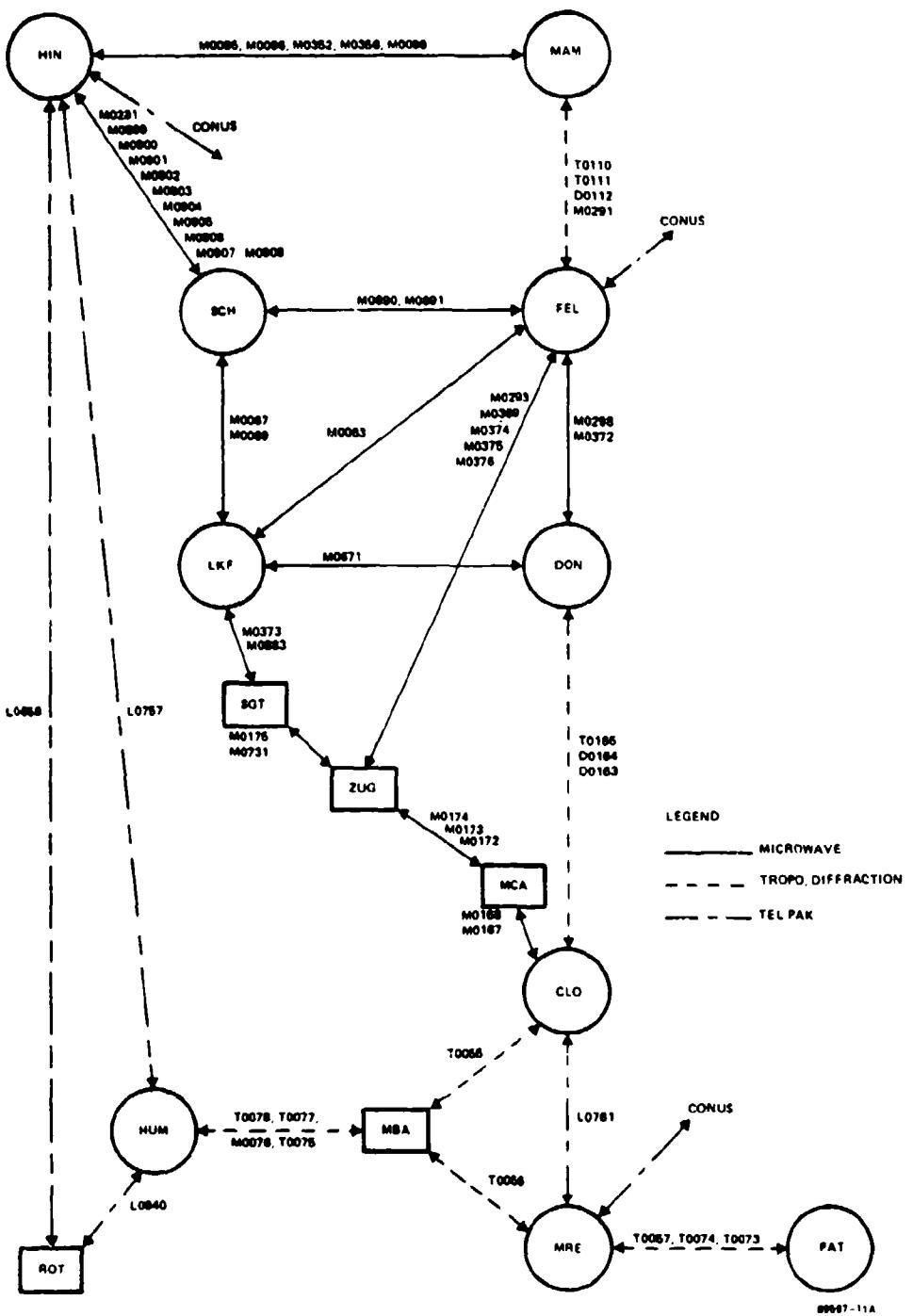
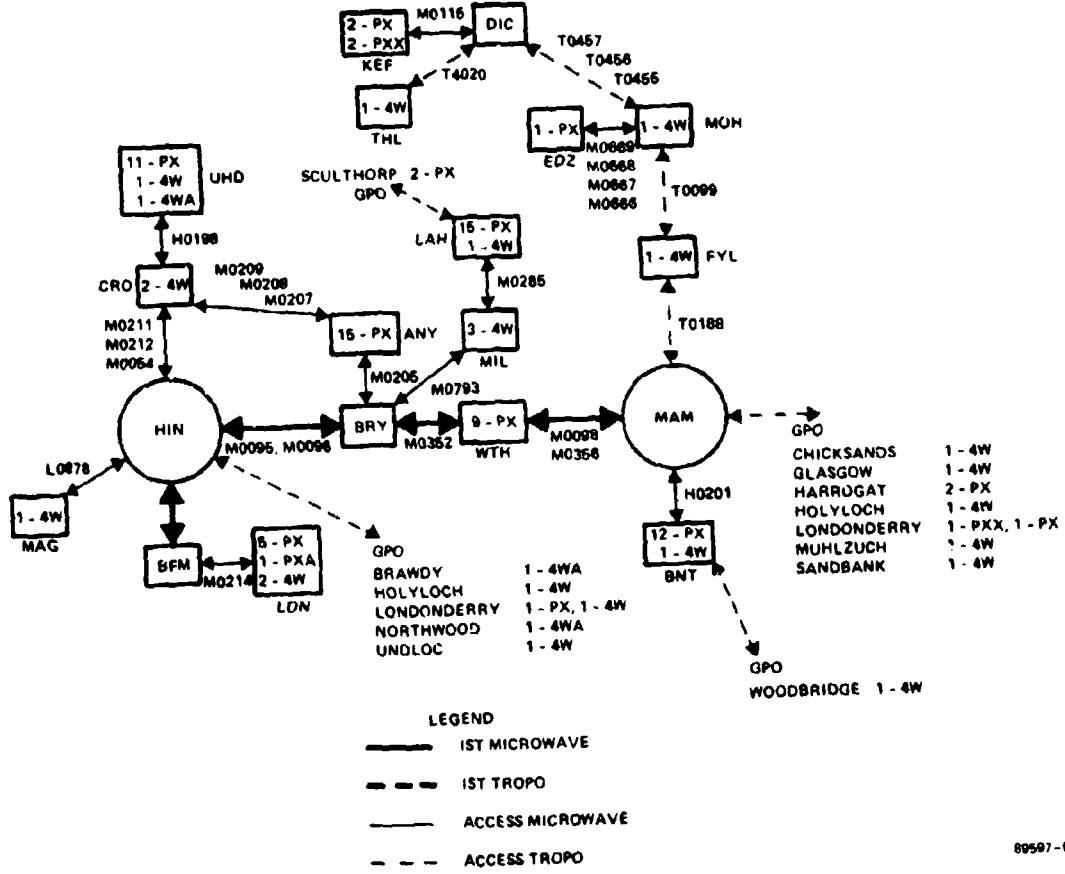


Figure A-1. European IST Network.

network will require some method of handling digital traffic over these links as well as over the LOS links, most of which are planned to be digitized in the DEB program. In all there are 40 microwave LOS links, 11 tropo links, four leased Telpak links and three diffraction links which handle interswitch traffic.

The network handling access line traffic is much more complex than that associated with the interswitch traffic. Figures A-2 through A-11 show the networks connecting each of the 10 switches with their subscriber locations. As before, circles indicate switches and squares indicate either subscriber locations or locations where baseband patches are present. Each of the subscriber locations has an indication of the number and type of subscriber lines coming from that location to the AUTOVON switch in question. The symbol, PX, indicates a PBX line, 4 W a four-wire line not going through a PBX, 4 WA a four-wire secure voice line, and PXA and PXX a line to a secure voice switch. As before the links transited in each segment are shown. The heavy lines, both solid and dotted, indicate IST links which appeared on Figure A-1. Solid lines indicate segments connected by either LOS links or government owned land lines. Dotted segments involve some other form of link. In addition dotted lines go to locations where interface with the public telephone circuits are used to supply subscriber service.

Table A-1 lists the total number of different subscriber locations for each switch and a breakdown as to how they are connected to the switch. The numbers under M indicate the numbers that involve only microwave LOS links. Under T are the numbers involving one or more tropo links. Under D are the number of locations requiring a diffraction link but no tropo hops. Under L are the number of subscriber locations which access the switch through leased Telpak service. The H column shows the number of subscribers involving a VHF or UHF LOS link. The number under PTT shows the number of subscribers using the public telephone services. As can be seen, 221 different routings are involved. Of those, 91 are connected by either LOS or government land line which should be relatively easy to digitize. Sixty-three involve tropo or diffraction links, and 67 involve commercial leased lines of some sort.



**Figure A-2.** Access Network for MAM

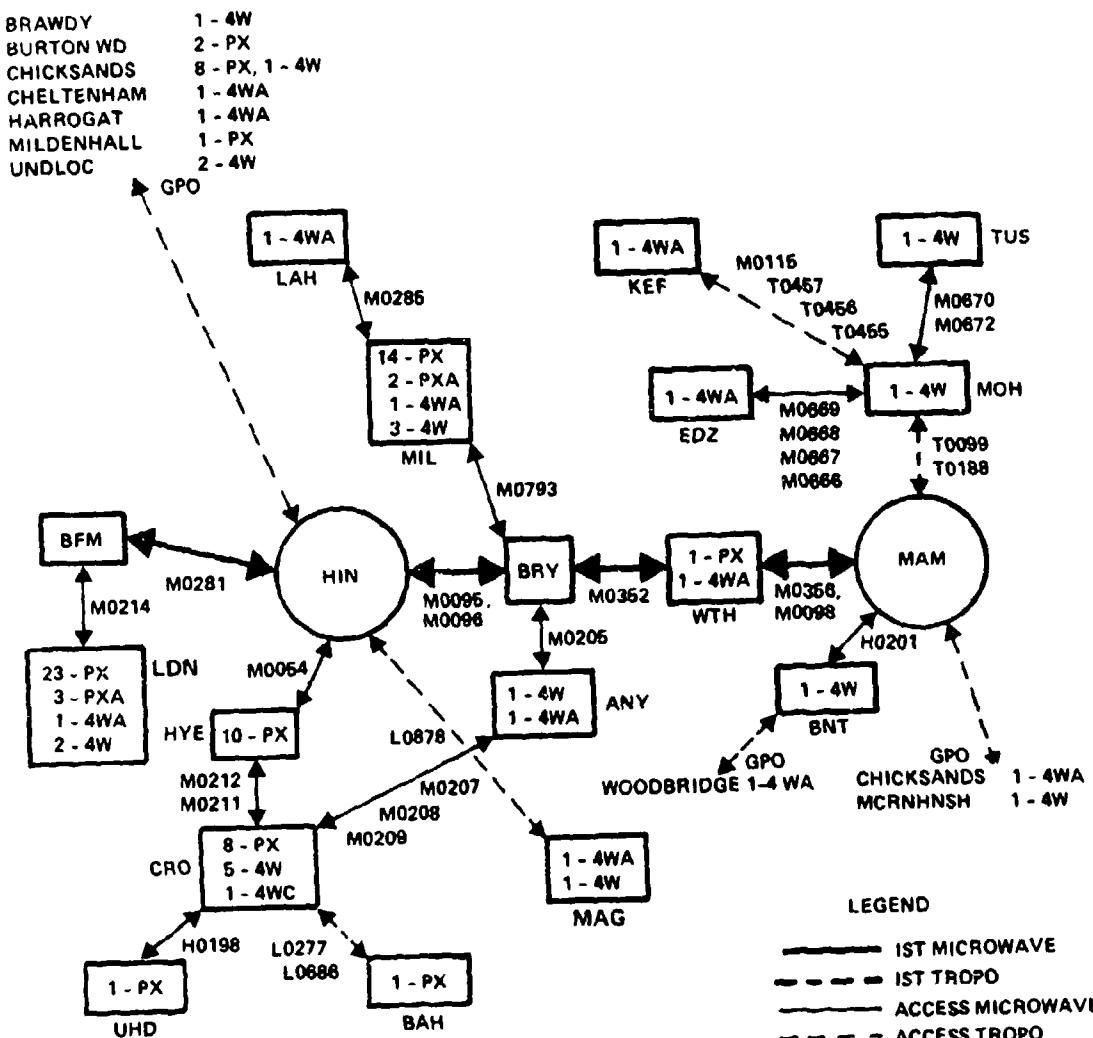
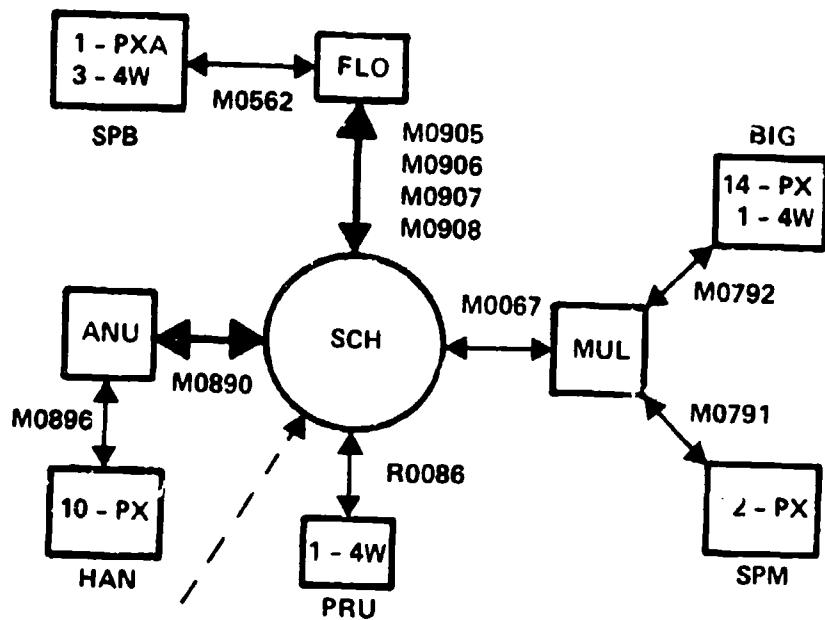


Figure A-3. Access Network for HIN



► DBP

BONN	1 - PXA, 2 - 4W
BRUNSSUM	1 - 4W
BRUSSELS	2 - 4W
CHIEVRS	1 - 4W, 1 - 4WA
EVERE	1 - 4W, 3 - PXA
PARIS	1 - PXA
SOESI - BRUECKE	1 - 4W

#### LEGEND

- — IST MICROWAVE
- — — IST TROPO
- — ACCESS MICROWAVE
- — — ACCESS TROPO

89597-8

Figure A-4. Access Network for Schoenfeld

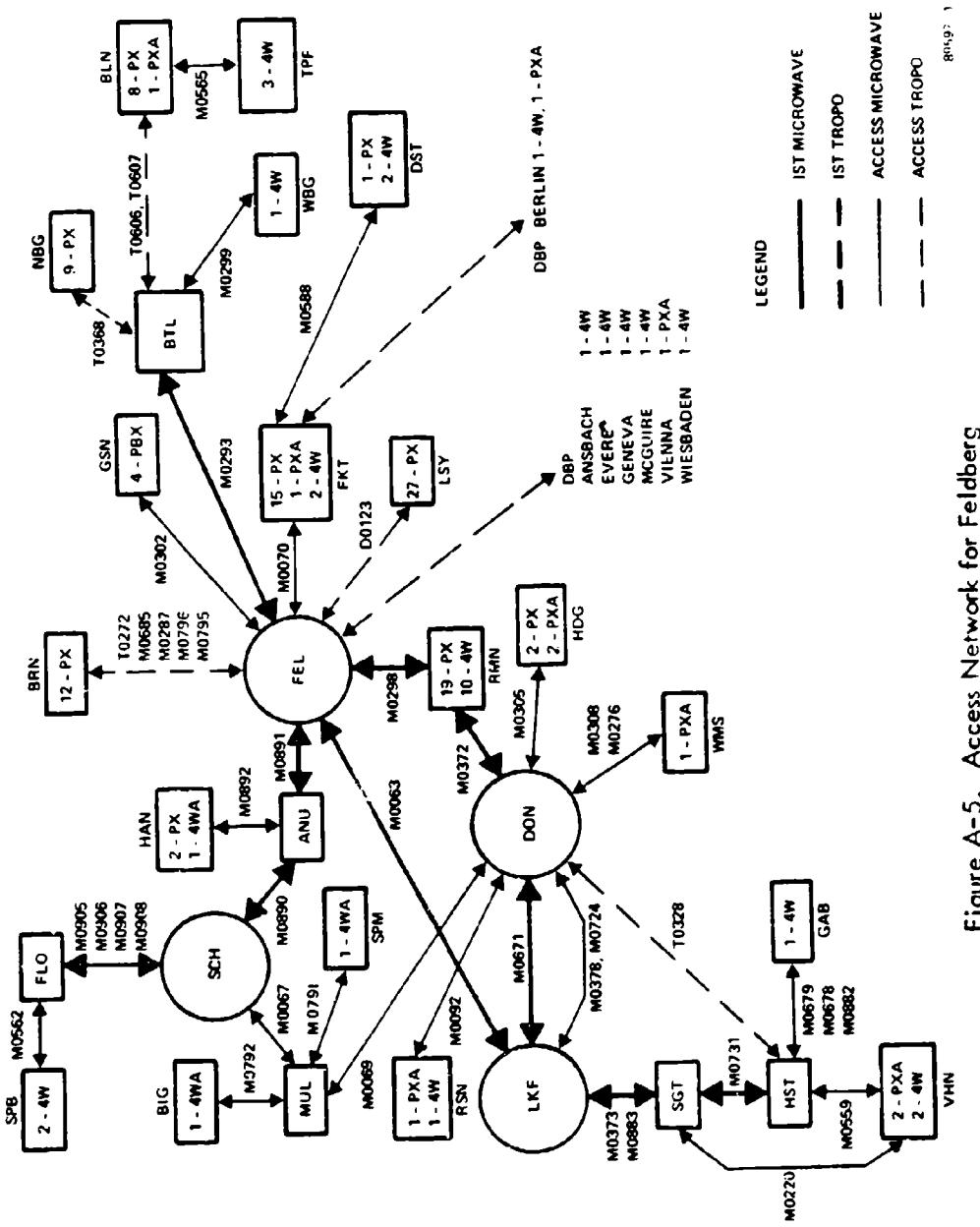
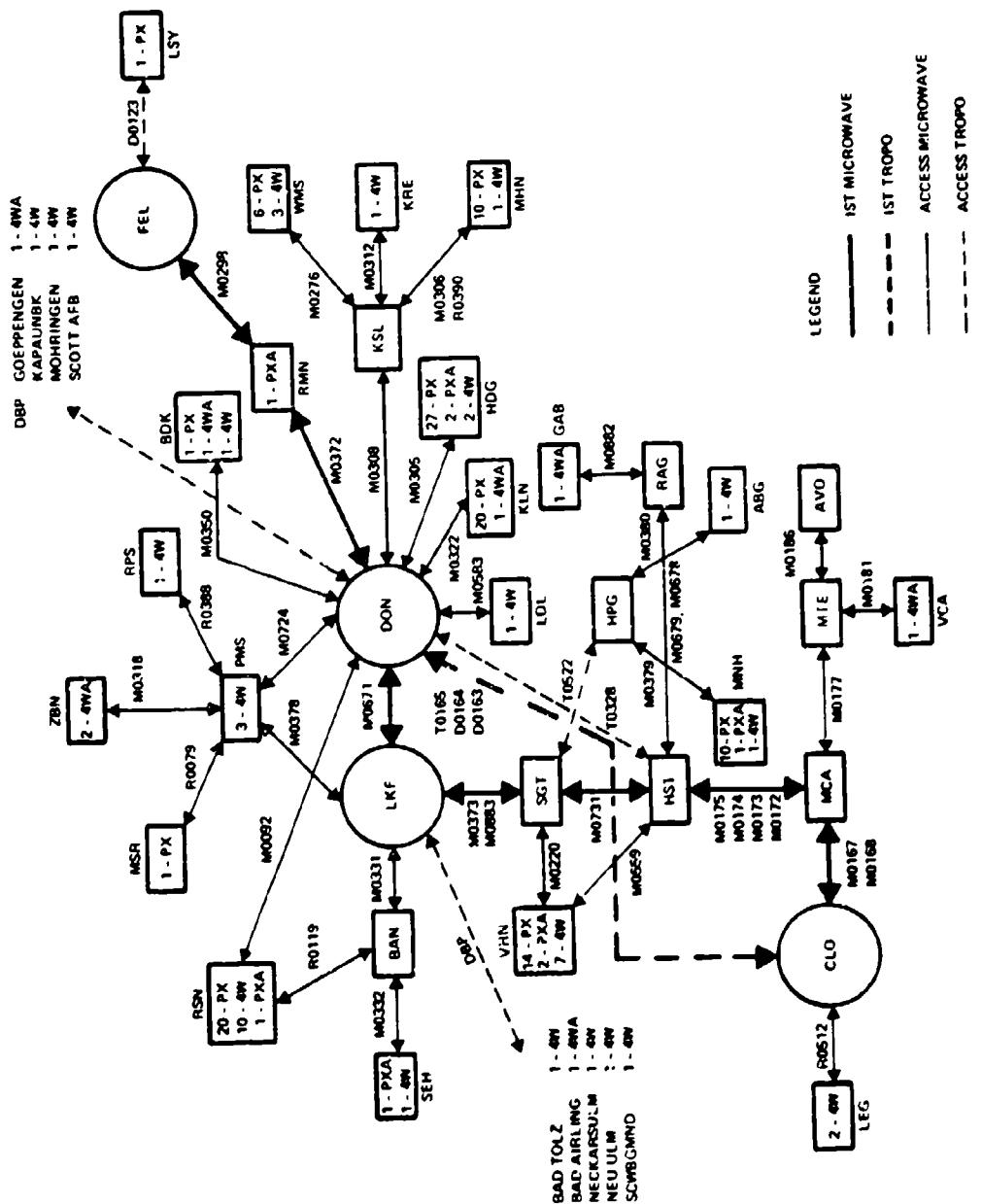
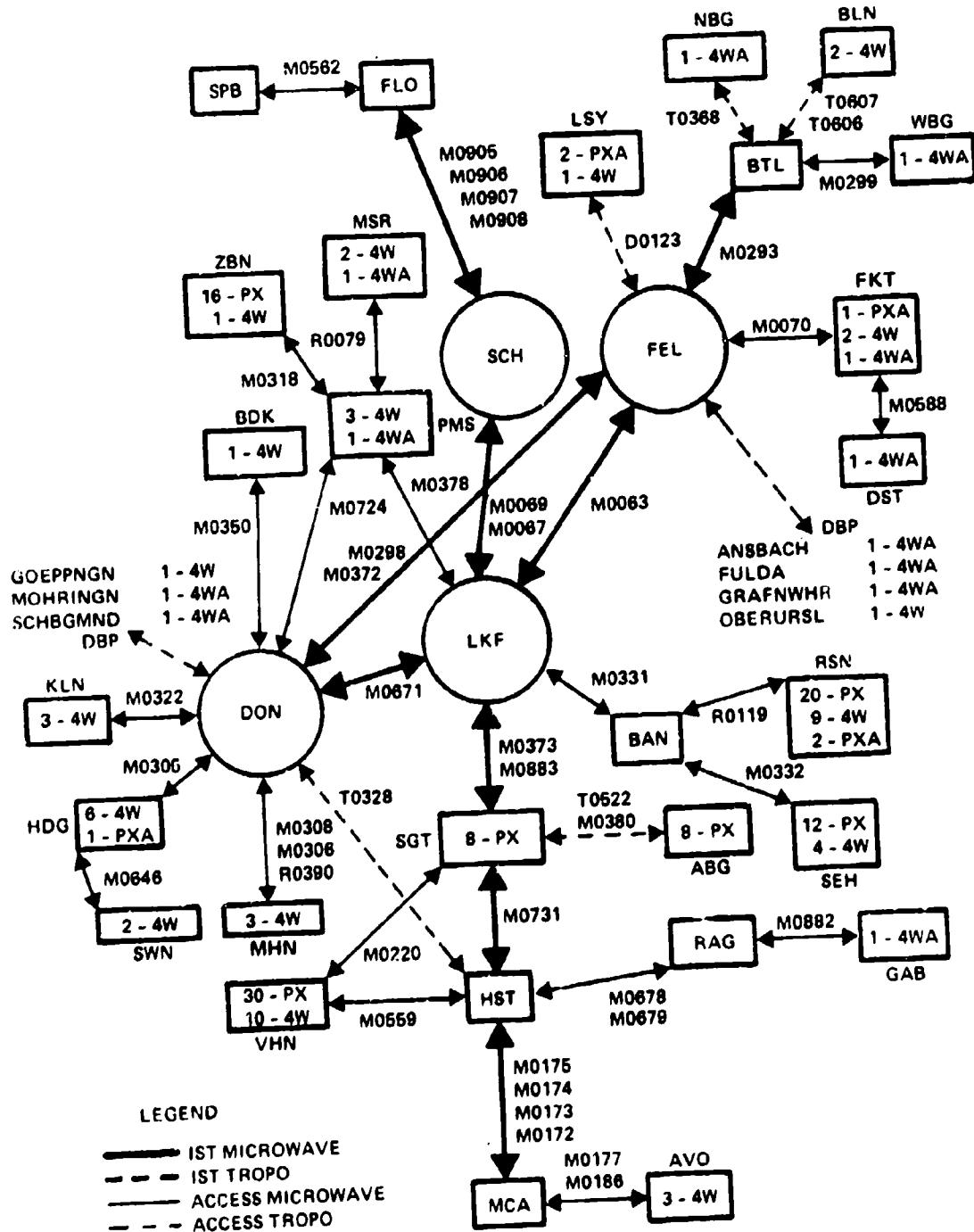


Figure A-5. Access Network for Felabbers

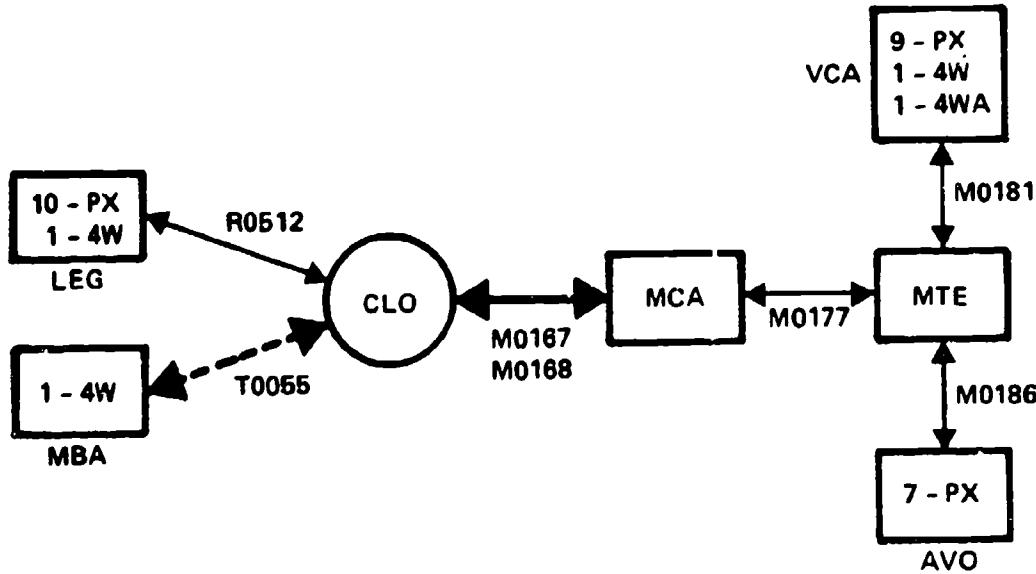


**Figure A-6:** Access Network for Donnersburg



895.7-9

Figure A-7. Access Network for Langerkopf

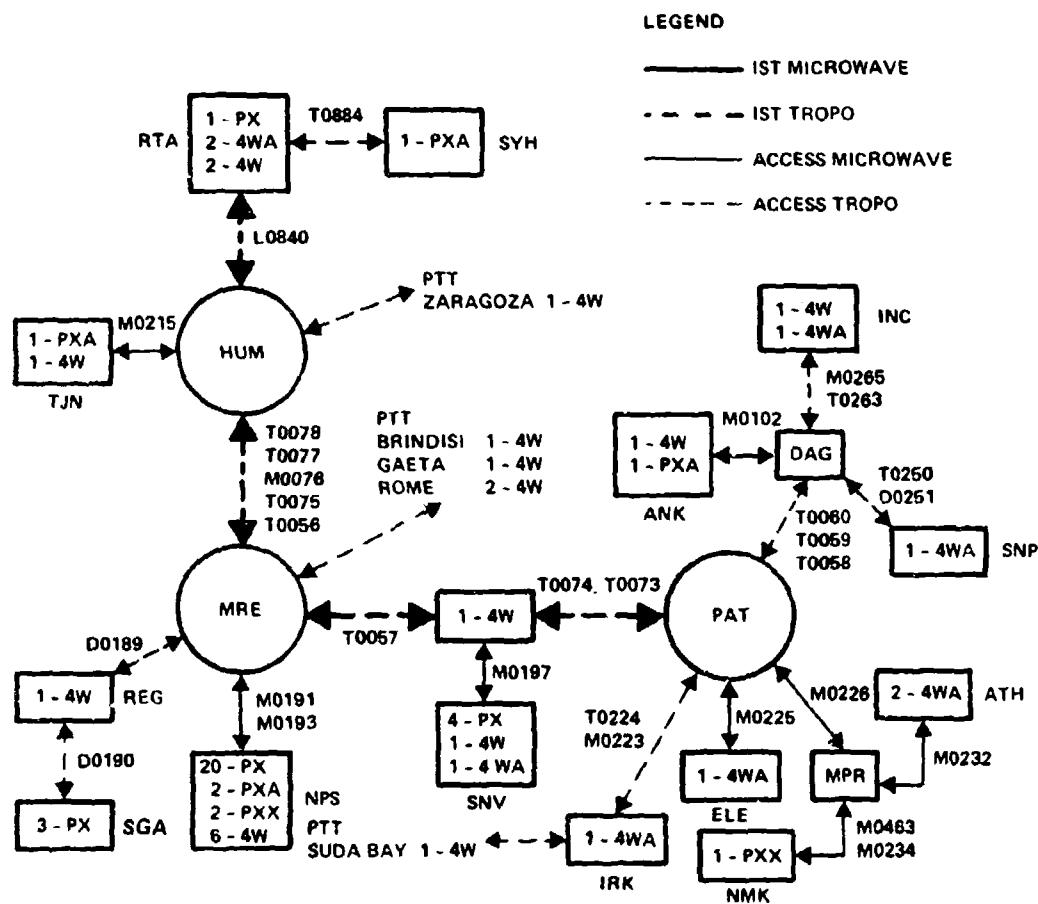


#### LEGEND

- IST MICROWAVE
- - - - - IST TROPO
- ACCESS MICROWAVE
- - - - - ACCESS TROPO

89597-10

Figure A-8. Access Network for Coltano



80507-5

Figure A-9. Access Network for Mt. Vergine

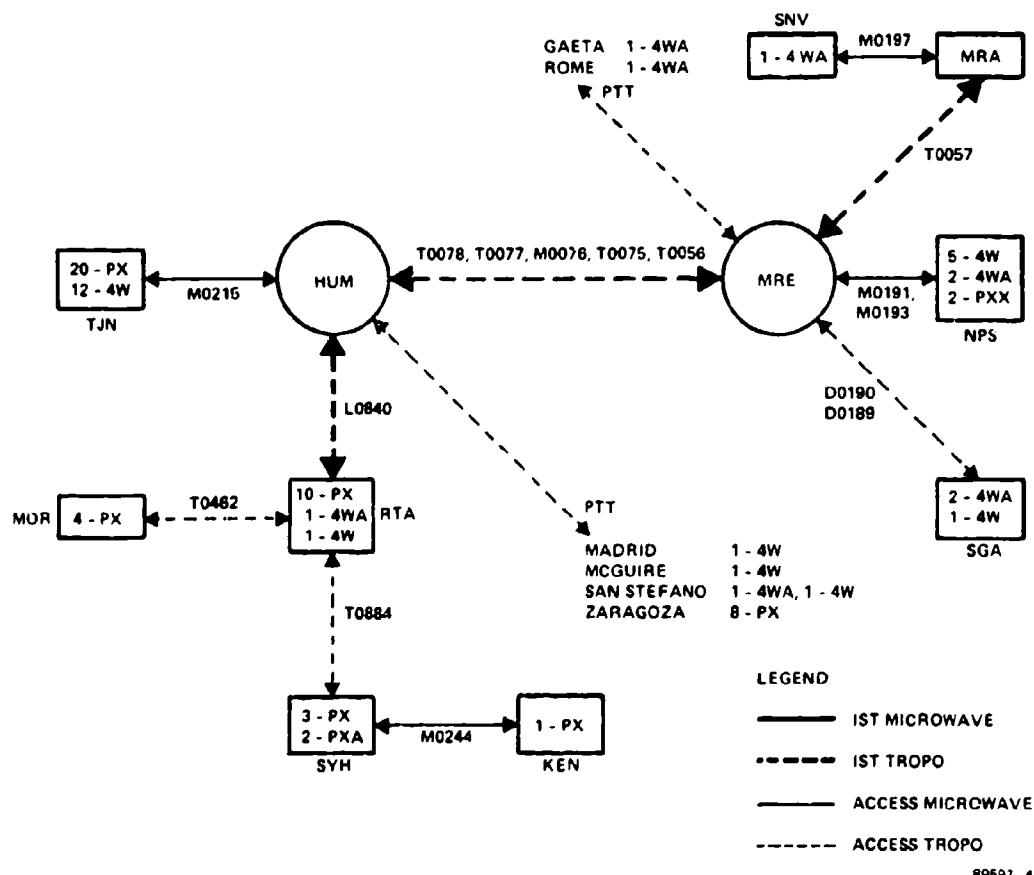


Figure A-10. Access Network for Humosa

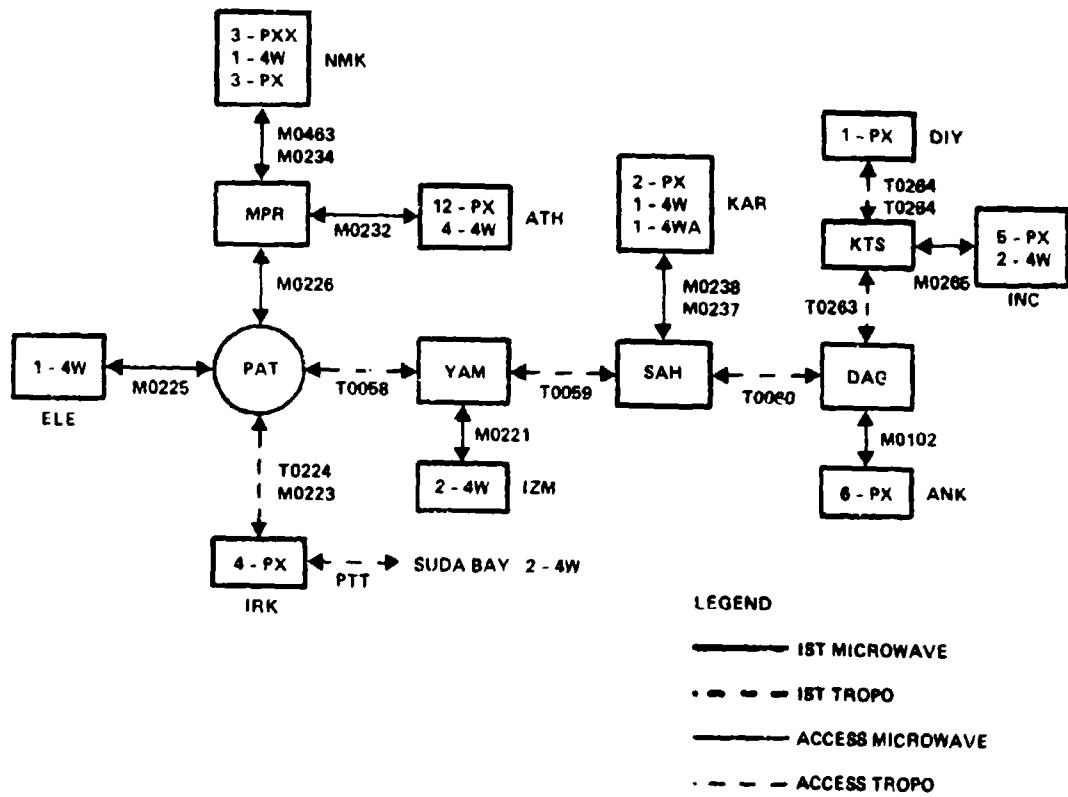


Figure A-11. Access Network for Mt. Pateras

Table A-1. Summary of Access Line Routings

	Types of Routing							
	M	T	D	L	R	H	PTT	Total No.
CLO	2	1	0	0	1	0	0	4
DON	16	8	1	0	4	0	9	38
FEL	17	6	1	0	0	0	9	33
LKF	16	5	2	0	3	0	7	33
SCH	4	0	0	0	1	0	7	12
HIN	9	4	0	2	0	2	12	29
MAM	9	5	0	0	0	4	15	29
HUM	1	7	0	1	0	0	5	14
PAT	3	7	0	0	0	0	0	10
MRE	<u>1</u>	<u>14</u>	<u>2</u>	<u>0</u>	<u>0</u>	<u>0</u>	<u>3</u>	<u>13</u>
Totals	76	57	6	3	9	6	67	221

Table A-2 shows a breakdown of the types of service and the types of links connecting the individual circuits. In this table the circuits involving LOS and government landlines (M, H, and R) have been combined as have those requiring tropo, diffraction or Telpak service (T, D and L). The first column indicates the number of subscriber locations with one or more circuits of the variety shown. The second column lists the total number of circuits involved. Thus there are 62 PBX's served which are connected by 600 circuits to the AUTOVON switches. There are 91 locations that connect 226 four wire circuits which are not switched by a PBX. Many of the 91 locations are common with those that have PBX service or other types of service. The number of routes is greater than the number of locations since some locations are connected to a switch by more than one route or are connected to more than one AUTOVON switch. There are 122 different subscriber locations connecting 928 circuits to AUTOVON switches.

There are a total of 77 different microwave LOS links, 22 different tropo links, four diffraction links, five government land line links, three Telpak links and two VHF or VHF-LOS links involved in the access network exclusive of links serving the IST network.

### A.3

#### The Pacific Network

Figure A-12 shows the Pacific IST network connections. As can be seen most of the segments are connected by either DSCS satellites, Intelsat satellite service or undersea cables. The exceptions are two segments from the Philippines to Okinawa and from Okinawa to Japan. These links involve combinations of tropo, microwave, diffraction and undersea cable links.

Data on the access lines in the Pacific was not available in sufficient detail to make the type of analysis presented for the European network. The access lines tested were to secure voice manual switchboards (SECORDS) in the Pacific area. There are 18 different such switchboards in the Pacific.

**Table A-2. Summary of Access Line Circuits**

<u>Types of Routing</u>						
	<u>No. of Locations</u>	<u>No. of Circuits</u>	<u>M + R + H</u>	<u>T + D + L</u>	<u>PTT</u>	<u>No. of Routes</u>
PX	62	600	42	24	8	74
4 WA	56	60	21	20	18	59
PXA	26	42	18	11	5	34
4 W	<u>91</u>	<u>226</u>	<u>57</u>	<u>29</u>	<u>39</u>	<u>125</u>
<b>Totals</b>	<b>122</b>	<b>928</b>	<b>91</b>	<b>63</b>	<b>67</b>	<b>221</b>
			41%	29%	30%	

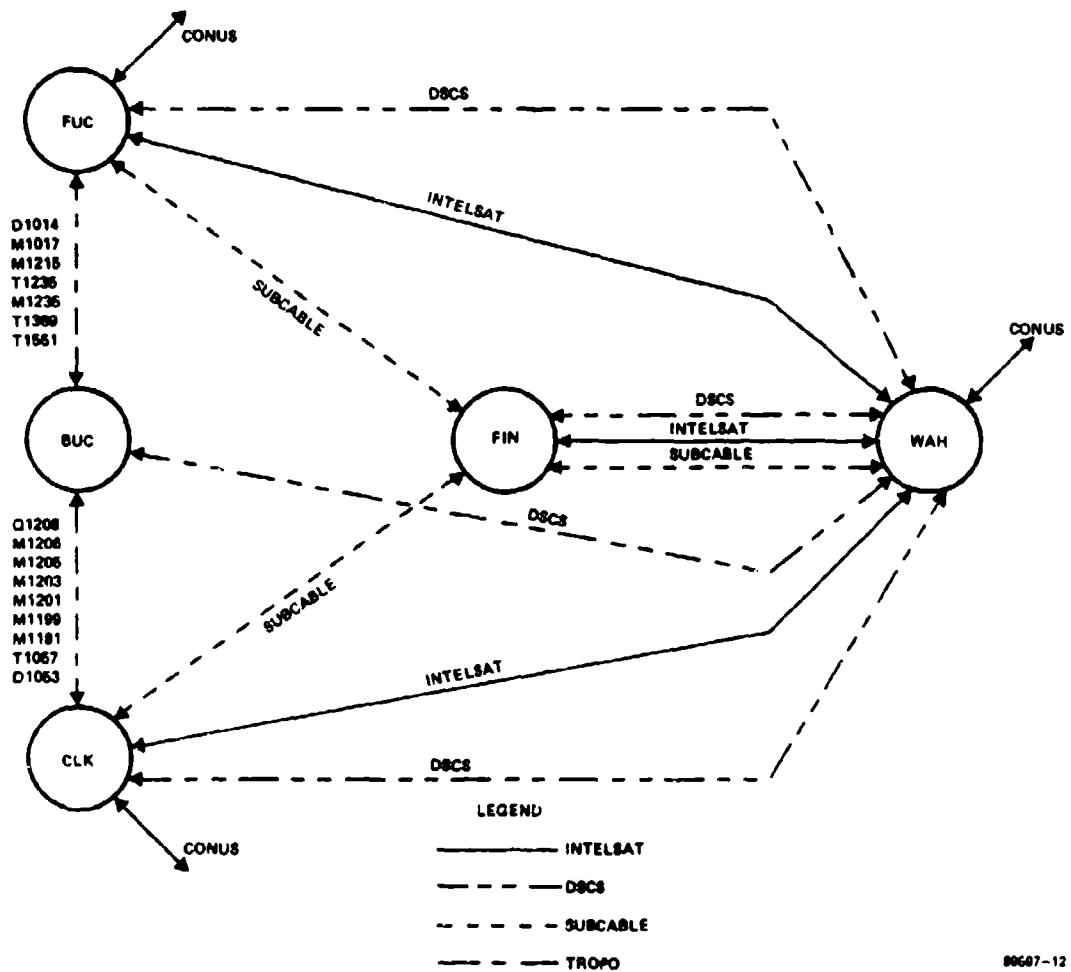


Figure A-12. Pacific IST Network

APPENDIX B  
TEST SCHEDULE

<u>Date</u>	<u>Receiver/Transmitter</u>	<u>Location</u>	<u>Transmitter</u>
November 1	Travel		Travel
2	Travel		Travel
3		Coltano, Italy	Coltano, Italy
4			Coltano, Italy
5			Travel
6			Hillingdon, England
7			
8			
9			
10			
11			
12	Travel		
13		Feldberg, Germany	
14			
15			
16			
17			
18			
19			
20			
21	Travel		Travel
22		Hillingdon, England	Coltano, Italy
23			

APPENDIX B  
TEST SCHEDULE (Continued)

<u>Date</u>	<u>Receiver/Transmitter</u>	<u>Location</u>	<u>Transmitter</u>
November 24	Hillingdon, England		Coltano, Italy
25			
26			
27			
28			
29	Christchurch, England		Ft. Detriech, MD
30	Hillingdon, England		
December 1			
2			
3			Travel
4	Travel		
9	Travel		
10	Pearl Harbor, Hawaii		Stockton, CA
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21	Travel		Travel

## APPENDIX C

### TABLES OF DATA

Since the interpretation of data collected in a test program is always influenced by the use for which the interpretation is intended, it was felt necessary to include all of the raw data that was gathered during the tests. These are presented in this section in ten tables. Since the quantity of information gathered on each test was quite large, it was found necessary to divide the horizontal column and present them on two sheets. The first sheet contains the information associated with modem performance; and the second sheet contains all of the line test data and other pertinent information. When the number of entries in a table is too large to fit on one page, all of the pages associated with the first sheets (Sheet 1) of the table are first given, followed by all of the pages associated with the second sheets (Sheet 2) of the table. The second sheet entries are indexed by title so that the two sheets can be easily correlated.

Before presenting the tables the following glossary is given which identifies the meaning of the data in the columns. The glossary for Table C-1 is given first, followed by a glossary of the columns in subsequent tables having headings which differ from those in Table C-1.

#### GLOSSARY FOR TABLE C-1

1. Table No. - Numbers indicating table and location within the table.
2. Call No. - Numbers of the calls and data sheets in chronological order. The photographs in Appendix D are keyed to call numbers. A table converting call numbers to table numbers is given in Appendix D.
3. Locations - The two locations between which the call was placed. In the case of looped calls the modem location is given first and the location of the loop is

given second. In the case of one-way calls the transmitter location is given first, followed by the modem location.

4. Date - The month and day of the call. The year of all calls was 1976 except for those conducted in January of 1977.
5. Time - The time of day the call was established.
6. BER (A) 16-110 - The 16 kb error rate (including anomalous readings\*\*) for the modem in the standard mode (110).
7. BER 8-110 - The 8 kb error rate (including anomalous readings\*\*) for the modem in the standard mode (110).
8. BTP - Block throughput. The percent of 1-second (8000 bit) intervals which were error free.
9. M - The number of microwave LOS links transited by the call.\*
10. T - The number of tropo links transited by the call.\*
11. D - The number of diffraction links transited by the call.\*
12. L - The number of commercial Telpak land links transited by the call.\*
13. LC - The number of commercial undersea cable links transmitted by the call.\*
14. DIST - The total distance traveled by the signal in statute miles.\*
15. BER (B) 16-110 - The 16 kb error rate (excluding anomalous readings\*\*) for the modem in the standard mode (110).

\*In the case of loop around calls each link has been transmitted twice. This fact has been included in the numbers of links and distance.

\*\*A discussion of the meaning of anomalous readings is presented on Page 11.

16. BER 16-130 - The 16 kb error rate in mode (130).
17. BER 16-111 - The 16 kb error rate in mode (111).
18. BER 16-C - The 16 kb error rate in mode (C).
19. Sync tries-hits - The total number of sync tries in a call in the normal sync mode followed by the number of successful synchronizations and equalization processes.
20. S/N - The equalizer signal-to-noise ratio in dB. This is the ratio of the equalizer error signal at the beginning of the training sequence (weights zeroes) to the equalizer error signal after training.
21. Table No. - Repeat of Column 1 to help index results.
22. Table No. - Same as Columns 1 and 21
23. Call No. - Same as Column 2.
24. Location (abbreviation) - An abbreviated version of the call locations given in Column 3.
25. Line Loss (Data) - The ratio in dB of the transmit signal to the receive signal when data is transmitted.
26. Line Loss - (1 kHz) - The ratio in dB of the transmit signal to the receive signal when a 1 kHz tone is transmitted.
27. S/N (Data) - The ratio in dB of the received line signal when data is transmitted to the received noise when a quiet line exists. Both signals are passed through a C-message weighted filter.
28. S/N (1 kHz) - The ratio in dB of the received signal when 1 kHz is transmitted to the received line signal when 1 kHz is notched out at the receiver. A C-message weighted filter is used.

29. PJ<sup>o</sup> - Peak-to-peak phase jitter in degrees.
30. HD 2nd - Second harmonic distortions in dB below the transmitted signal level.
31. HD 3rd - Third harmonic distortion in dB below the transmitted signal level.
32. HD Percent - Total harmonic distortion in percent of the transmitted signal level. (The square root of the sum of the squares of the second and third harmonic distortion values.)
33. GH +3 - Number of 3 dB gain hits in 5 minutes.
34. PH 20 - Number of 20 phase hits in 5 minutes.
35. 59 - Number of impulses exceeding 59 dBRNO in 5 minutes.
36. 63 - Number of impulses exceeding 63 dBRNO in 5 minutes.
37. 67 - Number of impulses exceeding 67 dBRNO in 5 minutes.
38. DO - Number of dropouts in 5 minutes.
39. Types of pictures - This specifies the type of pictures included in Appendix D for this call. The letter A indicates an amplitude-delay response picture is included. The letter B indicates a phase jitter picture. The letter C indicates an envelope picture, and D indicates a picture of the equalizer weights. Combination of letters indicate combinations of pictures are present.
40. Location of Recording - This provides the tape number and location on the tape of the recording made on this call.\*
41. Type of Recording - This indicates the type of recording that was made. The first letter indicates:
  - A - A 16 kb recording of test sentence from an IEEE tape
  - B - A 16 kb recording of test sentences read by operator

\*These tapes have been delivered to RADC as a part of the contract. Requests concerning these tapes should be addressed to RADC/DCLD.

C - No test sentences but some brief recording

D - An 8 kb recording of test sentences from an IEEE tape

E - An 8 kb recording of test sentence read by operator

The number following the letter indicates which set of test sentences was played or read. Appendix E contains the test sentence sets and their numbers.

42. Routing - This gives the last four digits of the CCSD designators of circuits involved in the routing. The first four digits of the CCSD designators have been omitted since they are the same for AUTOVON circuits in a given area. In a few instances CCSD designators were not identified, but group and channel numbers were included in their place.

Following each CCSD number is an indication as to whether the circuit is listed as V1, V2, or S3 conditioned.

43. Line Characteristics - This column indicates the highest line condition that the amplitude and delay characteristics of the composite circuits of the call meet, based on the picture of Appendix D.

44. Comments - These are comment numbers which are keyed to the table of comments in Table C-11 following the data tables.

45. Table No. - Same as Columns 1, 21 and 22.

Table C-2

- 13 R - The number of government land-line links transited by the call
- 14 DIG - The number of digital links transited by the call

Table C-5

- 9 NATO 1 - The number of satellite links through the NATO satellite with terminals located at Norfolk, Virginia and Oakhanger, England.
- 10 NATO 2 - The number of satellite links through the NATO satellite with terminals located at Lakehurst, New Jersey and Donnersburg, Germany.
- 11 INTELSAT - The number of satellite links through an INTELSAT satellite with terminals located at Andover, Maine and Goonhillydown, England.
- 12 TAT-I - The number of undersea cable links through the TAT-I cable with terminals located at Sydney Mines, Nova Scotia and Oban, Scotland.
- 13 TAT-III - The number of undersea cable links through the TAT-III cable with terminals located at Tuckerton, New Jersey and Widemouth, England.
- 14 TAT-IV - The number of undersea cable links through the TAT-IV cable with terminals located at Tuckerton, New Jersey and St. Hilairede Riez, France.
- 15 TAT-V - The number of undersea cable links through the TAT-V cable with terminals located at Greenhill, Rhode Island and Conil, Spain.

Table C-6

- 9 DSCS - The number of satellite links through a DSCS satellite with terminals located at Camp Roberts, California and Wahiawa, Hawaii.
- 10 INTELSAT I - The number of satellite links through an INTELSAT satellite with terminals located at San Luis Obispo, California and Wahiawa, Hawaii.

Table C-6 (Continued)

- 11 INTELSAT II - The number of satellite links through an INTELSAT satellite with terminals located at Lodi, California and Wahiawa, Hawaii.
- 12 HAWAII I - The number of undersea cable links through the HAWAII I cable with terminals located at San Luis Obispo, California and Makaha, Hawaii.
- 13 HAWAII II - The number of undersea cable links through the HAWAII II cable with terminals located at Pt. Arena, California and Hanaumby, Hawaii.
- 14 HAWAII III - The number of undersea cable links through the HAWAII III cable with terminals located at San Luis Obispo, California and Makaha, Hawaii.

Table C-7

- 9 COMSAT - The number of satellite links through an INTELSAT satellite transited by call.
- 10 DSCS - The number of satellite links through a DSCS satellite transited by call
- 11 Cable - The number of undersea cable links transited by call.
- 12 Tropo - The number of tropo links transited by call.

Table C-10

- 9 Type of Call - The special characteristic of the call.

Table C-1. European IST Loops (Sheet 1)

Loop	Location	PRIMARY ROUTINGS												S/NO	T/NO-HI	Z/NO	T/NO			
		1	2	3	4	5	6	7	8	9	10	11	12							
1-1	10	Coltano, Italy - Hillingdon, Eng.	11/4	1454	3.08E-2	6.12E-5	68	32	8	2	0	3576	3.08E-2	3.25E-2	3.15E-2	2.79E-2	5-5	18	1-1	
1-2	55	Coltano, Italy - Hillingdon, Eng.	11/9	2223	2.58E-3	3.13E-4	94	32	8	2	0	3576	2.58E-3	4.05E-3	2.85E-3	3.52E-3	4-4	22	1-2	
1-3	58	Coltano, Italy - Hillingdon, Eng.	11/9	2336	8.49E-3	4.77E-4	97	32	8	2	0	3576	8.49E-3	8.99E-3	6.84E-3	9.00E-3	4-4	20	1-3	
1-4	41	Coltano, Italy - Hillingdon, Eng.	11/8	1615	5.37E-2	2.13E-3	84	2	8	0	6	?	4238	5.37E-2	6.19E-2	8.57E-2	7.41E-2	4-4	18	1-4
1-5	47	Coltano, Italy - Hillingdon, Eng.	11/9	1107	1.32E-2	1.00E-5	97	32	8	2	0	3576	1.32E-2	7.50E-3	1.15E-2	8.20E-3	4-4	20	1-5	
1-6	13	Coltano, Italy - Feldberg, Germ.	11/14	1705	3.40E-4	0	100	20	0	0	0	1080	3.40E-4	6.24E-4	-	-	3-3	25	1-6	
1-7	2	Coltano, Italy - Humosa, Spain	11/3	1545	1.85E-2	4.50E-5	95	2	8	0	2	0	2374	1.85E-2	8.69E-3	2.11E-2	1.59E-2	7-7	21	1-7
1-8	28	Coltano, Italy - Humosa, Spain	11/8	0815	2.55E-3	7.87E-5	97	2	8	0	2	0	2374	2.55E-3	1.88E-3	3.92E-3	1.90E-3	4-4	25	1-8
1-9	54	Coltano, Italy - Humosa, Spain	11/9	2157	1.62E-3	8.87E-5	97	2	8	0	2	0	2374	1.62E-3	1.67E-3	1.68E-3	4.54E-4	4-4	24	1-9
1-10	57	Coltano, Italy - Humosa, Spain	11/9	2315	1.46E-4	0	100	2	8	0	2	0	2374	1.46E-4	3.67E-4	4.61E-4	2.76E-4	4-4	25	1-10
1-11	4	Coltano, Italy - Mt. Pateros, Greece	11/4	0920	1.91E-4	2.87E-5	99	2	6	0	2	0	1612	1.91E-4	1.38E-4	1.38E-1	3.14E-4	4-4	25	1-11
1-12	27	Coltano, Italy - Mt. Pateros, Greece	11/5	1620	1.24E-3	0	100	2	6	0	2	0	1612	1.24E-3	1.52E-3	2.71E-3	8.06E-4	4-4	24	1-12
1-13	56	Coltano, Italy - Mt. Pateros, Greece	11/9	2250	4.02E-4	0	100	2	6	0	2	0	1612	4.02E-4	8.45E-4	1.03E-2	7.68E-4	4-4	24	1-13
1-14	59	Coltano, Italy - Mt. Pateros, Greece	11/9	2357	3.58E-4	5.00E-6	99	2	6	0	2	0	1612	3.58E-4	3.38E-4	2.00E-4	1.14E-4	4-4	23	1-14
1-15	62	Coltano, Italy - Mt. Pateros, Greece	11/10	1507	1.02E-4	6.37E-5	95	2	6	0	2	0	1612	1.02E-4	2.74E-4	2.79E-4	2.71E-4	4-4	25	1-15
1-15	6	Coltano, Italy - Mt. Virgine, Italy	11/4	1005	3.31E-4	1.50E-5	100	0	0	2	0	580	3.31E-4	6.25E-5	-	-	4-4	28	1-16	
1-17	7	Coltano, Italy - Schoenfeld, Germ.	11/4	1027	1.60E-4	0	100	4	2	4	0	1252	1.60E-4	1.40E-4	8.75E-5	6.62E-5	4-4	26	1-17	
1-18	9	Coltano, Italy - Martlesham Heath, Eng.	11/3	1216	1.33E-3	5.25E-5	100	6	6	4	0	1844	1.33E-3	1.39E-3	1.83E-3	1.14E-3	4-4	24	1-18	
1-19	12	Coltano, Italy - Donnersburg, Germ.	11/4	1556	6.00E-5	1.00E-5	100	0	2	4	0	970	6.00E-5	1.87E-5	1.60E-5	7.50E-5	4-4	29	1-19	
1-20	14	Coltano, Italy - Langenkopf, Germ.	11/4	1723	3.40E-4	0	100	18	0	0	0	1004	3.40E-4	6.24E-4	-	-	4-4	25	1-20	
1-21	69	Feldberg, Germ.- Hillingdon, Eng.	11/15	0933	1.75E-5	2.00E-5	100	26	0	0	0	842	1.75E-5	7.50E-6	0	1.25E-5	4-4	28	1-21	
1-22	77	Feldberg, Germ.- Hillingdon, Eng.	11/15	1518	0	0	100	26	0	0	0	842	0	0	0	0	4-4	30	1-22	
1-23	136	Feldberg, Germ.- Hillingdon, Eng.	11/19	1350	3.75E-6	0	100	26	0	0	0	842	3.75E-6	0	0	0	4-4	28	1-23	
1-24	99	Feldberg, Germ.- Colfano, Italy	11/17	1110	2.45E-3	8.87E-5	99	28	0	0	0	1682	2.45E-3	1.99E-3	3.16E-3	1.69E-3	3-3	21	1-24	
1-25	98	Feldberg, Germ.- Humosa, Spain	11/17	0956	3.31E-2	5.14E-4	92	22	12	0	0	3996	3.31E-2	3.34E-2	3.14E-2	3.73E-2	4-4	19	1-25	
1-26	95	Feldberg, Germ.- Mt. Pateros, Greece	11/17	0925	1.16E-2	1.20E-4	89	20	10	0	0	3234	1.16E-2	2.42E-2	1.24E-2	1.12E-2	4-4	22	1-26	

**Table C-1.** European IST Loops (Sheer) (Continued)

Table C-1. European 151 Loops (Sheet 1 Continued)

Loop	Location	SECONDARY ROUTINGS (CONTINUED)																	
		1	2	3	4	5	6	7	8	9	10	11	12						
1-51	25 Colfano, Italy - Mt. Pateros, Greece	11/5	1528	2.66E-2	3.75E-5	85	0	14	8	0	0	3836	2.66E-2	4.12E-2	4.07E-2	4.56E-2	4-4	20	1-51
1-52	35 Colfano, Italy - Mt. Vergine, Italy	11/8	1058	4.75E-2	8.25E-5	80	40	4	0	0	0	3282	4.75E-2	4.71E-2	4.24E-2	6.62E-2	3-3	18	1-52
1-53	30 Colfano, Italy - Schoenfeld, Germ.	11/8	0913	7.36E-4	0	100	24	0	0	0	0	1272	7.36E-4	9.50E-4	1.13E-4	9.07E-4	4-4	23	1-53
1-54	29 Colfano, Italy - Mortlesham Heath, Eng.	11/8	0848	2.33E-2	8.87E-5	91	22	4	2	0	0	1768	8.57E-3	8.01E-3	8.56E-3	8.75E-3	3-2	20	1-54
1-55	31 Colfano, Italy - Donnersburg, Germ.	11/8	0943	1.03E-3	0	100	24	0	0	0	0	1168	1.03E-3	9.98E-4	1.01E-3	8.85E-4	4-4	23	1-55
1-56	32 Colfano, Italy - Langendorf, Germ.	11/8	1008	7.65E-4	-	-	22	0	0	0	0	1220	7.05E-4	1.70E-3	1.11E-3	-	2-2	23	1-56
1-57	33 Colfano, Italy - Langendorf, Germ.	11/8	1010	9.59E-4	7.50E-6	96	22	0	0	0	0	1220	9.59E-4	7.27E-4	7.51E-4	1.50E-3	4-4	23	1-57
1-58	79 Feldberg, Germ.- Hillington, Eng.	11/15	1530	3.06E-4	-	100	12	4	2	0	0	892	3.06E-4	-	-	-	1-1	25	1-58
1-59	13C Feldberg, Germ.- Hillington, Eng.	11/19	1040	2.44E-3	7.28E-4	98	12	4	2	0	0	892	2.44E-3	2.97E-3	3.81E-3	3.01E-3	4-4	23	1-59
1-60	109 Feldberg, Germ.- Colfano, Italy	11/17	1522	4.25E-5	1.25E-4	99	4	2	4	0	0	1138	4.25E-5	2.12E-5	5.16E-5	2.11E-4	5-4	27	1-60
1-61	104 Feldberg, Germ.- Humosa, Spain	11/17	1340	1.17E-2	5.06E-3	96	-	-	-	-	-	1.17E-2	1.25E-2	1.14E-2	1.32E-2	4-4	20	1-61	
1-62	105 Feldberg, Germ.- Mt. Pateros, Greece	11/17	1410	2.05E-2	-	-	4	12	4	0	0	2934	2.05E-2	2.27E-2	1.55E-2	9.19E-3	2-2	20	1-62
1-63	107 Feldberg, Germ.- Mt. Vergine, Italy	11/17	1441	2.20E-2	4.12E-5	93	0	6	4	0	0	1834	2.20E-2	2.12E-2	3.78E-2	2.17E-2	4-4	20	1-63
1-64	112 Feldberg, Germ.- Schoenfeld, Germ.	11/17	1630	3.49E-3	0	100	8	0	0	0	0	390	3.49E-3	5.45E-3	2.53E-3	7.65E-4	4-4	24	1-64
1-65	128 Feldberg, Germ.- Mortlesham Heath, Eng.	11/19	0838	7.72E-4	1.50E-5	97	6	4	2	0	0	874	7.72E-4	9.34E-4	9.06E-4	4.33E-4	6-6	25	1-65
1-66	108 Feldberg, Germ.- Donnersburg, Germ.	11/17	1503	5.00E-6	0	100	4	0	0	0	0	186	5.00E-6	0	3.75E-6	0	6-4	29	1-66
1-67	113 Feldberg, Germ.- Langendorf, Germ.	11/17	1658	0	0	100	6	0	0	0	0	134	0	7.50E-6	1.50E-5	7.50E-6	7-4	25	1-67
1-68	156 Hillington, Eng.- Colfano, Italy	11/24	1413	5.03E-3	2.50E-6	91	46	0	0	0	0	1922	5.03E-3	6.52E-3	6.26E-3	6.45E-3	4-4	19	1-68
1-69	178 Hillington, Eng.- Mortlesham Heath, Eng.	11/26	1410	1.79E-3	1.50E-5	91	12	4	2	0	0	892	1.79E-3	2.24E-3	2.13E-3	1.96E-3	3-3	20	1-69
1-70	52 Hillington, Eng.- Humosa, Spain	11/25	1028	8.11E-3	4.75E-5	90	50	8	0	0	0	3822	8.11E-3	1.05E-2	1.67E-2	1.03E-2	4-4	20	1-70
1-71	168 Hillington, Eng.- Mt. Pateros, Greece	11/25	1542	9.41E-2	-	-	-	-	-	-	-	3944	9.41E-2	-	-	-	1-1	18	1-71
1-72	180 Hillington, Eng.- Mt. Pateros, Greece	11/26	1455	2.30E-2	6.45E-4	76	20	10	0	0	0	2946	2.30E-2	1.83E-2	2.05E-2	2.04E-2	5-5	18	1-72
1-73	173 Hillington, Eng.- Mt. Vergine, Italy	11/26	1030	1.03E-2	5.00E-6	99	46	4	0	0	0	3041	1.01E-2	1.19E-2	1.23E-2	1.89E-2	4-4	20	1-73
1-74	175 Hillington, Eng.- Schoenfeld, Germ.	11/26	1135	1.25E-6	0	100	30	0	0	0	0	2394	1.25E-6	7.50E-6	5.00E-6	0	4-4	28	1-74
1-75	179 Hillington, Eng.- Donnersburg, Germ.	11/26	1435	1.09E-3	7.00E-5	89	16	4	2	0	0	1076	1.09E-3	1.20E-3	8.48E-4	9.53E-4	5-4	24	1-75
1-76	177 Hillington, Eng.- Langendorf, Germ.	11/26	1155	1.30E-3	2.50E-6	99	28	0	0	0	0	984	1.25E-3	4.69E-6	3.13E-6	4-4	25	1-76	

Table C-1. European ISI Loops (Sheet 1 Continued)

Loop ID	Location	TERNARY ROUTINGS												NONENGINEERED ROUTINGS														
		011-91	011-91	011-91	011-91	011-91	011-91	011-91	011-91	011-91	011-91	011-91	Δ	011-91	011-91	011-91	011-91	011-91	011-91	011-91	011-91	011-91	011-91	011-91				
1-77	106	Feldberg, Germ.-Humosa, Spain	11-17	1418	6.25E-3	3.01E-3	98	26	0	4	2	2706	6.25E-6	2.00E-5	3.12E-5	2.50E-6	4-4	28	1-77									
1-78	172	Hillingdon, Eng.-Humosa, Spain	11-26	0952	2.45E-2	3.87E-5	98	48	12	0	0	4838	2.45E-2	2.18E-2	2.17E-2	2.06E-2	5-4	19	1-78									
1-79	174	Hillingdon, Eng.-Donnersburg, Germ.	11-26	1050	2.08E-3	2.50E-6	99	30	0	0	0	930	2.88E-5	4.00E-5	3.50E-5	4-4	27	1-79										
1-80	176	Hillingdon, Eng.-Donnersburg, Germ.	11-26	1150	3.75E-6	-	-	30	0	0	0	930	8.75E-6	-	-	-	-	1-1	27	1-80								
1-81	43	Cotzano, Italy - Hillingdon, Eng.	11-8	1645	5.54E-4	9.12E-5	94	16	6	0	0	2048	5.54E-4	7.69E-4	7.39E-4	6.96E-4	5-5	23	1-81									
1-82	45*	Cotzano, Italy - Hillingdon, Eng.	11-9	1000	1.59E-2	0	100	2	8	0	6	2	4238	1.59E-2	1.92E-2	1.89E-2	2.33E-2	5-5	20	1-82								
1-83	81	Feldberg, Germ.-Hillingdon, Eng.	11-15	1630	2.23E-2	7.37E-5	94	2	10	4	2	6156	2.23E-2	2.41E-2	2.66E-2	8-4	22	1-83										
1-84	134	Feldberg, Germ.-Hillingdon, Eng.	11-19	1245	1.99E-2	7.50E-6	87	-	-	-	-	-	1.99E-2	1.43E-2	3.82E-2	1.99E-2	3-3	17	1-84									
1-85	132	Feldberg, Germ.-Hillingdon, Eng.	11-19	1215	1.18E-1	4.05E-3	62	52	12	2	0	0	5296	1.18E-1	7.32E-2	1.22E-1	8.08E-2	7-6	12	1-85								

Table C-1. European IS1 Loops (Sheet 2)

Loop	Call	Location	Line Loss	IDB10	S/N (1 kHz)	Pj0	HD 2nd	HD 3rd	HD 4th	HD 5th	HD 6th	HD 7th	HD 8th	HD 9th	HD 10th	HD 11th	PRIMARY ROUTINGS						Recording of Pictures of Locations of Recorders	Type of Recording	Routing	Comments											
																	59	63	67	Q	D	C	B	A	9	3	H	E	D	C	B	A					
1-1	10	CLO-HIN	-3	-3	28	26	12	45	46	.75	0	39	1732	641	89	2	A	1-1,156	A-6,D-7	CLO 9CVM V2 MRE 9AE8 V2 HIN V2	1-1																
1-2	55	CLO-HIN	-1	-2	3?	29	13	40	1.00	0	7	1145	73	12	10	AB	2-1,057	A-10	CLO 9CVM V2 MRE 9AE8 V2 HIN V2	1-2																	
1-3	58	CLO-HIN	6	4	30	30	13	43	42	1.06	1	7	1075	54	9	8	AB	2-1,093	C	CLO 9CVM V2 MRE 9AE8 V2 HIN V2	1-3																
1-4	41	CLO-HIN	3	1	30	32	10	40	39	1.50	2	28	475	177	56	5	AC	1-2,219	A-5	CLO 9CVR S3 MRE 9CHL S3 HUM V1	1-4																
1-5	47	CLO-HIN	5	3	30	28	14	44	41	1.09	1	32	1579	203	0	0	AB	1-2,417	A-8	CLO 9DQF S3 MRE 9AE8 V2 HIN V2	1-5																
1-6	13	CLO-FEL	2	1	33	32	8	50	47	.55	0	0	224	2	0	0	A	—	—	CLO 9CUX V2 FEL	V2	1-6															
1-7	2	CLO-HUM	-1	-3	37.5	33	7	41	38	1.54	3	4	578	245	68	0	A	1-1,016	B-2	CLO 9DQD V2 MRE — HUM V2	1-7																
1-8	28	CLO-HUM	-3	-3	36	36	5	39	37	1.80	0	1	271	125	42	0	A	1-7,021	A-1	CLO 9CVM V2 MRE 9CHU V2 HUM V2	1-8																
1-9	54	C.O-HUM	5	4	31.5	33	6	38	40	1.61	1	0	53	12	1	1	AC	1-2,036	A	CLO 9CVN V2 MRE 9CPG V2 HUM V2	1-9																
1-10	57	C.O-HUM	7	6	34.5	34	6	40	40	1.41	0	0	233	71	9	0	A	1-2,057	A	CLO 9DQD V2 MRE 9CPG V2 HUM V2	1-10																
1-11	4	CLO-PAT	-1	-4	39	37	4	40	39	1.50	0	0	146	47	6	0	A	1-1,051	A-4	CLO 9CVN V2 MRE 9CWY V2 PAT	V2	1-11															
1-12	27	CLO-PAT	-1	-3	40	28	8	37	37	2.00	0	0	490	112	21	0	AB	1-2,001	A-1	CLO 9CVN V2 MRE 9DDA V2 PAT	V2	1-12															
1-13	56	C.O-PAT	4	2	32	33	7	41	39	1.43	0	0	197	27	4	0	AD	2-1,078	C	CLO 9CVM V2 MRE 9CWX V2 PAT	V2	1-13															
1-14	59	C.O-PAT	-3	-4	39.5	33	9	35	37	2.27	0	0	315	54	9	0	A	2-1,101	C	CLO 9CVM V2 MRE 9DDA V2 PAT	V2	1-14															
1-15	62	CLO-PAT	1	0	37	30	10	39	36	1.94	0	0	302	113	16	0	AL	2-1,184	C	CLO 9CVM V2 MRE 9CXD S3 PAT	V2	1-15															
1-16	6	C.O-MRE	2	1	40	39	4	49	46	.61	-	0	189	92	39	1	A	1-1,086	C	CLO 9CVR S3 MRE	V2	1-16															
1-17	7	CLO-SCH	1	0	35	36	4	54	49	.41	0	1	3	2	1	0	A	1-1,093	B-4	CLO 9CWB S3 DON 9CHC S3 SCH V2	1-17																
1-18	9	CLO-MAM	-1	-1	31	29	8	30	45	.56	1	1	1295	168	67	0	A	1-1,138	B-6	CLO 9CVX S3 DON 9EPN V2 NAM V2	1-18																
1-19	12	CLO-DON	0	1	40	37	3	38	38	0	0	0	19	7	5	0	A	1-1,204	B-7	CLO 9CWW V2 DON	S1	1-19															
1-20	14	CLO-LK	2	1	33	32	8	50	47	.55	0	0	224	2	0	0	A	1-1,222	A-8	CLO 9CWW V2 DON	V2	1-20															
1-21	69	FEL-HIN	2	1	43.5	44	4	53	50	.45	0	4	3	3	0	A	2-1,356	C	FEL 9ACF S3 HIN	S3	1-21																
1-22	77	FEL-HIN	1	0	42.5	34.5	5	55	50	.36	6	0	3	2	1	4	A	2-2,052	C	FEL 9ACL S3 HIN	S3	1-22															
1-23	136	FEL-HIN	1	1	45.5	43	4	55	49	.40	0	0	0	0	0	0	A	—	—	FEL 9ACF S3 HIN	S3	1-23															
1-24	99	FEL-CLO	6	-	35	27	15	50	52	.40	0	2	1237	4	0	0	A	2-2,400	B-9	FEL 9CUV S3 CLO	V2	1-24															
1-25	96	FEL-HUM	1	0	29.5	30	14	40	37	1.73	2	23	400	80	15	2	A	2-2,346	A-6	FEL 9AC1 S3 MRE 9CHN S3 HUM V2	1-25																
1-26	95	FEL-PAT	5	4	30.5	30	10	43	40	1.22	7	3	1030	196	101	15	AB	2-2,312	A-5	FEL 9CEQ V2 MRE 9CWX V2 PAT	V2	1-26															
1-27	97	FEL-MRE	3	3	36.5	36..	9	45	46	.75	2	5	564	137	25	4	A	2-2,387	C	FEL 9ACT S3 MRE	V2	1-27															

Table C-1. European IST Loops (Sheet 2 Continued)

Secondary Routings																							
1-44	39	CLO-HIN	0	1	33	32	10	48	.45	.69	0	1	787	13	7	0	A8	1-2,160	A-4	CLO 9CVD S3 FEL 9ACF S3 HIN	V2	5	1-44
1-45	51	CLO-HIN	6	5	33	31	14	49	.44	.72	1	2	441	28	18	4	A8	1-2,510	C	CLO 9CVW S3 FEL 9ACH S3 HIN	V2	1-45	
1-46	53	CLO-HIN	8	6	31	30	16	45	.44	.84	0	1	1231	53	10	0	A8	2-1,019	B-8	CLO 9CUW S3 FEL 9ACG S3 HIN	S1	1-46	
1-47	36	CLO-FEL	2	1	37	39	3	40	.43	.71	0	0	11	7	1	0	A	1-2,103	C	CLO 9CVX S3 DON -	-FEL	S1	1-47
1-48	22	CLO-HUM	3	2	27	27	15	40	.39	1.12	11	33	1807	1526	952	41	A8	1-1,329	E-2	CLO 9CVT V2 DON 9DGC V2 HUM	V2	1-48	
1-49	23	CLO-HUM	4	4	26	26	15	44	.42	1.01	0	13	1846	1490	135	0	A8	1-1,373	A-9	CLO 9CVV V2 DON 9CGS S3 HUM	V1	1-49	
1-50	24	CLO-HUM	9	9	26	24	23	37	.42	1.62	1	77	1805	1704	186	1	A8	1-1,407	C	CLO 9POG V2 DON 9CGS S3 HUM	V2	7	1-50
1-51	25	CLO-PAT	2	1	32	27	9	41	.38	1.54	28	139	1510	451	63	3	A	1-1,423	B-1	CLO 9DOH S3 DON 9DAB V2 PAT	V2	1-52	

Table C-1. European IST Loops (Sheet 2 Continued)

Rounding											
Type of Recording											
Pictures of Recordings											
Comments	Character	Line	Total	Line Loss							
Comments	Character	Line	Total	Line Loss							
1-52	CLO-MRE	4	2	24	26	14	45	46	.75	1	6
1-53	CLO-SCH	4	3	34	30	11	53	45	.60	0	3
1-54	CLO-MAM	7	5	30	28	16	49	46	.61	-	-
1-55	CLO-DON	1	0	35	31	10	40	44	.63	0	0
1-56	CLO-LKF	-	-	-	-	-	-	-	-	-	-
1-57	CLO-LKF	3	1	34	33	8	42	47	.91	2	3
1-58	FEL-HIN	-	-	-	-	-	-	-	-	-	-
1-59	FEL-HIN	7	6	29	31	6	51	45	.63	1	31
1-60	FEL-CLO	10	9	37.5	34	5	52	46	.56	4	2
1-61	FEL-HUM	-2	-3	33	39.5	15	42	41	1.19	5	7
1-62	FEL-PAT	-	-	-	-	-	-	-	-	-	-
1-63	FEL-MRE	2	1	33.5	33	12	41	38	1.54	5	5
1-64	FEL-SCH	2	2	29.5	32	5	39	65	1.12	1	1
1-65	FEL-MAM	0	0	26.5	31	8	53	42	.82	0	0
1-66	FEL-DON	3	2	37	40	1	49	44	.72	0	0
1-67	FEL-LKF	-1	-1	44	41	4	54	41	.91	0	0
1-68	HIN-CLO	10	10	28.5	27	15	48	48	.56	0	2
1-69	HIN-FEL	0	0	29	30	14	45	45	.56	0	10
1-70	HIN-HUM	2	1	30.5	28	12	43	42	1.06	0	3
1-71	HIN-PAT	9	7	16	24	10	39	48	1.19	4	10
1-72	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-73	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-74	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-75	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-76	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-77	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-78	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-79	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-80	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-81	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-82	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-83	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-84	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-85	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-86	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-87	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-88	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-89	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-90	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-91	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-92	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-93	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-94	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-95	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-96	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-97	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-98	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-99	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-100	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-101	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-102	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-103	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-104	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-105	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-106	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-107	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-108	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-109	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-110	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-111	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-112	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-113	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-114	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-115	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-116	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-117	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-118	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-119	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-120	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-121	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-122	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-123	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-124	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-125	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-126	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-127	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-128	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-129	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-130	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-131	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-132	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-133	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-134	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-135	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-136	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-137	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-138	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-139	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-140	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-141	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-142	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-143	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-144	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-145	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-146	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-147	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-148	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-149	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-150	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-151	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-152	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-153	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-154	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-155	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-156	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-157	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-158	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-159	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-160	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-161	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-162	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-163	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-164	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-165	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-166	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-167	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-168	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-169	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-170	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-171	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-172	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-173	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-174	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-175	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-176	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-177	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-178	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-179	HIN-SCH	6	6	38	38	2	54	47	.49	-	-
1-180	HIN-DON	3	3	32.5	30.5	6	60	60	.00	0	0
1-181	HIN-LKF	6	5	34.5	37	4	51	43	.76	-	-
1-182	HIN-PAT	-4	-4	32	33	17	40	41	.89	0	9
1-183	HIN-MRE	9	9	28.5	27.5	12	42	43	.71	-	-
1-184	HIN-SCH	6	6	38	3						

Table C-1. European IST Loops (Sheet 2 Continued)

Loop #	Circuit #	Location (Abbrev.)	Line Loss (Data)	Line Loss (1 kHz)	Line Loss (10 kHz)	S/N (11 Hz)	HD 2nd	HD 3rd	HD 6th	PH 208	GH 3	PH 63	O	TERNARY ROUTINGS			NON-ENGINEERED ROUTINGS							
														Type of Pictures	Location of Recording	Type of Recording	Type of Pictures	Location of Recording	Type of Recording					
1-77	106	FEL-HUM	3	2	38	39	2	49	43	.79	0	0	9	6	2	0	AD	3-1,000	A-8	FEL 9ACD V2 HIN	9CMR S3 HUM	V2	1-77	
1-78	172	HIN-HUM	6	6	25	25.5	18	43	49	.45	-	-	-	-	-	-	ABD	4-1,057	A-10	HIN 9ACD V2 FEL	9CEO S3 HUM	V2	1-78	
1-79	174	HIN-DON	4	4	38	40	2	54	45	.60	-	-	-	-	-	-	AD	4-1,088	A-1	HIN 9ACD V2 FEL	9CFZ V2 DON	V2	1-79	
1-80	173	HIN-DON	-	-	-	-	-	-	-	-	-	-	-	-	-	-	HIN 9ACD V2 FEL	-	-	DON	-	1-80		
<hr/>																								
1-81	43	CLO-HIN	-2	-4	33	32	9	49	41	.89	3	9	268	83	27	0	A	1-2,270	A-6	CLO 9CVU V2 DON	9DTY V2 MAM	V2	1-81	
1-82	45	CLO-HIN	-4	-4	35	33	8	40	32	2.70	0	0	157	56	14	0	AD	1-2,320	A-7	CLO 9CVS S3 MRE	-	HUM	V2	1-82
1-83	81	FEL-HIN	12	9	23	26	13	37	42	1.62	1	6	1789	877	44	1	A	2-2,104	B-4	FEL 9CFIC V2 HIN	9CMT V2 HIN	V1	1-83	
1-84	134	FEL-HIN	3	2	30.5	28.5	15	-	-	-	-	-	-	-	-	-	FEL 9CFB V2 DON	-	-	HUM	-	1-84		
1-85	132	FEL-HIN	-2	-3	27.5	26	14	38	39	1.69	15	140	1787	1322	314	13	A	3-1,441	C	FEL 9CEP V2 MRE	9AEA V2 MIN	V1	1-85	

Topic C-2: External Access Loops (Sheet 1)

Table C-2. European Access Loops (Sheet 1 Continued)

Table C-2. European Access Loops (Sheet 2)

Table C-2. European Access Loops (Sheet 2 Continued)

Table	Call #	Location (Abbrev.)	Line Loss (Dots)	Line Loss (1 kHz)	S/N (DBR)	S/N (1 kHz)	Pj <sub>0</sub>	HD 2nd	HD 3rd	HD %	G/H +3	PH 200	DG	Types of Pictures	Location of Recording	Type of Recording	Routing	Comments	Line Character	Table #		
2-26	145	HIN-CRO	2	2	37	36	.56	45	.58	0	0	315	10	4	0	A	3-2,113	A-1	HIN 9ECX V2 CRO	S1	2-26	
2-27	147	HIN-CRO	2	2	38	38	.56	58	.20	0	0	9	2	1	0	A	3-2,142	C	HIN 33JMB3-10 CRO	S1	2-27	
2-28	139	HIN-CKS	0	3	51	50.5	0	52	40	1.03	0	0	0	0	0	A	3-2,027	B-4	HIN 9DPC V2 CKS	V2	2-28	
2-29	140	HIN-MIL	0	-1	54	46	1	51	.51	.40	0	0	5	2	0	0	A	3-2,041	C	HIN 9DW8 V2 MIL	S2	2-29
2-30	141	HIN-LDR	2	0	38.5	37	3	42	.38	1.49	0	0	35	20	3	0	A	3-2,046	A-9	HIN 9AKL V2 LDR	V2	2-30
2-31	148	HIN-LDR	1	-	36.5	29	2	47	.50	.55	0	0	199	16	3	0	A	3-2,150	C	HIN 9BUV V2 LDR	S1	2-31
2-32	142	HIN-UHD	-1	0	38	32	6	49	.41	.96	0	0	74	38	26	1	A	3-2,066	C	HIN 9DNQ S3 UHD	S1	2-32
2-33	145	HIN-LDN	3	2	42	43	.5	54	.39	1.14	0	0	0	0	0	A	3-2,075	A-10	HIN 9DCL V2 LDN	V1	2-33	
2-34	146	HIN-LDN	4	3	47	45	2	61	.60	.13	0	0	0	0	0	A	3-2,136	C	HIN 33EMAS-10 LDN	S2	2-34	

Table C-3: European Remote Access Losses (Sheet 1)

**Table C-3.** European Remote Access Loops (Sheet 2)

Table C-3. European Remote Access Loops (Sheet 2 Continued)

Loop No.	Cable ID	Loop Type	Loop Location	Type of Recording	Recording of Routing	Comments	
						Line Loss (dB/100m)	Line Loss (dB/100m)
3-19	84	FEL-RSN	2 1	45	.37	4	51
						46	.57
						1 0	.29
						0 0	0
						1 A	1 A
						2-2,146	A-10
						FEI 44CM4A-3	V2
						DON WGNI VI RSN	3-19
3-20	85	FEL-CRO	1 1	44	.39	6	51
						.57	.31
						0 0	0 4
						3 3	0 A
						0 0	0 A
						0 0	0 A
						2-2,170	C
						FEI 34JMAA-4	HIN 9GTN D1 CRO
						HIN WEFV VI LAH	SI
3-21	87	FEL-LAH	4 3	43	42.5	4	56
						.48	.43
						0 0	0 0
						0 0	0 0
						0 0	0 0
						2-2,207	C
						FEI 34JMAA-4	HIN WEFV VI LAH
						SI	3-21
3-22	88	FEL-YCA	12 12	27	25	14	47
						**	**
						.45	**
						**	**
						**	**
						**	**
						**	**
						**	**
						**	**
						**	**
						**	**
3-23	114	FEL-YCA	16	-	-	-	-
						-	-
						-	-
						-	-
						-	-
						-	-
						-	-
						-	-
3-24	115	FEL-YCA	6 5	33	32	9	47
						.43	.84
						0 0	1 0
						1941	1993 1883
						1 A	3-1,102
						1 A	A-10
						0 A	4-2,030
						0 A	A-4
						0 A	HIN 9ACJ S2 FEL 44CZG1-4 BRN
						0 A	SI
3-25	183	HIN-BRN	6 6	37	38	5	56
						.51	.32
						1 4	1 1
						5 3	5 3
						0 A	4-2,030
						0 A	A-4
						0 A	HIN 9ADP S2 LKF 9CJN V2 SCH
						0 A	SI
						0 A	3-25
3-26	226	HIN-SPM	10 10	36	32	16	48
						.39	1.19
						3 24	228
						200 172	7
						A 6	5-1,391
						5-1,391	A-5
						9BRM SPM	199/200

**Table C-4.** European One-Way IST Calls (Sheet 1)

Table C-4. European One-Way IST Calls (Sheet 2)

Order	Species	Common Name	Color	Length (mm)	Weight (g)	Males	Females	Young	Total	Recordings		Recordings		Recordings		Recordings		Recordings					
										♂	♀	♂	♀	♂	♀	♂	♀	♂	♀				
4-1	37	CLO-HIN	-1	-1	.35	.34	.7	.47	.50	.55	0	1	.52	.42	.29	0	A8C	—	HIN 9ACF S3 FEL 9CUX V2 CLO	S1	4-1		
4-2	38	CLO-HIN	-3	-3	.37	.33	.10	.50	.51	.42	0	0	.19	.17	.13	0	A8	—	HIN 9ACF S3 FEL 9CVD S3 CLO	S1	4-2		
4-3	135	FEL-HIN	1	0	.48	.48	1	.55	.55	.25	0	0	0	0	0	0	A	3-1,489	A-9	HIN 9ACF S3 FEL	S3	4-3	
4-4	40	CLO-HIN	-1	-1	.39	.37	.7	.48	.37	.46	1	22	.215	.103	.38	0	A8C	1-2,180	A-2,3	HIN 9CMN S3 HUM 9CHL S3 MRE 9CVR S3 CLO	V2	4-4	
4-5	44	CLO-HIN	-5	-5	.39	.36	.6	.44	.36	.70	0	0	.89	.24	.6	0	AD	1-2,293	A-!	HIN 9CAMP S3 HUM — — MRE 9CVS S3 CLO	V2	4-5	
4-6	48	CLO-HIN	-5	-5	.39	.36	.6	.40	.40	.41	0	0	.62	.10	.2	0	A	—	—	HIN 9CMN S3 HUM — — MRE 9CVM V2 CLO	S3	4-6	
4-7	42	CLO-HIN	3	2	.34	.34	7	—	.50	.32	0	2	.320	.98	.20	0	A	1-2,246	A-4	HIN 9CWA S3 MAM 9DTY V2 DON 9CVU V2 CLO	S3	4-7	
4-8	46	CLO-HIN	3	3	.30	.30	.12	—	.44	.63	0	6	.1275	.64	.9	0	A	1-2,351	A-2,34	HIN 9AEC V2 MRE 9DGF S3 CLO	V2	4-8	
4-9	50	CLO-HIN	2	2	.41	.41	.5	11	.48	.45	.69	0	.0	.3	1	0	C	—	1-2,457	A-5,6	HIN 9ACH S3 FEL 9CLW S3 CLO	—	4-9
4-10	52	CLO-HIN	3	2	.39	.32	.17	.52	.46	.56	0	1	.28	.17	.9	0	AB	2-1,000	A-8	HIN 9ACG S3 FEL 9CLW S3 CLO	S1	4-10	
4-11	72	FEL-HIN	1	1	.46,5	.47,5	4	.55	.55	.25	1	0	.3	.3	.2	1	A	2-1,476	A-1	HIN 9ACF S3 FEL	S3	4-11	
4-12	76	FEL-HIN	0	1	.44	.45,5	4	—	.51	.28	0	0	0	0	0	0	A	2-2,055	A-2	HIN 9ACL S3 FEL	S3	4-12	
4-13	78	FEL-HIN	1	0	.35	.34	6	—	.48	.40	0	0	.49	.27	0	0	A	2-2,059	A-3	HIN 9CLM S3 MAM 9CKD S3 FEL	S3	4-13	
4-14	129	FEL-HIN	4	4	.31	.30	8	.47	.45	.72	0	3	.293	.86	.30	2	A	3-1,341	A-6	HIN 9CLL S3 MAM 9EPR V2 FEL	S3	4-14	
4-15	86	FEL-HIN	7	8	.29	.29	9	.40	.46	.112	0	0	.1442	.3110	.26	0	A	2-2,087	A-4	HIN 9CMF V2 HUM 9DQV V2 DON 9FCF V2 FEL	V2	4-15	
4-16	133	FEL-HIN	5	4	.23,5	.25	.12	—	.41	.89	.33	3	.1759	.175	.12	1	A	3-1,450	A-8	HIN 9CMR S3 HUM — — DON 9EFB V2 FEL	V2	4-16	
4-17	149	HIN-CLO	-5	-6	.34,5	.34	.6	.53	.44	.67	0	0	.127	.31	.9	0	A	—	—	CLO 9CYN V2 MRE — — HUM	V2	4-17	
4-18	153	HIN-CLO	4	3	.34	.33,5	.5	.47	.50	.55	1	2	.498	.116	.16	0	A	3-2,209	A-2	CLO 9CYN V2 MRE 9AEC S3 HIN	V2	4-18	
4-19	151	HIN-CLO	-3	-4	.35,5	.33	.10	.51	.42	.84	0	7	.298	.57	.7	1	AC	3-2,138	A-1	CLO 9CYN V2 MRE 9ALA V2 HIN	V2	4-19	
4-20	131	HIN-CLO	1	1	.26	.27	.13	.32	.40	.27	10	.62	.1816	.1389	.286	6	A	3-1,401	A-7	HIN 9AEA V2 MRE 9CEP V2 FEL	V2	4-20	
4-21	155	HIN-CLO	2	1	.39	.35	.7	.55	.50	.36	0	1	.12	.7	.3	1	A	3-2,258	A-3	CLO 9CUY S3 FEL 9ACF S3 HIN	V2	4-21	

### Table C-5. Trans - Atlantic Calls (Sheet 1)

ID	Name	Location	NATO 1		NATO 2		INTELSAT		Sync		Sync+Hin	
			Lat	Long	Lat	Long	Lat	Long	Lat	Long	Lat	Long
5-1	Ft. Dietrich, Md - Hillington, Eng	12°1' 2155	6.39E-3	0	100	2	0	0	0	0	6.39E-3	9.83E-3
5-2	Ft. Dietrich, Md - Hillington, Eng	12°1' 2218	2.04E-1	-	-	-	-	-	2.04E-1	-	-	2.53E-1
5-3	Ft. Dietrich, Md - Hillington, Eng	12°1' 1751	4.46E-3	0	100	2	0	0	0	0	4.46E-3	4.81E-3
5-4	Ft. Dietrich, Md - Hillington, Eng	12°1' 1805	1.92E-1	-	-	-	-	-	1.92E-1	-	-	2.22E-1
5-5	Ft. Dietrich, Md - Hillington, Eng	11°30' 1337	4.02E-3	1.75E-5	99	0	2	0	0	0	4.02E-3	4.08E-3
5-6	Ft. Dietrich, Md - Hillington, Eng	11°30' 1601	2.37E-1	-	-	-	-	-	2.37E-1	-	-	2.37E-3
5-7	Ft. Dietrich, Md - Hillington, Eng	11°30' 1625	2.40E-2	0	100	0	2	0	0	0	2.40E-2	1.87E-2
5-8	Ft. Dietrich, Md - Hillington, Eng	11°30' 1648	1.87E-1	-	-	-	-	-	1.87E-1	-	-	1.87E-2
5-9	Ft. Dietrich, Md - Hillington, Eng	12°2' 2137	4.87E-3	1.12E-5	98	0	2	0	0	0	4.87E-3	5.84E-3
5-10	Ft. Dietrich, Md - Hillington, Eng	12°2' 2158	2.44E-1	-	-	-	-	-	2.44E-1	-	-	2.51E-1
5-11	Ft. Dietrich, Md - Hillington, Eng	12°1' 2220	2.62E-3	0	100	0	2	0	0	0	2.62E-3	3.69E-3
5-12	Ft. Dietrich, Md - Hillington, Eng	12°1' 2240	2.66E-1	-	-	-	-	-	2.66E-1	-	-	No Sync
5-13	Ft. Dietrich, Md - Hillington, Eng	12°2' 2020	1.30E-2	0	100	0	2	0	0	0	1.30E-2	1.45E-2
5-14	Ft. Dietrich, Md - Hillington, Eng	12°2' 2040	2.44E-1	-	-	-	-	-	2.44E-1	-	-	2.76E-1
5-15	Ft. Dietrich, Md - Hillington, Eng	12°1' 1950	2.37E-2	5.00E-6	98	0	0	0	2	0	2.37E-2	2.81E-2
5-16	Ft. Dietrich, Md - Hillington, Eng	12°1' 2015	1.51E-1	-	-	-	-	-	1.51E-1	-	-	1.76E-1
5-17	Ft. Dietrich, Md - Hillington, Eng	12°2' 1944	1.61E-2	1.37E-5	94	0	0	0	2	0	1.61E-2	1.76E-2
5-18	Ft. Dietrich, Md - Hillington, Eng	12°2' 2005	1.02E-1	-	-	-	-	-	1.02E-1	-	-	1.11E-1
5-19	Ft. Dietrich, Md - Hillington, Eng	12°1' 2123	1.33E-2	1.00E-5	95	0	0	0	2	0	1.33E-2	1.66E-2
5-20	Ft. Dietrich, Md - Hillington, Eng	12°1' 2141	1.34E-1	-	-	-	-	-	1.34E-1	-	-	1.65E-1
5-21	Ft. Dietrich, Md - Hillington, Eng	12°1' 1551	3.39E-3	8.75E-6	99	0	0	0	2	0	3.39E-3	3.80E-3
5-22	Ft. Dietrich, Md - Hillington, Eng	12°1' 1610	8.99R-2	-	-	-	-	-	8.99E-2	-	-	1.01E-1
5-23	Ft. Dietrich, Md - Hillington, Eng	12°2' 1650	1.14E-2	1.25E-6	98	0	0	0	2	0	1.14E-2	1.28E-2
5-24	Ft. Dietrich, Md - Hillington, Eng	12°2' 1707	9.34E-2	-	-	-	-	-	9.34E-2	-	-	1.36E-1
5-25	Ft. Dietrich, Md - Hillington, Eng	12°1' 1930	1.82E-3	0	100	0	0	0	2	0	1.82E-3	2.05E-3
5-26	Ft. Dietrich, Md - Hillington, Eng	12°1' 1950	3.71E-2	-	-	-	-	-	3.71E-2	-	-	3.99E-2

**Table C-5.** Trans-Atlantic Calls (Sheet 1 Continued)

Table C-5. Trans-Atlantic Calls (Sheet 1 Continued)

Call No.	Date	Location	Trans-Atlantic Calls												
			BBP	BTP	NATO 1	NATO 2	TAT I	TAT II	TAT III	TAT IV	TAT V	BER (B)	BER (T)	BER (U)	
5-53	135	Ft. Dietrich, Md - Hittingdon, Eng	12.2	1640	8.50E-2	-	0	0	0	0	0	8.50E-2	-	-	1.05E-1
5-54	208	Ft. Dietrich, Md - Hittingdon, Eng	12.1	1646	1.12E-3	0	100	0	0	0	0	1.12E-3	1.81E-3	2.39E-3	1.86E-3
5-55	207	Ft. Dietrich, Md - Hittingdon, Eng	12.1	1705	3.48E-2	-	0	0	0	0	0	3.48E-2	-	-	5.27E-2
5-56	238	Ft. Dietrich, Md - Hittingdon, Eng	12.2	1721	6.54E-4	0	100	0	1	0	0	6.54E-4	3.01E-3	1.02E-3	1.12E-3
5-57	239	Ft. Dietrich, Md - Hittingdon, Eng	12.2	1743	3.39E-2	-	0	0	2	0	0	3.39E-2	-	-	2.87E-2
5-58	198	Ft. Dietrich, Md - Hittingdon, Eng	11/30	2133	4.24E-4	0	100	0	0	0	0	4.24E-4	2.32E-4	4.12E-4	5.70E-4
5-59	199	Ft. Dietrich, Md - Hittingdon, Eng	11/30	2150	1.97E-2	-	0	0	2	0	0	1.97E-2	-	-	2.01E-2
5-60	196	Ft. Dietrich, Md - Hittingdon, Eng	11/30	2030	1.73E-3	0	100	0	0	0	0	1.73E-3	2.14E-3	3.05E-3	2.78E-3
5-61	197	Ft. Dietrich, Md - Hittingdon, Eng	11/30	2044	4.25E-2	-	0	0	2	0	0	4.25E-2	-	-	4.62E-2
5-62	218	Ft. Dietrich, Md - Hittingdon, Eng	12/1	2056	8.72E-4	0	100	0	0	0	0	8.72E-4	9.58E-4	1.38E-3	1.42E-3
5-63	219	Ft. Dietrich, Md - Hittingdon, Eng	12/1	2115	8.25E-2	-	0	0	2	0	0	8.25E-2	-	-	1.45E-1

Table C-5. Trans-Atlantic Calls (Sheet 2)

Call	Abbrev.	Line Loss (DBm)	Line Loss (dBc)	S/N (1 KHz)	S/N (100 Hz)	HD 3rd	HD 2nd	HD %	G/H %	P/H 2nd	59	63	67	8	Comments
Line	Character									Type of Recording	Location of Picture	Recording	Routing		Table
5-1	222	FTD-HIN	3	-2	38	30	9	44	35	1.88	0	0	1173	3	V2
5-2	223	Looped	3	1	33.5	28	11	38	29	3.76	-	-	-	A	5-1
5-3	210	FTD-HIN	1	1	37	29.5	5	38	2.17	0	0	1467	3	V1	
5-4	211	Looped	-2	-3	33	27	6	36	27	4.74	-	-	A	—	5-2
5-5	186	FTD-HIN	2	1	36	34	7	40	35	2.04	-	-	AD 4-2,397 A-8	FTD — CED 8486 V2 HIN	
5-6	187	Looped	1	0	27	29	10	37	29	3.82	-	-	A	—	Same as 222
5-7	188	FTD-HIN	1	-2	34.5	33	8	44	36	1.71	0	0	47	16	V2
5-8	189	Looped	-2	-1	26	30	10	38	30	3.40	-	-	A	—	5-3
5-9	248	FTD-HIN	-1	-3	37	35	5	41	35	1.99	0	0	14	10	V1
5-10	249	Looped	-4	-4	33	-	8	35	28	4.14	-	-	A	—	5-4
5-11	224	FTD-HIN	0	-1	33	32.5	8	42	36	1.77	0	0	157	29	V1
5-12	225	Looped	0	-2	28	30	10	38	29	3.76	-	-	A	—	5-5
5-13	244	FTD-HIN	1	1	33	28	7	31	32	3.77	0	0	1692	74	V1
5-14	245	Looped	-2	-2	28	27	8	35	26	5.32	-	-	A	—	5-6
5-15	214	FTD-HIN	-1	1	36	24	13	38	27	4.64	0	0	1874	1965	V1
5-16	215	Looped	-3	-1	27	22	17	29	22	8.70	-	-	A	—	5-7
5-17	242	FTD-HIN	1	2	33.5	35	10	34	33	2.99	0	0	1839	1892	V1
5-18	243	Looped	-1	0	28	21	14	41	24	6.37	-	-	A	—	5-8
5-19	220	FTD-HIN	2	1	30.5	25	12	34	1.99	0	0	1864	1685	V1	
5-20	221	Looped	-2	-1	25.5	23	13	32	26	5.61	-	-	A	—	5-9
5-21	204	FTD-HIN	2	2	32	32	5	44	31	2.89	0	4	270	0	V1
5-22	205	Looped	0	-1	23	27	8	43	26	5.06	-	-	A	—	5-10
5-23	236	FTD-HIN	-5	-5	32.5	25	10	37	37	1.99	0	0	1864	1735	V1
5-24	237	Looped	-4	-5	26.5	25	13	38	28	4.17	-	-	A	—	5-11
5-25	212	FTD-HIN	4	3	28	29.5	6	40	35	2.04	0	0	1394	7	V1
5-26	213	Looped	5	6	23.5	25	10	36	26.5	4.99	-	-	A	—	5-12

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Table C-5. Trans-Atlantic Calls (Sheet 2 Continued)

Call	Location	Line Loss (Dots)	Line Loss (1 kHz)	S/N (1 kHz)	P <sub>0</sub>	H20 <sub>0</sub>	G <sub>0</sub>	H2 <sub>0</sub>	G <sub>0</sub>	H20 <sub>0</sub>	G <sub>0</sub>	H2 <sub>0</sub>	G <sub>0</sub>	Type of Recording	Recording of	Line Character	Comments	Table			
5-27	216 FTD-HIN	4	3	30	25	12	38	1.26	0	1848	1743	3	0	A	5-1,000 A-1	FTD	CED 8478 S3 HIN	V2	5-27		
5-28	217 Looped	5	6	25	22	17	29	3.55	-	-	-	-	-	A	—	-	Some as 216	V2	5-28		
5-29	218 FTD-HIN	1	1	36	33	5	43	31	2.91	0	0	9	1	1	0	A	4-2,280 A-4	FTD	CED 8482 S3 HIN	S1	5-29
5-30	219 Looped	-2	-	26	30	7	47	25	5.64	-	-	-	-	A	—	-	Some as 202	V2	5-30		
5-31	220 FTD-HIN	1	0	36	35	5	42	34	2.15	0	0	0	0	0	A	5-1,137 A-7	FTD	CED 8482 S3 HIN	S1	5-31	
5-32	220 Looped	-2	-3	36	39	7	35	27	4.81	-	-	-	-	A	—	-	Same as 229	V2	5-32		
5-33	190 FTD-HIN	2	2	35	34	4	42	35	1.95	0	0	402	286	112	0	AD	4-2,135 A-8	FTD	CED 8485 S3 HIN	S1	5-33
5-34	191 Looped	-2	-2	29	30	7	35	26	5.32	-	-	-	-	A	—	-	Some as 190	V2	5-34		
5-35	227 FTD-HIN	2	2	36	33	4	41	33	2.41	0	C	80	0	0	A	5-1,116 A-6	FTD	CED 8485 S3 HIN	S1	5-35	
5-36	228 Looped	-	-	-	-	-	-	-	-	-	-	-	-	A	—	-	Some as 227	-	5-36		
5-37	192 FTD-HIN	2	2	36.5	33.5	5	40	35	2.04	0	0	20	2	1	0	A	4-2,154 A-9	FTD	POT 8439 S3 HIN	V2	5-37
5-38	193 Looped	-1	-2	28	28	8	30	27	5.47	-	-	-	-	A	—	-	Some as 193	V2	5-38		
5-39	200 FTD-HIN	2	0	36	33	6	35	1.77	0	4	18	0	0	A	4-2,257 A-3	FTD	POT 8439 S3 HIN	V2	5-39		
5-40	201 Looped	-2	-3	28	29	10	34	28	4.45	-	-	-	-	A	—	-	Some as 200	V2	5-40		
5-41	194 FTD-HIN	-5	-5	37.5	32	6	35	33	2.85	0	0	411	133	28	0	A	4-2,176 A-10	FTD	POT 8438 S3 HIN	S1	5-41
5-42	195 Looped	-7	-5	26	24	11	34	25	5.97	-	-	-	-	A	—	-	Some as 19+	V2	5-42		
5-43	222 FTD-HIN	4	4	33.5	25	10	42	40	1.28	2	42	1820	1805	21	31	A	5-1,159 A-8	FTD	POT 8434 S3 HIN	S1	5-43
5-44	223 Looped	3	3	28	22	15	32	25	6.15	-	-	-	-	A	—	-	Some as 232	V2	5-44		
5-45	220 FTD-HIN	0	0	32	25	8	28	31	4.88	0	0	1880	1856	0	0	AC	5-1,260 A-2	FTD	POT 8431 S3 HIN	V2	5-45
5-46	221 Looped	0	0	30	23	11	29	24	7.28	-	-	-	-	A	—	-	Some as 240	V1	5-46		
5-47	226 FTD-HIN	-1	0	36	30	7	29	32	4.35	0	0	1644	14	3	0	A	5-1,343 A-5	FTD	CED 8477 S3 HIN	S2	5-47
5-48	227 Looped	-4	-4	32.5	24	10	27	24	7.73	-	-	-	-	A	—	-	Some as 246	V2	5-48		
5-49	228 FTD-HIN	4	4	31	29.5	8	36	32	3.53	0	0	1845	1245	1	1	A	4-2,363 A-7	FTD	POT 2436 S3 HIN	V2	5-49
5-50	229 Looped	-1	-2	27	27	9	38	27	4.64	-	-	-	-	A	—	-	Some as 208	V1	5-50		
5-51	231 FTD-HIN	-	-	-	-	-	-	-	-	-	-	-	-	A	—	-	FTD	POT 8436 S3 HIN	-	5-51	
5-52	234 FTD-HIN	-2	-2	31	27	13	42	30	3.28	0	0	1803	151	2	0	A	5-1,185 A-9	FTD	POT 8437 S3 HIN	S1	5-52

Table C-5. Trans-Atlantic Calls (Sheet 2 Continued)

Call No.	Line Loss (Dots) (1 kHz)	Line Loss (Dots) (1 kHz)	S/N (Dots) (1 kHz)	S/N (Dots) (1 kHz)	Line Loss (Dots) (1 kHz)	Looped	FTD-HIN	HD 2nd	HD 3rd	HD 6th	HD 20th	PH 20th	PH 59	PH 63	PH 67	O	Type of Recording	Type of Recording	Picture of Frequencies	Location of Recoding	Type of Recording	Comments	Character of Tables	Line Character	Comments	Line Character	Character of Tables
5-53	225	Looped	-3	-1	28	26	18	39	26	5.13	-	-	-	-	-	A	-	-	-	-	Some as 234	FTD — POI B435 S3 HIN	V2	5-53	5-53		
5-54	206	FTD-HIN	1	1	33	30	12	40	34	2.23	0	461	1366	159	68	0	A8	4-2,333	A-6	-	-	Some as 206	FTD — CED B476 S3 HIN	V2	5-54	5-54	
5-55	207	Looped	-2	-3	29	27	29	39	27	4.61	-	-	-	-	-	A8	-	-	-	-	-	-	-	-	5-55	5-55	
5-56	238	FTD-HIN	4	4	31	26	6	45	36	1.68	0	0	1444	7	0	0	A	5-1,236	A-1	-	-	Some as 238	FTD — CED B480 S3 HIN	V2	5-57	5-57	
5-57	239	Looped	3	4	27.5	25.5	8	33	27	4.99	-	-	-	-	-	A	-	-	-	-	-	-	-	-	5-58	5-58	
5-58	198	FTD-HIN	5	5	34	32	5	40	35	2.04	0	0	18	0	0	A	4-2,225	A-2	-	-	-	-	-	-	-	5-59	5-59
5-59	199	Looped	3	3	28	29	4	43	25	5.67	-	-	-	-	-	A	-	-	-	-	Some as 198	FTD — CED B483 S3 HIN	V2	5-60	5-60		
5-60	196	FTD-HIN	4	3	32	32	6	35	32	3.07	0	0	35	0	0	AD	4-2,196	A-1	-	-	Some as 196	FTD — CED B479 S3 HIN	V2	5-61	5-61		
5-61	197	Looped	5	5	26	29	7	30	27	5.47	-	-	-	-	-	A	-	-	-	-	-	-	-	-	5-62	5-62	
5-62	218	FTD-HIN	2	2	32.5	30.5	6	43	35	1.91	0	0	649	1	0	A	5-1,019	A-2	-	-	Some as 218	FTD — CED B479 S3 HIN	S1	5-63	5-63		
5-63	219	Looped	2	2	29	28	7	30	27	5.47	-	-	-	-	-	A	-	-	-	-	-	-	-	-	5-63	5-63	

Table C-6. Trans-Pacific Calls (Sheet 1)

Call No.	Date	Location	DSCS		INTELSAT II		HAWAII I		HAWAII II		HAWAII III		Telsat II			
			8/30	8/31	8/30	8/31	8/30	8/31	8/30	8/31	8/30	8/31	8/30	8/31		
6-1	278	Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1245	1.24E-4	3.50E-5	94	0	0	0	1	1.24E-4	5.30E-3	5.94E-3	4-4	
6-2	279	Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1307	1.94E-1	-	0	0	0	0	2	1.94E-1	-	2.22E-1	1-1	
6-3	285	Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1451	1.19E-4	0	100	0	0	0	1	1.19E-4	1.54E-4	3.78E-4	4-4	
6-4	286	Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1512	8.76E-3	-	0	0	0	0	2	8.76E-3	-	1.01E-2	1-1	
6-5	287	Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1533	2.11E-4	0	100	0	0	0	1	2.11E-4	3.58E-4	5.36E-4	4-4	
6-6	288	Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1555	3.02E-2	-	0	0	0	0	2	3.02E-2	-	2.87E-2	1-1	
6-7	302	Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1355	1.68E-3	0	100	0	0	0	1	1.68E-3	2.59E-3	3.61E-3	4-4	
6-8	303	Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1412	6.29E-2	-	0	0	0	0	2	6.29E-2	-	8.17E-2	1-1	
6-9	326	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1520	5.12E-5	0	100	0	0	0	1	5.12E-5	5.12E-5	3.23E-4	3.36E-4	
6-10	327	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1535	1.33E-2	-	0	0	0	0	2	1.33E-2	-	1.58E-2	1-1	
6-11	319	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1319	8.90E-4	0	100	0	0	0	1	8.90E-4	1.05E-3	1.94E-3	1.50E-3	
6-12	320	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1335	5.74E-2	-	0	0	0	0	2	5.74E-2	-	6.94E-2	1-1	
6-13	323	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1417	2.66E-4	0	100	0	0	0	1	2.66E-4	3.77E-4	7.96E-4	7.20E-4	
6-14	324	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1440	1.05E-2	-	0	0	0	0	2	1.05E-2	-	1.07E-2	1-1	
6-15	325	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1448	4.00E-5	0	100	0	0	0	Cable	4.00E-5	1.21E-4	2.15E-4	3-3	
6-16	289	Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1604	1.37E-5	0	100	0	0	0	1	1.37E-5	7.60E-6	1.19E-4	1.16E-4	
6-17	290	Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1623	4.47E-3	-	0	0	0	0	2	4.47E-3	-	4.38E-3	1-1	
6-18	318A	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1310	3.20E-4	-	0	0	0	0	Cable	3.20E-4	-	-	1-1	
6-19	369	Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1618	6.62E-5	0	100	0	0	0	1	6.62E-5	2.75E-5	4.87E-5	4-4	
6-20	310	Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1637	5.39E-3	-	0	0	0	0	2	5.39E-3	-	5.61E-3	1-1	
3-21	321	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1348	9.12E-5	0	100	0	0	0	1	9.12E-5	4.00E-5	9.87E-5	1.16E-4	
6-22	322	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1407	9.38E-3	-	0	0	0	0	2	9.38E-3	-	9.47E-3	1-1	
6-23	330	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1628	5.00E-6	0	100	0	0	1	0	5.00E-6	6.37E-5	1.12E-5	4-4	
6-24	331	Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1640	4.97E-3	-	0	0	0	0	2	0	4.97E-3	-	4.82E-3	1-1
6-25	335	Stockton, Calif. - Pearl Harbor, Hawaii	12/17	1255	3.00E-5	0	100	0	0	0	1	0	3.00E-5	5.42E-5	1.87E-4	1.39E-4
6-26	336	Stockton, Calif. - Pearl Harbor, Hawaii	12/17	1315	8.81E-3	-	0	0	0	0	2	0	8.81E-3	-	-	1-1

Table C-6. Trans-Pacific Calls (Sheet 1 Continued)

Call No.	Location	TELESAT		HAWAII		HAWAII		HAWAII		TELESAT		TELESAT	
		DSCS	DSR	DSR	DSR	DSR	DSR	DSR	DSR	DSR	DSR	DSR	DSR
6-27	298 Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1249	1.74E-4	0	100	0	0	Cable	1.74E-4	4.19E-4	7.59E-4	4-4
6-28	299 Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1314	1.45E-2	-	0	0	0	Cable	1.45E-2	-	1.76E-2	1-1
6-29	303 Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1606	5.24E-4	-	0	0	0	Cable	5.24E-4	6.09E-4	-	2-2
6-30	304 Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1430	5.25E-5	7.25E-5	95	0	1	0	0	5.25E-5	9.37E-5	2.15E-4
6-31	305 Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1458	5.04E-3	-	0	0	2	0	0	5.04E-3	-	4.36E-3
6-32	317 Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1240	6.37E-5	5.00E-6	98	0	0	1	0	0	6.37E-5	1.51E-4
6-33	318 Stockton, Calif. - Pearl Harbor, Hawaii	12/16	1300	3.60E-3	-	0	0	2	0	0	3.60E-3	-	3.66E-3
6-34	267 Stockton, Calif. - Pearl Harbor, Hawaii	12/13	1532	2.25E-5	6.25E-6	99	0	0	1	0	0	2.25E-5	9.00E-5
6-35	268 Stockton, Calif. - Pearl Harbor, Hawaii	12/13	1600	7.37E-3	-	0	0	2	0	0	4.38E-3	-	4.06E-3
6-36	280 Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1319	5.67E-3	0	100	0	0	1	0	0	5.67E-3	5.58E-3
6-37	300 Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1324	1.29E-4	1.75E-5	95	0	1	0	0	1.29E-4	9.38E-5	9.84E-5
6-38	301 Stockton, Calif. - Pearl Harbor, Hawaii	12/15	1344	3.78E-3	-	0	0	2	0	0	3.78E-3	-	3.83E-3
6-39	282 Stockton, Calif. - Pearl Harbor, Hawaii	12/14	1400	1.31E-2	1.71E-4	51	0	0	1	0	0	6.46E-3	7.59E-3
6-40	337 Stockton, Calif. - Pearl Harbor, Hawaii	12/17	1317	5.26E-4	2.50E-4	99	0	1	0	0	5.26E-4	6.84E-4	7.96E-4
6-41	338 Stockton, Calif. - Pearl Harbor, Hawaii	12/17	1343	2.01E-2	-	0	2	0	0	0	2.01E-2	-	1.12E-3
6-42	269 Stockton, Calif. - Pearl Harbor, Hawaii	12/13	1615	2.35E-3	2.50E-4	99	0	1	0	0	2.35E-3	2.95E-3	1.41E-4
6-43	270 Stockton, Calif. - Pearl Harbor, Hawaii	12/13	1640	1.53E-2	-	0	2	0	0	0	1.53E-2	-	1.46E-2

Table C-6. Trans-Pacific Calls (Sheet 2)

**Table C-6.** Trans-Pacific Calls (Sheet 2 Continued)

Table C-7. Pacific IST Loops (Sheet 1)

Loop	Location	PRIMARY ROUTINGS										SECONDARY AND TERNARY ROUTINGS									
		8-110 BBR	8-111 BBR	8-112 BBR	8-113 BBR	8-114 BBR	8-115 BBR	8-116 BBR	8-117 BBR	8-118 BBR	8-119 BBR	8-120 BBR	8-121 BBR	8-122 BBR	8-123 BBR	8-124 BBR	8-125 BBR	8-126 BBR	8-127 BBR	8-128 BBR	8-129 BBR
7-1	252 Pearl Harbor, Hawaii - Fuchi, Japan	12/13 08i7	2.59E-4	0	100	0	0	2	0	2.59E-4	4.66E-4	3.60E-4	2.50E-4	4-4	26	7-1					
7-2	253 Pearl Harbor, Hawaii - Fuchi, Japan	12/13 0848	1.12E-5	0	100	2	0	0	0	1.12E-5	1.62E-5	1.87E-5	3.62E-5	4-4	27	7-2					
7-3	262 Pearl Harbor, Hawaii - Fuchi, Japan	12/13 1234	1.27E-4	0	100	2	0	0	0	1.27E-4	1.82E-4	1.82E-4	1.52E-4	4-4	25	7-3					
7-4	332 Pearl Harbor, Hawaii - Fuchi, Japan	12/17 0753	2.87E-5	0	100	2	0	0	0	2.87E-5	7.37E-5	3.00E-5	5.00E-5	4-4	26	7-4					
7-5	256 Pearl Harbor, Hawaii - Fuchi, Japan	12/13 1359	1.12E-5	0	100	2	0	0	0	1.12E-5	2.27E-4	1.39E-5	2.12E-5	4-4	27	7-5					
7-6	250 Pearl Harbor, Hawaii - Ft. Buckner, Okinawa	12/13 1130	4.46E-4	0	100	0	2	0	0	4.46E-4	6.14E-4	7.87E-4	5.31E-4	4-4	25	7-6					
7-7	271 Pearl Harbor, Hawaii - Ft. Buckner, Okinawa	12/14 0757	1.22E-4	-	0	2	0	0	0	1.22E-4	2.15E-4	1.46E-3	1.06E-3	2-2	26	7-7					
7-8	272 Pearl Harbor, Hawaii - Ft. Buckner, Okinawa	12/14 0806	4.51E-4	0	100	0	2	0	0	4.51E-4	6.22E-4	4.86E-4	4.27E-4	4-4	25	7-8					
7-9	314 Pearl Harbor, Hawaii - Ft. Buckner, Okinawa	12/16 1000	2.55E-3	-	0	2	0	0	0	2.55E-3	-	-	-	1-1	22	7-9					
7-10	254 Pearl Harbor, Hawaii - Ft. Buckner, Okinawa	12/13 0918	4.31E-4	2.50E-4	99	0	2	0	0	4.31E-4	6.15E-4	7.15E-4	5.01E-4	4-4	25	7-10					
7-11	264 Pearl Harbor, Hawaii - Finegeyan, Guam	12/13 1316	5.87E-5	0	100	2	0	0	0	5.87E-5	1.70E-4	4.25E-5	2.25E-5	4-4	28	7-11					
7-12	291 Pearl Harbor, Hawaii - Finegeyan, Guam	12/15 0810	1.56E-3	0	100	0	0	2	0	1.56E-3	1.85E-3	1.93E-3	8.22E-4	4-4	22	7-12					
7-13	316 Pearl Harbor, Hawaii - Finegeyan, Guam	12/16 1030	7.52E-4	0	100	0	0	2	0	7.52E-4	1.20E-3	9.70E-4	7.96E-4	4-4	24	7-13					
7-14	259 Pearl Harbor, Hawaii - Finegeyan, Guam	12/13 1110	1.17E-3	2.50E-4	99	0	2	0	0	1.17E-3	3.54E-4	3.90E-4	3.10E-4	4-4	26	7-14					
7-15	255 Pearl Harbor, Hawaii - Finegeyan, Guam	12/13 0942	3.09E-4	5.00E-6	99	0	2	0	0	3.09E-4	3.57E-4	2.67E-4	2.10E-4	4-4	26	7-15					
7-16	258 Pearl Harbor, Hawaii - Clark, Philippines	12/13 1045	3.12E-5	0	100	2	0	0	0	3.12E-5	1.35E-4	8.12E-5	9.37E-5	4-4	27	7-16					
7-17	265 Pearl Harbor, Hawaii - Clark, Philippines	12/13 1335	3.26E-4	0	100	0	2	0	0	3.26E-4	3.57E-4	4.39E-4	3.29E-4	4-4	25	7-17					
7-18	256 Pearl Harbor, Hawaii - Clark, Philippines	12/13 1002	4.99E-4	0	:00	0	0	2	0	4.99E-4	1.13E-3	6.02E-4	6.33E-4	4-4	24	7-18					
225/226																					
7-19	273 Pearl Harbor, Hawaii - Fuchi, Japan	12/14 0835	5.62E-4	0	100	0	2	0	2	5.62E-4	5.70E-4	5.32E-4	5.42E-4	4-4	25	7-19					
7-20	277 Pearl Harbor, Hawaii - Fuchi, Japan	12/14 1110	3.01E-3	1.77E-3	95	0	2	0	2	3.81E-3	6.67E-3	1.58E-2	5.52E-3	3-3	23	7-20					
7-21	274 Pearl Harbor, Hawaii - Fuchi, Japan	12/14 0958	4.88E-3	0	100	0	2	2	0	4.88E-3	4.06E-3	4.41E-3	4.44E-3	3-3	22	7-21					
7-22	263 Pearl Harbor, Hawaii - Ft. Buckner, Okinawa	12/13 1258	7.03E-3	0	100	0	2	0	2	2.64E-3	2.02E-3	3.20E-3	2.02E-3	3-3	22	7-22					
7-23	315 Pearl Harbor, Hawaii - Ft. Buckner, Okinawa	12/16 1005	9.25E-4	2.50E-6	99	2	0	0	2	9.25E-4	1.32E-3	1.53E-3	1.66E-3	4-4	21	7-23					
7-24	275 Pearl Harbor, Hawaii - Clark, Philippines	12/14 1008	1.03E-3	2.50E-6	99	0	2	0	2	1.03E-3	1.95E-3	1.80E-3	1.95E-3	4-4	24	7-24					
7-25	276 Pearl Harbor, Hawaii - Clark, Philippines	12/14 1037	2.85E-2	4.66E-3	6	0	2	0	2	2.85E-2	2.12E-2	2.51E-2	2.41E-2	5-5	20	7-25					

Table C-7. Pacific IST Loops (Sheet 2)

Loop #	Line ID	Line Label	Line Type	Line ID	Line Label	Line Type	PRIMARY ROUTINGS						Type of Routing	Location of Recording	Pictrue of	Comments		
							P-2	P-3	P-4	P-5	P-6	P-7	P-8	P-9	P-10	P-11		
7-1	252	PHR-FUC	-1	-2	30.5	33	3	44	44	.53	0	0	3	0	0	0	A	P1-1,000 A-8 PHR KC41 S3 WAH KHS5 S3 FUC
7-2	253	PHR-FUC	-2	-3	34	36	2	48	44	.74	0	0	3	0	0	0	A	P1-1,025 A-9 PHR KC41 S3 WAH KH47 S3 FUC
7-3	262	PHR-FUC	-2	-3	34	34	3	46	43	.87	0	0	1	0	0	0	A	P1-1,167 B-3 PHR KC41 S3 WAH — FUC
7-4	332	PHR-FUC	-1	-2	32	34	3	46	43	.87	0	0	3	1	0	0	A	P2-1,234 B-4 PHR KC41 S3 WAH KHS5 S3 FUC
7-5	266	PHR-FUC	-2	-3	34	36	3	50	44	.71	0	0	1	0	0	0	A	P1-1,221 B-4 PHR KC41 S3 WAH KH47 S3 FUC
7-6	260	PHR-BUC	-3	-4	32	34	2	46	37	1.50	C	0	3	1	0	0	A	P1-1,145 B-2 PHR KC41 S3 WAH KKCS S3 FTB
7-7	271	PHR-BUC	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	PHR KC41 S3 WAH — FTB
7-8	272	PHR-BUC	-3	-4	32	34	3	33	37	2.65	0	0	1	0	0	0	A	P1-2,022 B-1 PHR KC41 S3 WAH KK85 S3 FTB
7-9	314	PHR-BUC	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	PHR KC41 S3 WAH — FTB
7-10	254	PHR-BUC	-3	-4	32	34	2	42	39	1.37	0	0	1	0	0	0	A	P1-1,048 B-1 PHR KC41 S3 WAH KK85 S3 FTB
7-11	264	PHR-FIN	-2	-4	35	37	2	47	45	.72	0	6	6	1	1	C	A	P1-1,185 B-4 PHR KC41 S3 WAH KE48 S3 FIN
7-12	291	PHR-FIN	-2	-2	31	31	3	46	39	1.23	0	0	131	0	0	0	A	P1-1,232 B-8 PHR KC41 S3 WAH KE37 S3 FIN
7-13	316	PHR-FIN	-1	-2	31	32	3	50	38	1.30	0	0	21	i	1	0	A	P2-1,090 C PHR KC41 S3 WAH KE46 S3 FIN
7-14	259	PHR-FIN	-2	-2	32	33	3	44	39	1.29	0	0	55	11	3	0	A	P1-1,129 B-9 PHR KC41 S3 WAH KE20 S3 FIN
7-15	255	PHR-FIN	0	-1	31	33	3	43	40	1.08	0	0	35	16	7	0	A	P1-1,065 B-3 PHR KC41 S3 WAH KE19 S3 FIN
7-16	258	PHR-CLK	-2	-3	33	35	4	47	43	.84	0	0	0	0	0	0	A	P1-1,109 B-7 PHR KC41 S3 WAH KP15 S3 CLK
7-17	265	PHR-CLK	-5	-6	32	34	3	47	38	1.34	0	0	2	0	0	0	A	P1-1,202 B-3 PHR KC41 S3 WAH KD75 S3 CLK
7-18	256	PHR-CLK	-2	-3	30	32	4	43	42	1.06	0	0	650	0	0	0	A	P1-1,083 B-5 PHR KC41 S3 WAH KD96 S3 CLK
SECONDARY AND TERNARY ROUTINGS																		
7-19	273	PHR-FUC	-2	-1	32	33	4	49	39	1.16	0	0	8	6	1	1	A	P1-2,037 B-1,B-2 PHR KC41 S3 WAH KK83 BUC
7-20	277	PHR-FUC	-4	-5	33	34	4	45	36	1.68	-	-	-	-	-	-	-	TROPO FUC
7-21	274	PHR-FUC	-2	0	28	32	5	47	39	1.21	-	-	-	-	-	-	-	PHR KC41 S3 WAH KE18 FIN CABLE FUC
7-22	263	PHR-BUC	-5	-5	27	33	4	46	34	2.06	-	-	-	-	-	-	-	PHR KC41 S3 WAH KD73 CLK
																		TROPO BUC

Table C-7. Pacific IST Loops (Sheet 2 Continued)

Call #	Location (Address, etc.)	Line loss (Data)	Line loss (Data)	S/N (Data)	S/N (kHz)	HD 2nd	HD 3rd	PJ <sub>0</sub>	HD 2nd	HD 3rd	GH +3	PH 206	GH -3	00	67	63	59	59	63	67	00	Picture of Recording	Location of Recording	Type of Recording	Routing	Line Character	Comments	Table #
SECONDARY AND TERNARY ROUTINGS (CONTINUED)																												
7-23	315 PHF-BUC	1	-2	33	36	5	45	55	.59	0	2	10	11	2	0	A	P2-1,082	C	PHR KC41 S3 WAH KH48 FUC	TROPO CLK	PHR KC41 S3 WAH KK93 BUC	V1	7-23					
7-24	275 PHK-CLK	0	-1	28	29	5	46	37	1.49	0	0	1418	9	0	0	A	P1-2,062	B-3	PHR KC41 S3 WAH KK93 BUC	TROPO CLK	PHR KC41 S3 WAH KH48 FUC	S1	7-24					
7-25	276 PHR-CLK	-2	-2	25	26	15	36	31	3.23	0	1	1835	1735	1305	0	ABC	P1-2,078	B-4	PHR KC41 S3 WAH KH49 FIN	CABLE CLK	PHR KC41 S3 WAH KH49 FIN	V2	36	7-25				

Table C-8. Pacific Remote Access Loops (Sheet 1)

Case	Location	COMSAT									
		DSCS	Cbde	Trsp	M	RFR	16-110	8-110	8-110	8-110	8-110
8-1 28	Pearl Harbor - Misawa, Japan (Record 58)	12:15	1055	1.42E-3	0	100	2	0	0	4	1.42E-3
8-2 29	Pearl Harbor - Yokosuka, Japan (Record 16)	12:15	1000	1.35E-4	0	100	2	0	0	6	1.35E-4
8-3 31	Pearl Harbor - Yokota, Japan (Record 44)	12:16	0818	2.08E-3	0	100	0	0	2	0	2.08E-3
8-4 29	Pearl Harbor - Seoul, Korea (Record 12)	12:15	1025	8.59E-4	0	100	0	0	0	0	8.59E-4
8-5 29	Pearl Harbor - Kadota, Okinawa (Record 13)	12:15	0940	3.86E-7	3.00E-5	96	0	2	0	2	3.86E-2
8-6 31	Pearl Harbor - Kadota, Okinawa (Record 23)	12:16	0913	6.37E-3	0	100	2	0	0	0	6.37E-3
8-7 328	Pearl Harbor - Clark, Philippines (Record 16)	12:16	1350	9.48E-3	0	100	0	0	2	0	9.48E-3
8-8 29	Pearl Harbor - Taipei, Taiwan (Record 17)	12:15	0855	5.47E-2	1.72E-3	52	0	2	0	0	4.18E-2
8-9 313	Pearl Harbor - Taipei, Taiwan (Record 17)	12:16	0928	5.05E-2	2.36E-4	51	0	2	0	0	5.05E-2

Table C-8. Pacific Remote Access Loops (Sheet 2)

Table	Call	Abbrev.	Line Loss	QdB/Hz	Line Loss	S/N	PJ <sub>0</sub>	HD 2nd	HD 3rd	HD	PH 230	G	59	53	67	D	Types of Pictures	Recording	Type of Recording	Receiving	Transmitter	Comments	
8-1	296	PHR-MIS	-2	-3	32	34	3	46	39	1.23	0	0	3	0	0	0	A	P1-2,302	B-10	PHR KC41 S3 WAH RH48 S3 FUC	—	V2	8-1
8-2	294	PHR-YKS	-3	-4	33	35	3	43	40	1.23	0	0	2	1	0	0	A	P1-2,270	C	PHR KC41 S3 WAH KH50 S3 FUC	—	V2	8-?
8-3	311	PHR-YOK	-1	0	29	30	4	46	46	.71	0	0	565	4	2	0	A	P2-1,939	A-10	PHR KC41 S3 WAH YOK (44)	—	V2	8-3
8-4	295	PHR-SEO	-2	-1	33	29	3	37	35	2.27	0	0	1461	24	8	0	A	P1-2,280	B-8	KC42 S3 WAH KA98 S3 SEO (12)	V1	37	8-4
8-5	293	PHR-KAD	-1	-	29	-	-	-	-	-	-	-	-	-	-	-	—	—	—	PHR KC41 S3 WAH DSCS S3 CLK	—	—	8-5
8-6	312	PHR-KAO	3	3	32	31	5	43	30	3.24	0	0	183	3	1	0	AD	P2-1,048	B-4	PHR KC41 S3 WAH KH49 S3 FUC TROPOV1	FTB — KAD (73)	8-6	
8-7	328	PHR-CLK	-10	-10	27	28	7	46	34	2.06	0	0	1774	239	8	0	A	P2-1,198	B-8	PHR KC41 S3 WAH KD96 S3 CLK	— (16) V2	8-7	
8-8	292	PHR-TAP	-4	-5	30	29	7	33	27	4.99	0	0	1053	19	1	0	ACD	P1-2,251	B-8	PHR KC41 S3 WAH KD75 S3 CLK TROPOV2	TAP (17)	8-8	
8-9	313	PHR-TAP	-3	-5	31	30	9	31	30	4.23	2	0	893	4	1	0	ABCD	P2-1,084	B-5	PHR KC41 S3 WAH KD71 S3 CLK TROPOV1	TAP (17)	8-9	

Table C-9. CONUS 1ST Loops (Sheet 1)

9-1	340	Melbourne, Fla #1 - Polk City, Fla	1/11	1002	6.25E-6	0	160		6.25E-6	2.50E-6	2.50E-6	3-3	29	9-1					
9-2	380	Melbourne, Fla #2 - Polk City, Fla	1/17	0840	1.25E-6	0	100		1.25E-6	0	0	1.12E-5	3-3	30	9-2				
9-3	381	Melbourne, Fla #1 - Ellenville, Fla	1/11	1038	1.62E-5	0	100		1.62E-5	7.50E-6	0	1.62E-5	3-3	30	9-3				
9-4	381	Melbourne, Fla #2 - Ellenville, Fla	1/17	0900	1.55E-4	0	100		1.55E-4	1.60E-4	1.35E-4	1.31E-4	3-3	24	9-4				
9-5	342	Melbourne, Fla #1 - Oranerville, Vir	1/11	1104	2.88E-2	0	100		2.88E-2	2.93E-2	2.92E-2	3.09E-2	3-3	21	9-5				
9-6	382	Melbourne, Fla #2 - Oranerville, Vir	1/17	0920	1.49E-4	0	100		1.49E-4	1.44E-4	2.15E-4	1.71E-4	3-3	25	9-6				
9-7	343	Melbourne, Fla #1 - Brewton, Ala	1/11	1337	4.25E-5	0	100		4.25E-5	8.12E-5	9.25E-5	7.50E-5	3-3	28	9-7				
9-8	383	Melbourne, Fla #2 - Brewton, Ala	1/17	0935	2.00E-5	0	100		2.00E-5	4.37E-5	3.00E-5	3.37E-5	3-3	27	9-8				
9-9	344	Melbourne, Fla #1 - Jasper, Ala	1/11	14C2	5.12E-5	0	100		5.12E-5	1.27E-4	1.64E-4	1.64E-4	3-3	26	9-9				
9-10	384	Melbourne, Fla #2 - Jasper, Ala	1/17	0955	8.25E-5	0	100		8.25E-5	6.32E-5	1.11E-4	8.62E-5	3-3	26	9-10				
9-11	345	Melbourne, Fla #1 - Chatham, N. Car	1/11	1440	3.41E-4	0	100		3.41E-4	7.25E-4	4.39E-4	5.79E-4	3-3	23	9-11				
9-12	385	Melbourne, Fla #2 - Chatham, N. Car	1/17	1010	2.55E-4	2.50E-5	99		2.51E-4	2.54E-4	2.55E-4	2.04E-4	3-3	24	9-12				
9-13	346	Melbourne, Fla #1 - Stanfield, N. Car	1/11	1500	1.56E-4	0	100		1.59E-4	5.72E-3	2.46E-4	2.29E-4	3-3	25	9-13				
9-14	386	Melbourne, Fla #2 - Stanfield, N. Car	1/17	1030	3.54E-3	0	100		3.54E-3	3.70E-3	3.36E-3	3.86E-3	3-3	20	9-14				
9-15	347	Melbourne, Fla #1 - Leesburg, Vir	1/11	1520	1.79E-2	0	100		1.79E-2	1.67E-2	1.94E-2	1.74E-2	3-3	20	9-15				
9-16	387	Melbourne, Fla #2 - Leesburg, Vir	1/17	1045	6.28E-3	0	100		6.28E-3	7.66E-3	7.75E-3	6.19E-3	3-3	19	9-16				
9-17	348	Melbourne, Fla #1 - Charlottesville, Vir	1/12	0803	4.75E-3	1.25E-6	99		4.74E-3	5.25E-3	4.73E-3	5.00E-3	3-3	21	9-17				
9-18	388	Melbourne, Fla #2 - Charlottesville, Vir	1/17	1420	4.94E-3	0	100		4.54E-3	5.57E-3	5.11E-3	5.38E-3	3-3	19	9-18				
9-19	349	Melbourne, Fla #1 - Mosely, Vir	1/12	0824	1.65E-4	0	100		1.65E-4	3.16E-4	2.11E-4	2.17E-4	3-3	24	9-19				
9-20	389	Melbourne, Fla #2 - Mosely, Vir	1/24	1015	3.06E-3	0	100		3.08E-3	4.35E-3	3.22E-3	3.11E-3	3-3	22	9-20				
9-21	350	Melbourne, Fla #1 - Williamsburg, Ken	1/12	0845	4.50E-3	0	100		4.50E-3	4.61E-3	4.20E-3	4.90E-3	3-3	22	9-21				
9-22	390	Melbourne, Fla #2 - Williamsburg, Ken	1/24	1045	4.33E-3	0	100		4.33E-3	6.31E-3	4.13E-3	5.25E-3	3-3	20	9-22				
9-23	351	Melbourne, Fla #1 - Hagerstown, Md	1/12	0905	3.56E-2	4.37E-5	97		3.56E-2	3.98E-2	3.39E-2	4.15E-2	3-3	19	9-23				
9-24	391	Melbourne, Fla #2 - Hagerstown, Md	1/24	1105	3.00E-3	0	100		3.03E-3	4.21E-3	3.21E-3	4.48E-3	3-3	21	9-24				
9-25	352	Melbourne, Fla #1 - Toledo Junction, Ohio	1/12	0930	2.99E-3	4.25E-5	92		2.99E-3	3.60E-3	3.29E-3	3.10E-3	3-3	22	9-25				
9-26	392	Melbourne, Fla #2 - Toledo Junction, Ohio	1/24	1215	7.40E-4	0	100		7.40E-4	9.65E-4	1.25E-3	9.44E-4	3-3	24	9-26				

Table C-9. CONUS IST Loops (Sheet 1 Continued)

Table C-9. CONUS IST Loops (Sheet 1 Continued)

9-53	368	Melbourne, Fla #1 - Apache Junction, Ariz	1/12	1545	2.75E-2	0	100			2.75E-2	3.16E-2	2.91E-2	3.05E-2	3-3	3-3	17	9-53
9-54	436	Melbourne, Fla #2 - Apache Junction, Ariz	1/25	0820	7.89E-3	0	100			7.89E-3	8.24E-3	8.63E-3	7.70E-3	3-3	3-3	20	9-54
9-55	349	Melbourne, Fla #1 - Cheyenne Mountain, Col	1/13	0800	5.24E-3	0	100			5.24E-3	6.24E-3	5.83E-3	5.90E-3	3-3	3-3	21	9-55
9-56	407	Melbourne, Fla #2 - Cheyenne Mountain, Col	1/25	0840	4.78E-3	2.37E-5	99			4.78E-3	5.99E-3	5.29E-3	5.47E-3	3-3	3-3	21	9-56
9-57	370	Melbourne, Fla #1 - Lamar, Col	1/13	0825	5.02E-3	0	100			5.02E-3	6.07E-3	5.43E-3	5.29E-3	3-3	3-3	22	9-57
9-58	408	Melbourne, Fla #2 - Lamar, Col	1/25	0900	8.49E-3	4.87E-5	94			8.49E-3	1.00E-2	9.65E-3	1.19E-2	3-3	3-3	20	9-58
9-59	371	Melbourne, Fla #1 - Mounds, Okla	1/13	0915	1.98E-2	0	100			1.98E-2	5.82E-3	5.48E-3	5.16E-3	3-3	3-3	23	9-59
9-60	409	Melbourne, Fla #2 - Mounds Okla	1/25	0915	7.19E-3	2.50E-6	99			7.19E-3	8.05E-3	7.28E-3	5.62E-3	3-3	3-3	21	9-60
9-61	372	Melbourne, Fla #1 - Lyons, Neb	1/13	0940	6.92E-3	0	100			6.92E-3	7.09E-3	6.18E-3	6.35E-3	3-3	3-3	22	9-61
9-62	410	Melbourne, Fla #2 - Lyons, Neb	1/25	0930	9.62E-3	0	100			9.62E-3	1.13E-2	0.43E-3	8.76E-3	3-3	3-3	21	9-62
9-63	339	Melbourne, Fla #1 - Helens, Mont	1/11	0910	6.23E-3	0	100			6.23E-3	7.59E-3	1.06E-2	7.82E-3	3-3	3-3	18	9-63
9-64	411	Melbourne, Fla #2 - Helens, Mont	1/25	0945	2.91E-2	1.39E-4	94			2.91E-2	3.51E-2	3.38E-2	3.69E-2	3-3	3-3	16	9-64
9-65	373	Melbourne, Fla #1 - Lodi, Cal	1/13	1010	4.12E-3	0	100			4.12E-3	3.94E-3	5.64E-3	3.40E-3	3-3	3-3	22	9-65
9-66	412	Melbourne, Fla #2 - Lodi, Cal	1/25	1000	8.28E-3	0	100			8.28E-3	7.87E-3	6.75E-3	5.84E-3	3-3	3-3	20	9-66
9-67	374	Melbourne, Fla #1 - Julian, Cal	1/13	1030	1.21E-2	5.00E-6	98			1.21E-2	1.37E-2	1.65E-2	1.29E-2	3-3	3-3	19	9-67
9-68	413	Melbourne, Fla #2 - Julian, Cal	1/25	1025	5.91E-3	1.87E-5	99			5.91E-3	6.70E-3	8.01E-3	7.77E-3	3-3	3-3	21	9-68
9-69	375	Melbourne, Fla #1 - Mojave, Cal	1/13	1040	6.30E-3	0	100			6.30E-3	6.98E-3	6.28E-3	6.02E-3	3-3	3-3	22	9-69
9-70	414	Melbourne, Fla #2 - Mojave, Cal	1/25	1035	7.51E-3	0	100			7.51E-3	8.53E-3	7.63E-3	6.77E-3	3-3	3-3	21	9-70
9-71	376	Melbourne, Fla #1 - San Luis Obispo, Cal	1/13	1112	1.12E-2	8.75E-6	98			1.12E-2	2.77E-3	2.69E-3	2.54E-3	3-3	3-3	23	9-71
9-72	415	Melbourne, Fla #2 - San Luis Obispo, Cal	1/25	1055	2.16E-2	0	100			2.16E-2	2.34E-2	2.15E-2	2.15E-2	3-3	3-3	20	9-72
9-73	377	Melbourne, Fla #1 - Smith Falls, Ontar	1/13	1140	3.17E-2	5.00E-6	99			3.17E-2	3.51E-2	3.19E-2	3.71E-2	3-3	3-3	19	9-73
9-74	416	Melbourne, Fla #2 - Smith Falls, Ontar	1/25	1110	2.55E-2	0	100			2.55E-2	3.01E-2	2.72E-2	3.42E-2	3-3	3-3	18	9-74
9-75	378	Melbourne, Fla #1 - Sherbrooke, Quebec	1/13	1150	2.74E-2	5.00E-6	98			2.74E-2	3.05E-2	2.79E-2	3.20E-3	3-3	3-3	19	9-75
9-76	417	Melbourne, Fla #2 - Sherbrooke, Quebec	1/25	1230	2.02E-2	0	100			2.02E-2	2.94E-2	2.08E-2	2.11E-2	3-3	3-3	18	9-76
9-77	379	Melbourne, Fla #1 - Fredericton, Nbrnm	1/13	1220	2.53E-2	3.75E-6	99			2.93E-2	3.31E-2	3.60E-2	3-3	3-3	18	9-77	
9-78	418	Melbourne, Fla #2 - Fredericton, Nbrnm	1/25	1245	3.17E-2	2.50E-6	99			3.17E-2	3.56E-2	3.11E-2	3.26E-2	3-3	3-3	18	9-78

Table C-9. CONUS 1st Loops (Sheet 2)

Table	Call	Location	Line Loss (dB@1 kHz)	S/N (Doppler)	S/N (Z : 1 kHz)	$\rho_{\text{g}}$	HD 2nd	HD 3rd	HD 4th	PH 20°	59	63	67	D	V2	Line Chordal Commens.	Table
9-1	340	MEL-POL	1	1	38.5	40.5	2	48	56	.43	0	0	1	0	0	0	9-1
9-2	380	MEL-POL	0	1	45	40	1	37	48	2.03	0	0	5	5	3	0	9-2
9-3	341	MEL-ELL	1	1	40	40	2	47	56	.47	0	0	2	0	0	0	9-3
9-4	381	MEL-ELL	-1	0	42	28.5	7	39	37	1.80	0	0	163	5	4	0	9-4
9-5	342	MEL-DRA	0	-1	37	28	5	30	31	4.23	0	0	992	3	0	0	9-5
9-6	382	MEL-DRA	-1	1	33	30	5	38	37	1.89	0	0	572	2	1	0	9-6
9-7	343	MEL-BRE	1	1	38	35	2	47	40	1.09	0	0	5	2	0	0	9-7
9-8	383	MEL-BRE	-1	0	39	34	2	38	39	1.26	0	0	15	6	3	0	9-8
9-9	344	MEL-JAS	1	1	38	35	2	48	40	1.07	0	0	5	1	0	0	9-9
9-10	384	MEL-JAS	1	2	37	31	3	40	38	1.61	0	0	15	5	4	0	9-10
9-11	345	MEL-CHA	1	1	36	39	6	40	40	1.41	0	1	29	1	0	0	9-11
9-12	385	MEL-CHA	-1	1	35	30	5	39	38	1.69	0	0	1117	2	0	0	9-12
9-13	346	MEL-STN	2	2	37	35	4	41	41	1.26	0	0	12	2	0	0	9-13
9-14	386	MEL-STN	-10	-9	43	32	8	37	35	2.27	0	0	9	0	0	0	9-14
9-15	347	MEL-LEE	-1	0	38	29	8	34	30	3.74	0	0	792	2	0	0	9-15
9-16	387	MEL-LEE	-1	-1	35.5	28	4	29	49	3.56	0	0	1014	3	1	0	9-16
9-17	348	MEL-CHV	-1	0	39	31	8	39	30	3.35	0	0	488	2	1	0	9-17
9-18	388	MEL-CHV	-3	-2	34.5	30.5	7	38	32	2.81	0	0	598	9	2	0	9-18
9-19	349	MEL-MOS	-1	1	38	30.5	8	35	36	2.38	0	0	519	1	0	0	9-19
9-20	389	MEL-MOS	1	-1	38.5	30	5	40	31	2.99	0	0	20	1	0	0	9-20
9-21	350	MEL-WIL	-2	-1	37.5	31	6	39	30	3.35	0	0	403	14	0	0	9-21
9-22	390	MEL-WIL	0	0	31	28.5	9	40	38	1.61	1	2	1373	16	5	1	9-22
9-23	351	MEL-HAG	-2	-1	35	31	8	38	27	4.64	1	1	920	102	11	0	9-23
9-24	391	MEL-HAG	2	2	30	29	5	40	33	2.45	0	0	1503	15	0	0	9-24
9-25	352	MEL-TOL	3	4	33.5	31	15	42	32	2.63	0	115	78	6	1	0	9-25
9-26	392	MEL-TOL	1	2	34.5	29	4	41	32	2.66	0	0	1219	11	5	0	9-26

Table C-9. CONUS iST Loops (Sheet 2 Continued)

Loop	Loop Revision	Loop ID	Loop Loss (1 kHz)	Loop Loss (DPA)	Loop Loss (DPB)	S/N (1 kHz)	S/N (2 kHz)	S/N (3 kHz)	S/N (4 kHz)	S/N (5 kHz)	S/N (6 kHz)	S/N (7 kHz)	S/N (8 kHz)	S/N (9 kHz)	S/N (10 kHz)	S/N (11 kHz)	S/N (12 kHz)	S/N (13 kHz)	S/N (14 kHz)	S/N (15 kHz)	S/N (16 kHz)	S/N (17 kHz)	S/N (18 kHz)	S/N (19 kHz)	S/N (20 kHz)	Comments	Character Line	Table	
9-27	353	MEL-CED	-1	2	35.5	31.5	4	34	32	3.21	0	0	26	2	0	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-27
9-28	393	MEL-CED	-1	-1	35.5	29	8	37	32	2.88	0	0	1316	13	0	0	0	0	0	0	0	0	0	0	0	0	0	V2	9-28
9-29	354	MEL-NTG	-2	-1	38	29.5	7	39	31	3.03	0	0	156	11	6	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-29
9-30	394	MEL-NTG	-2	-2	39	31	7	39	31	3.03	0	0	897	3	0	0	0	0	0	0	0	0	0	0	0	0	0	V2	9-30
9-31	357	MEL-POT	-1	1	36	27	10	36	29	3.88	0	2	1805	112	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-31	
9-32	395	MEL-POT	-2	-1	34	29	7	40	36	1.87	1	0	1581	16	2	0	0	0	0	0	0	0	0	0	0	0	V2	9-32	
9-33	358	MEL-CHE	-1	-1	38	32	8	39	31	3.03	0	0	75	1	0	0	0	0	0	0	0	0	0	0	0	0	V2	9-33	
9-34	396	MEL-CHE	-1	-1	35	28	7	41	31	2.95	0	0	1271	12	2	0	0	0	0	0	0	0	0	0	0	0	V1	9-34	
9-35	359	MEL-LIT	-1	0	37	30	10	40	32	2.70	0	0	886	7	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-35	
9-36	397	MEL-LIT	-2	-2	27.5	30	6	42	36	3.26	1	0	1486	11	2	0	0	0	0	0	0	0	0	0	0	0	V2	9-36	
9-37	360	MEL-DOV	-1	-1	37	31	10	39	31	3.03	0	0	412	2	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-37	
9-38	398	MEL-DOV	0	-2	33	30	6	39	31	3.03	1	0	1182	19	1	0	0	0	0	0	0	0	0	0	0	0	V2	9-38	
9-39	361	MEL-STV	3	5	34	29	10	39	31	3.03	0	0	1005	1	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-39	
9-40	399	MEL-STV	0	-1	31.5	26	7	29	30	4.19	0	0	1830	184	2	0	0	0	0	0	0	0	0	0	0	0	V1	9-40	
9-41	362	MEL-TLY	-1	0	37	29.5	12	41	31	2.95	0	12	1192	4	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-41	
9-42	460	MEL-TLY	-3	-2	34	29	8	38	30	3.40	0	0	1521	15	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-42	
9-43	363	MEL-WYO	-1	0	35	28	6	28	28	5.63	0	65	1052	1	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-43	
9-44	4C1	MEL-WYO	-3	-2	30	25	8	37	33	2.65	0	1	1831	730	3	0	0	0	0	0	0	0	0	0	0	0	V1	9-44	
9-45	364	MEL-MEM	0	1	38	35	6	41	42	1.19	0	6	1	0	0	0	0	0	0	0	0	0	0	0	0	V1	9-45		
9-46	4C2	MEL-MEM	0	0	35	36.5	6	35	34	2.67	0	0	1642	9	0	0	0	0	0	0	0	0	0	0	0	0	V2	9-46	
9-47	365	MEL-SEG	1	2	36.5	33	5	40	38	1.61	0	0	97	21	2	0	0	0	0	0	0	0	0	0	0	0	V1	9-47	
9-48	4C3	MEL-SEG	0	1	33	31	4	41	38	1.54	0	0	533	45	7	0	0	0	0	0	0	0	0	0	0	0	V2	9-48	
9-49	366	MEL-SWE	1	2	35	33	6	40	41	1.34	0	2	39	5	0	0	0	0	0	0	0	0	0	0	0	0	V2	9-49	
9-50	404	MEL-SWE	0	1	32	28	7	40	30	3.32	0	0	1672	251	2	0	0	0	0	0	0	0	0	0	0	0	V1	9-50	
9-51	367	MEL-SOC	-6	-6	36.5	36	10	42	43	1.06	0	451	10	4	2	0	0	0	0	0	0	0	0	0	0	V2	9-51		
9-52	405	MEL-SOC	1	1	29	29	6	35	39	2.10	0	0	1434	98	1	0	0	0	0	0	0	0	0	0	0	0	S1	9-52	

Table C-9. CONUS IST Loops (Sheet 2 Continued)

Line Character		Comments	
9-53	368	MEL-APA	-4 -3 36.5 31.5 18 37 28 4.22 0 0 79 3 0 0
9-54	406	MEL-APA	-2 -2 33 26 8 44 30 3.22 0 0 1997 502 3 0
9-55	369	MEL-CMC	4 5 30.5 29.5 7 48 34 2.03 0 0 295 1 0 0
9-56	407	MEL-CMC	1 0 39.5 27 8 37 32 2.88 0 0 1408 396 35 0
9-57	370	MEL-LAM	0 0 32 31 6 49 32 2.54 0 0 494 0 0 0
9-58	408	MEL-LAM	-3 -3 29 26 9 43 30 3.24 8 17 1898 1144 94 0
9-59	371	MEL-MOU	2 3 34.5 30 5 40 31 2.93 0 1 230 1 0 0
9-60	409	MEL-MOU	0 0 32.5 28 5 39 30 3.36 0 0 1239 6 2 0
9-61	372	MEL-LYO	1 2 34 30.5 7 44 32 2.59 0 0 751 0 0 0
9-62	410	MEL-LYO	-1 -1 30.5 26 8 41 31 2.95 0 0 1873 861 1 0
9-63	339	MEL-HEL	1 1 32 28 14 48 32 2.54 - - - - - -
9-64	411	MEL-HEL	-2 -2 28 25 18 35 31 3.33 1 317 1729 1434 12 0
9-65	373	MEL-LOD	0 1 33.5 28 9 34 31 3.45 0 0 947 1 0 0
9-66	412	MEL-LOD	-1 0 29 25 10 39 32 2.75 0 5 1725 - 3 0
9-67	374	MEL-JUL	5 5 32 24.5 24 42 36 1.77 0 100 1764 597 1 0
9-68	413	MUL-JUL	-1 -1 29 27 6 36 32 2.97 0 0 1782 155 3 0
9-69	375	MEL-MOJ	5 5 31 29.5 6 36 34 1.58 0 0 247 3 0 0
9-70	414	MEL-MOJ	-1 -1 28 28 7 36 31 3.23 0 1 1761 241 6 0
9-71	376	MEL-SLO	8 8 29.5 29.5 7 41 42 1.19 0 0 25 7 3 0
9-72	415	MEL-SLO	-3 -2 30 26 7 35 28 4.36 0 0 1640 137 3 0
9-73	377	MEL-SMF	-1 0 35.5 28.5 12 40 27 4.58 0 0 1773 140 2 0
9-74	416	MEL-SMF	-1 -1 31 24 13 41 29 3.66 0 1 1840 989 2 0
9-75	378	MEL-SME	-3 -2 34 29 10 35 29 3.97 0 0 1731 185 0 0
9-76	417	MEL-SME	-3 -3 32 24 9 44 29 3.60 0 0 1815 674 3 0
9-77	379	MEL-FRE	-1 -1 34 26 15 33 36 2.74 0 0 1858 953 0 0
9-78	418	MEL-FRE	-3 -2 31 24 11 36 28 4.28 0 0 1850 1800 8 0

Table C-10. Special Calls (Sheet 1)

10-1	257	Pearl Harbor, Hawaii - Wahiawa, Hawaii	12/13	1022	0	0	100	Pacific Access Loop	0	0	1.25E-6	1.25E-6	4-4	30	10-1				
10-2	157	Coltano, Italy - Hillington, Eng	11/24	1612	4.25E-3	5.12E-5	88	Combination Call	4.25E-3	4.33E-3	7.84E-3	4.08E-3	4-4	20	10-2				
10-3	158	Loced on 157	11/24	1632	3.80E-2	1.32E-3	24	Combination Call	3.80E-2	4.85E-2	3.28E-2	3.86E-2	4-4	15	10-3				
10-4	333	Pearl Harbor, Hawaii, Wa Lu Lei, Hawaii	12/17	0932	9.87E-3	0	100	HF Loop	6.23E-3	7.60E-3	6.56E-3	7.04E-3	5-5	21	10-4				
10-5	183A	Christchurch, Eng - Oakhamper, Eng	11/29	1020	0	-	-	GPO Loop	0	0	0	0	3-3	-	10-5				
10-6	183B	Christchurch, Eng - Whitehill, Eng	11/29	1030	5.00E-6	-	-	GPO Loop	5.00E-6	1.25E-5	5.00E-6	2.50E-6	2-2	-	10-6				
10-7	250	Hillingdon, Eng - Cedar Brook, NJ	12/3	1846	1.12E-2	-	-	Cedar Brook Loop	1.12E-2	-	-	-	1-1	20	10-7				
10-8	217	Hillingdon, Eng - Fr. Dietrich, Md	12/1	2030	1.29E-1	-	-	Fr. Dietrich Loop	1.29E-1	-	-	2.31E-1	1-1	14	10-8				
10-9	251	Hillingdon, Eng - Pottstown, Pa	12/3	1855	7.69E-2	-	-	Pottstown Loop	7.69E-2	-	-	-	1-1	18	10-9				
10-10	241	Hillingdon, Eng - Fr. Dietrich, Md	12/2	1906	1.40E-1	-	-	Fr. Dietrich Loop	1.40E-1	-	-	1.93E-1	1-1	14	10-10				
10-11	129A	Feldberg, Germ - Pottstown, Pa	11/19	0915	7.77E-2	-	-	Pottstown Loop	7.77E-2	-	-	-	4-4	-	10-11				
10-12	129B	Feldberg, Germ - Pottstown, Pa	11/19	0915	2.52E-3	0	100	Pottstown Loop	2.52E-3	-	-	1.39E-3	3-3	22	10-12				
10-13	306	Pearl Harbor, Hawaii - San Luis Obispo, Cal	12/15	1518	1.02E-3	0	100	San Luis Obispo Loop	1.02E-3	1.78E-3	1.37E-3	1.43E-3	4-4	23	10-13				
10-14	307	Pearl Harbor, Hawaii - San Luis Obispo, Cal	12/15	1543	1.93E-3	0	100	Mojave Loop	1.93E-3	2.22E-3	2.11E-3	1.88E-3	4-4	21	10-14				
10-15	326	Pearl Harbor, Hawaii - Stockton, Cal	12/16	1520	1.32F-2	-	-	Stockton Loop	1.32E-2	-	-	1.58E-2	1-1	20	10-15				
10-16	111	Feldberg, Germ - ?	12/17	1605	2.82E-2	1.17E-4	84	Last Loop	2.82E-2	2.27E-2	6.69E-2	3.13E-2	5-5	20	10-16				
10-17	127	Feldberg, Germ - ?	12/18	1702	2.82E-2	2.62E-5	79	Last Loop	2.82E-2	3.66E-2	3.18E-2	2.72E-2	3-3	20	10-17				
10-18	49	Hillingdon, Eng - Colzano, Italy	11/9	1440	1.50E-5	-	-	No routing	1.50E-5	-	-	-	2-2	25	10-18				
10-19	11	Colzano, Italy - Leghorn, Italy	11/14	1528	7.50E-6	-	-	2 Wire Loop	7.50E-6	-	-	-	1-1	30	10-19				
10-20	15	Colzano, Italy - Ankara, Turkey	11/5	0852	2.85E-1	-	-	2 Wire Loop	2.85E-1	-	-	-	2-2	10	10-20				
10-21	16	Colzano, Italy - Ankara, Turkey	11/5	0900	3.65E-2	2.62E-5	92	2 Wire Loop	3.65E-2	4.07E-2	-	-	3-3	20	10-21				
10-22	334	Pearl Harbor, Hawaii - Hillington, Eng	12/17	1100	1.25E-1	4.11E-4	-	WAH-HIN Loop	1.25E-1	-	-	-	2-2	-	10-22				
10-23	69A	Colzano, Italy - Wahiawa, Hawaii	11/11	1132	1.81E-1	1.34E-2	-	CLO-WAH Loop	1.81E-1	-	-	-	3-3	12	10-23				
10-24	17	Colzano, Italy - Aviano, Italy	11/5	0932	1.40E-1	-	-	SF Filter	1.40E-1	-	-	-	1-1	15	10-24				
10-25	34	Colzano, Italy - Mt. Vergine, Italy	11/8	1041	7.72E-2	6.14E-3	-	1600 Notch	7.72E-2	1.75E-1	1.52E-1	6.46E-2	3-3	14	10-25				
10-26	83	Feldberg, Germ - Ramstein, Germ	11/16	1000	-	-	-	Teletype Channel	-	-	-	-	1-0	-	10-26				

Table C-10. Special Calls (Sheet 1 Continued)

Call	Location	Date	C	E	R	8-110	8-110	Type of Call	BER (B)	BER 16-110	BER 16-130	BER 16-170	SER	Sync	Sync - H13	Total
10-27 98	Feldberg, Germ - Colfano, Italy	11/17	1048	1.08E-2	-	-	-	SF Filter	1.68E-2	3.90E-2	5.19E-2	-	2-2	14	10-27	
10-28 165	Hillingdon, Eng - Ms. Pateros, Greece	12/25	1453	1.54E-1	2.19E-3	-	-	Bad Channel	1.54E-1	-	-	-	2-2	12	10-28	
10-29 261	Pearl Harbor, Hawaii - Fuchs, Japan	12/13	1225	-	-	-	-	Bad Channel	-	-	-	-	3-0	-	10-29	
10-30 94	Feldberg, Germ - Stuttgart, Germ	11/16	1640	1.22E-1	2.49E-3	-	-	Pilot Stop Filter	1.22E-1	1.21E-1	1.23E-1	1.81E-1	3-3	15	10-30	

Table C-10. Special Calls (Sheet 2)

Table C-10. Special Calls (Sheet 2 Continued)

Table	Call	Location (Abbrev.)	Line loss (Data) (1 kHz)	S/N (Data) (1 kHz)	S/N (1 kHz)	$P_{j_0}$	HD 2nd	HD 3rd	HD %	GH +3	PH 20°	D	Type of Pictures	Location of Recording	Type of Recording	Line character.	Comments	Table	
10-25	34	CLO-MRE	9	7	32	33.5	12	-	-	-	-	-	-	-	-	CLO 9CLV (V2) FEL 9CEX (V2) MRE	V1	10-25	
10-26	83	CLO-RSN	-	-	-	-	-	-	-	-	-	-	-	-	-	FEL 44JNQS-12(RC) LKF 44JMH 5-2(SC) BAN 56ATX, 565REG	V1	10-26	
10-27	98	FEL-CLO	-	-	-	-	-	-	-	-	-	-	-	-	-	FEL 9CLV (V2) CLO	None	10-27	
10-28	165	HIN-PAT	11	19	22	16	24	33	27	2.65	-	-	-	-	-	HIN 9AEA (V2) MRE — PAT	None	10-28	
10-29	261	PHR-FUC	-	-	-	-	-	-	-	-	-	-	-	-	-	PHR KCA1 WAH KM93 FUC	None	10-29	
10-30	94	FEL-SGT	2	6	41	34	5	54	47	.49	0	1	3	2	1	2	A	V1	10-30

Table C-11. Comments

Call No.	Comment No.	Comments
2	1	Noticeable amplitude variation
3	14	SF filter inserted before recordings
20	15	Signal cut on and off several times prior to the 8 kb test
24	7	Faded for about 1 minute and came back prior to the 16-C test
33	9	Lost signal for several seconds during measurement of 16-C and at beginning of 8 kb test
35	8	Line dropped out during hit measurement
36	6	Line dropped during 16-130 measurement and came back
39	5	Appeared to be alternate routed for a brief period
43	12	Very bursty. No errors except for bursts
46	27	Bursty during recording
66	22	Lots of signal losses between BER and Line Test Data
75	17	Errors in bursts only
82	24	Gain varied 2 dB during 8 kb recording
86	23	S/N ratio varied widely
88	25	Very full weights. Periodic noise. Signal level jumped by 24 dB during bit count. Hit count not taken
90	18	Several signal level changes during measurements
92	16	Fine structure in amplitude response due to channel fading
95	3	Most errors are amplitude errors

Table C-11. Comments (Continued)

Call No.	Comment No.	Comments
97	4	Most errors are amplitude errors
99	2	Lissajou pattern shows periodic phase jitter
123	19	Several dropouts after sync
126	20	Line frequency A.M.
128	10	Lost line for 1 second - then 20 seconds - came back 8 dB down then back to original level
141	21	Dropped line for a second prior to 8 kb test
180	11	Appeared to be a change in channel characteristics during 16-C measurement 8 dB change in level
186	28	Low frequency phase jitter (1 Hz 30° p-p) not registered on Halcyon
187	29	Bad echos
188	30	Low frequency phase jitter
192	32	Interuption with test tone for about a minute
208	33	Double terminated at HIN
224	31	30° p-p low frequency phase jitter
226	26	Level changes of 6 dB during initial setup and hit measurement
267	34	Dialed datagrade
269	35	Dialed datagrade
276	36	36° p-p phase jitter at approximately 10 Hz
295	37	Signal level fluctuations of 6 dB and back
81	13	Receive level fluctuations of 6 dB

## APPENDIX D

### PHOTOGRAPHS

#### D-1 INTRODUCTION

This appendix contains the data collected in the form of CRT photographs, and is divided by the type of data presented.

#### D-2 AMPLITUDE AND ENVELOPE DELAY PHOTOGRAPHS

As described in Paragraph 2.4, the Halcyon line tester presents the line amplitude response and envelope delay and a stored CRT display. This was photographed with a Polaroid camera for a hard copy record. Unfortunately, the line tester is not equipped with a camera mounting bezel so there is some variation in geometry between different photos, and in some cases the marking of frequency, amplitude and delay are not visible in individual pictures. However, the scales are the same on all photos and are as follows:

- a. The horizontal (frequency) axis is 200 Hz per division and starts at 200 Hz on the left margin. The 1.0 kHz line is crossed with small horizontal tick marks.
- b. The relative amplitude scale (vertical) is 2.5 dB per division.
- c. The vertical envelope delay scale is 500  $\mu$ s per division. (The finer amplitude and envelope delay scales were not used for these tests.)

When making frequency sweeps on the lines, the tester was set to automatically skip a band in the vicinity of the 2600 Hz single frequency (S.F.) signaling tone, to avoid disconnecting the line. This shows up as a discontinuity on some of the amplitude and envelope delay traces; the true response would be a faired curve through this region.

In the tables of Appendix C, the highest level of conditioning met by each test connection is given. In these judgements, the bias was in favor of the line, that is, if the characteristics were close to the specifications it was counted as complying.

For reference purposes, characteristics of the simulated lines in the Axel Model 771 simulator (3002, C1, C2, C4) were measured on the line tester and are enclosed.

All pictures in this appendix are indexed by their call number. To assist the reader in locating the other line data contained in Appendix C corresponding to this call number, a cross-reference from call number to table number is given in Table D-1.

#### D-3 PHASE JITTER PHOTOGRAPHS

On calls which measured more than approximately  $15^{\circ}$  p-p on the line tester, the jitter spectrum was recorded and photographed. As a calibration of this setup, the line simulator was set up with known jitter frequency and amplitude and the results photographed. The calibration points were  $27^{\circ}$  p-p at 150 Hz and  $12^{\circ}$  p-p at 180 Hz. The horizontal calibration for this photo was 100 Hz/division. For the line tests, it was found that 50 Hz/division gave a more interesting presentation, and all line photos have this scale factor. The vertical calibration is the same for the line and calibration photos, 10 dB per division. All line photos are identified by their call numbers.

#### D-4 AMPLITUDE VARIATION PHOTOGRAPHS

On calls which exhibited significant amplitude modulation (fading), a constant amplitude 1004 Hz tone was transmitted and the received line signal photographed. The time base was chosen to best illustrate the nature of the AM, and is noted with each photo. In two cases (calls 41 and 86) two photos were made with different time bases.

Table D-1. Cross-Reference From Table Number to Call Number

<u>Call No.</u>	<u>Table No.</u>						
1	2-1	28	1-8	55	1-2	81	1-83
2	1-7	29	1-54	56	1-13	82	3-18
3	2-3	30	1-53	57	1-10	83	10-26
4	1-11	31	1-55	58	1-3	84	3-19
5	2-6	32	1-56	59	1-14	85	3-20
6	1-16	33	1-57	60	3-2	86	3-15
7	1-17	34	10-25	61	3-3	87	3-21
8	3-1	35	1-52	62	1-15	88	3-22
9	1-18	36	1-47	63	3-4	89	2-16
10	1-1	37	4-1	64	3-10	90	2-17
11	10-19	38	4-2	65	3-12	91	2-9
12	1-12	39	1-44	66	3-13	92	2-12
13	1-6	40	4-41	67	3-14	93	2-18
14	1-20	41	1-4	68	3-11	94	10-30
15	10-20	42	4-7	69	1-21	95	1-26
16	10-21	43	1-81	69A	10-23	96	1-25
17	10-24	44	4-5	70	2-8	97	1-27
18	2-2	45	1-82	71	2-10	98	10-27
19	2-4	46	4-8	72	4-11	99	1-24
20	2-5	47	1-5	73	2-11	100	1-31
21	3-9	48	4-6	74	2-13	101	1-30
22	1-48	49	10-18	75	2-15	102	1-28
23	1-49	50	4-9	76	4-12	103	1-29
24	1-50	51	1-45	77	1-22	104	1-61
25	1-51	52	4-10	78	4-13	105	1-62
26	2-7	53	1-46	79	1-58	106	1-77
27	1-12	54	1-9	80	4-15	107	1-63

Table D-1. Cross-Reference From Table Number to Call Number (Continued)

<u>Call No.</u>	<u>Table No.</u>						
108	1-66	133	4-16	160	1-34	185	
109	1-60	134	1-84	161	1-35	186	5-5
110	2-20	135	4-3	162	1-70	187	5-6
111	10-16	136	1-23	163		188	5-7
112	1-64	137	2-24	164	1-40	189	5-8
113	1-67	138	2-25	165	10-28	190	5-33
114	3-23	139	2-28	166	1-37	191	5-34
115	3-24	140	2-29	167	1-38	192	5-37
116	2-19	141	2-30	168	1-71	193	5-38
117	3-16	142	2-32	169	1-39	194	5-41
118	3-5	143	2-33	170	1-43	195	5-42
119	3-6	144	3-17	171	1-42	196	5-60
120	3-7	145	2-26	172	1-70	197	5-61
121		146	2-34	173	1-73	198	5-58
122		147	2-27	174	1-79	199	5-59
123	2-21	148	2-31	175	1-74	200	5-39
124	2-14	149	4-17	176	1-80	201	5-40
125	2-22	150		177	1-76	202	5-29
126	2-23	151	4-19	178	1-69	203	5-30
127	10-17	152	1-32	179	1-75	204	5-21
128	1-65	153	4-18	180	1-72	205	5-22
129	4-14	154	1-33	181	1-36	206	5-54
129A	10-11	155	4-21	182	3-8	207	5-55
129B	10-12	156	1-68	183	3-25	208	5-49
130	1-59	157	10-2	183A	10-5	209	5-50
131	4-20	158	10-3	183B	10-6	210	5-3
132	1-85	159	1-41	184		211	5-4

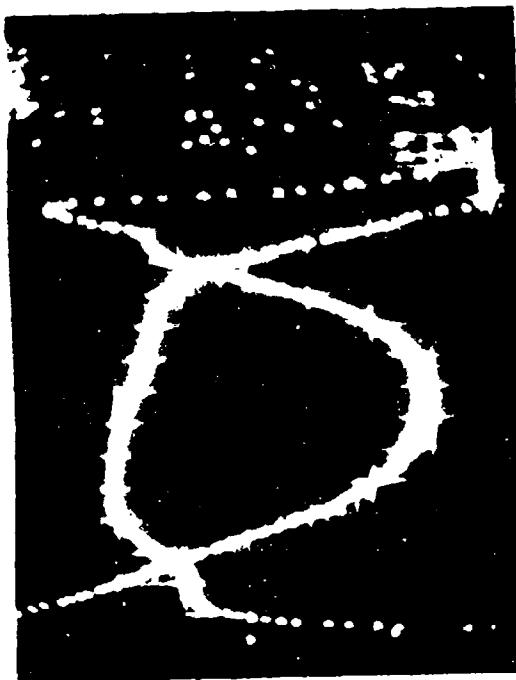
**Table D-1. Cross-Reference From Table Number to Call Number (Continued)**

<u>Call No.</u>	<u>Table No.</u>						
212	5-25	239	5-57	266	7-5	293	8-5
213	5-26	240	5-45	267	6-34	294	9-2
214	5-15	241	5-46 (10-10)	268	6-35	295	8-4
215	5-16	242	5-17	269	6-42	296	8-1
216	5-27	243	5-18	270	6-43	297	
217	5-28 (10-8)	244	5-13	271	7-7	298	6-27
218	5-62	245	5-14	272	7-8	299	6-28
219	5-63	246	5-47	273	7-19	300	6-37
220	5-19	247	5-48	274	7-21	301	6-38
221	5-20	248	5-9	275	7-24	302	6-7
222	5-1	249	5-10	276	7-25	303	6-8
223	5-2	250	10-7	277	7-20	304	6-30
224	5-11	251	10-9	278	6-1	305	6-11
225	5-12	252	7-1	279	6-2	306	10-13
226	3-26	253	7-2	280	6-36	307	10-14
227	5-35	254	7-10	281		308	6-29
228	5-36	255	7-15	282	6-39	309	6-19
229	5-31	256	7-18	283		310	6-20
230	5-32	257	10-1	284		311	8-3
231	5-51	258	7-16	285	6-3	312	8-6
232	5-43	259	7-14	286	6-4	313	8-9
233	5-44	260	7-6	287	6-5	314	7-9
234	5-52	261	10-29	288	6-6	315	7-23
235	5-53	262	7-3	289	6-16	316	7-13
236	5-23	263	7-22	290	6-17	317	6-32
237	5-24	264	7-11	291	7-12	318	6-33
238	5-56	265	7-17	292	8-8	318A	6-18

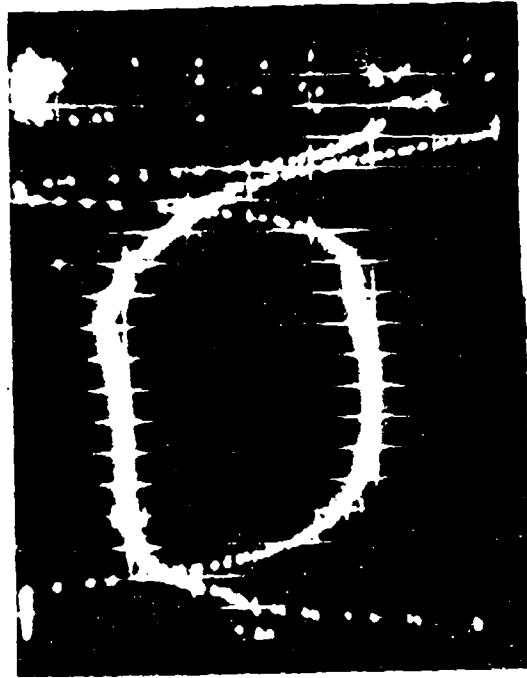
**Table D-1. Cross-Reference From Table Number to Call Number (Continued)**

<u>Call No.</u>	<u>Table No.</u>						
319	6-11	346	9-13	373	9-65	400	9-42
320	6-12	347	9-15	374	9-67	401	9-44
321	6-21	348	9-17	375	9-69	402	9-46
322	6-22	349	9-19	376	9-71	403	9-48
323	6-13	350	9-21	377	9-73	404	9-50
324	6-14	351	9-23	378	9-75	405	9-52
325	6-15	352	9-25	379	9-77	406	9-54
326	6-9	353	9-27	380	9-2	407	9-56
327	6-10 (10-15)	354	9-29	381	9-4	408	9-58
328	8-7	355		382	9-6	409	9-60
329		356		383	9-8	410	9-62
330	6-23	357	9-31	384	9-10	411	9-64
331	6-24	358	9-33	385	9-12	412	9-66
332	7-4	359	9-35	386	9-14	413	9-68
333	10-4	360	9-37	387	9-16	414	9-70
334	10-22	361	9-39	388	9-18	415	9-72
335	6-25	362	9-41	389	9-20	416	9-74
336	6-26	363	9-43	390	9-22	417	9-76
337	6-40	364	9-45	391	9-24	418	9-78
338	6-41	365	9-47	392	9-26		
339	9-63	366	9-49	393	9-28		
340	9-1	367	9-51	394	9-30		
341	9-3	368	9-53	395	9-32		
342	9-5	369	9-55	396	9-34		
343	9-7	370	9-57	397	9-36		
344	9-9	371	9-59	398	9-38		
345	9-11	372	9-61	399	9-40		

**AMPLITUDE AND ENVELOPE DELAY PHOTOGRAPHS**



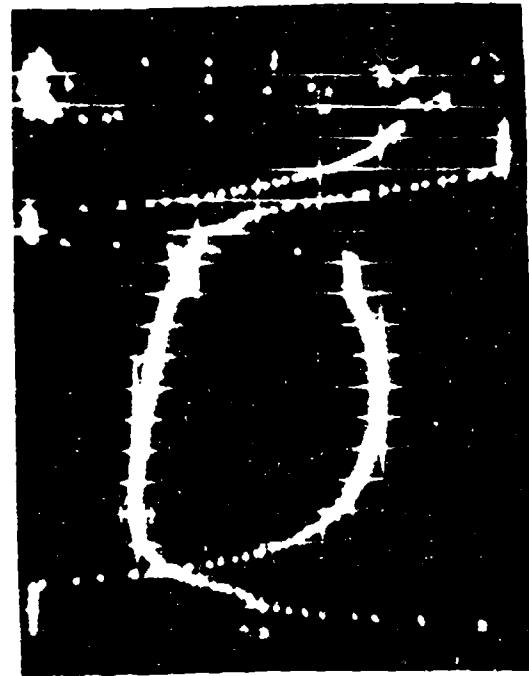
C-1



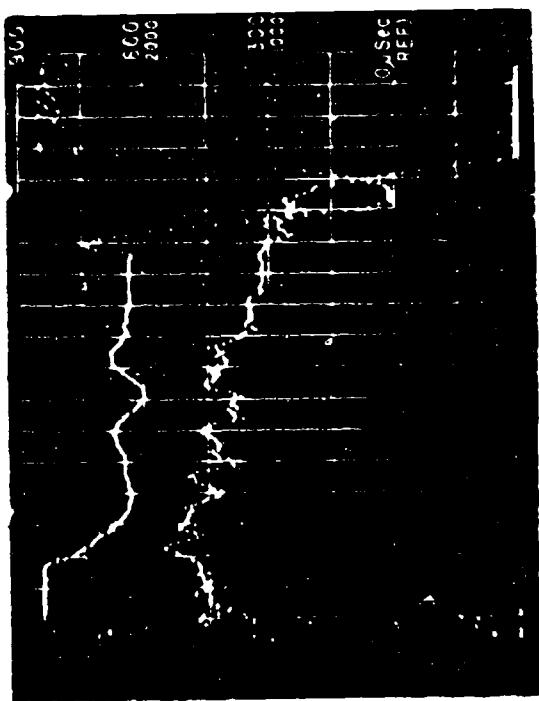
C-4



3002



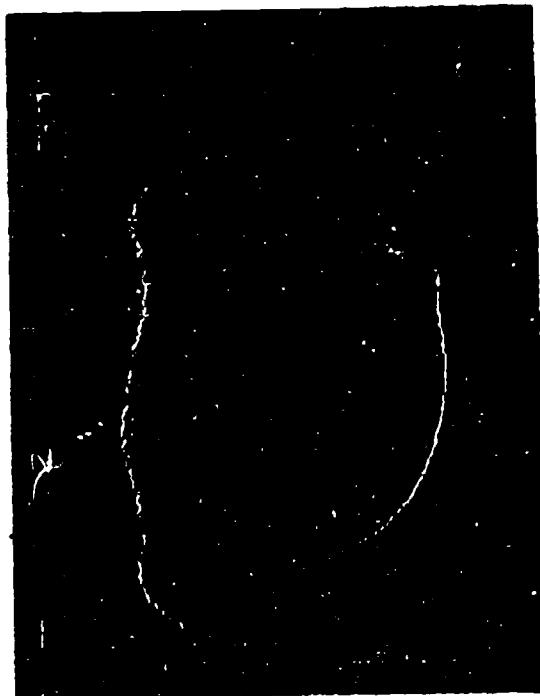
C-2



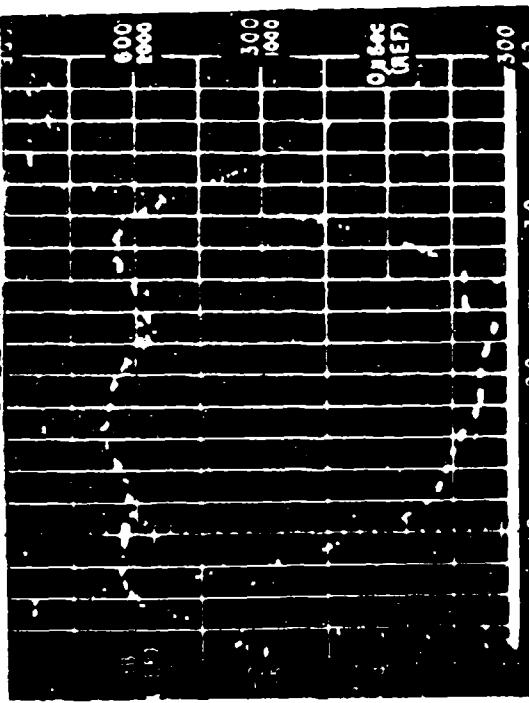
CALL #2



CALL #4



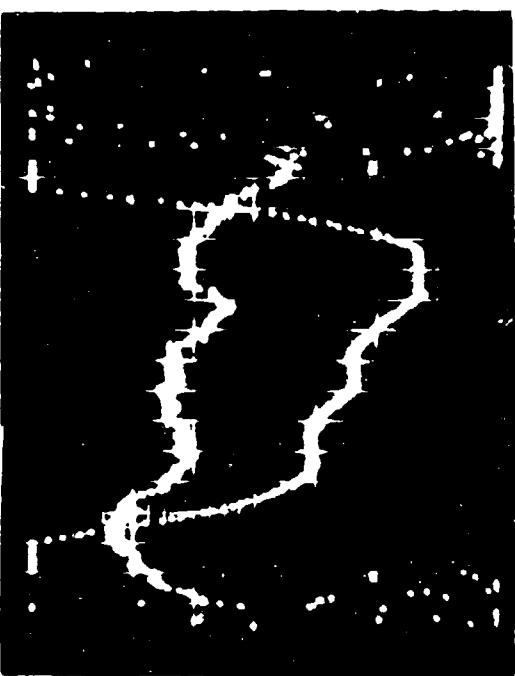
CALL #1



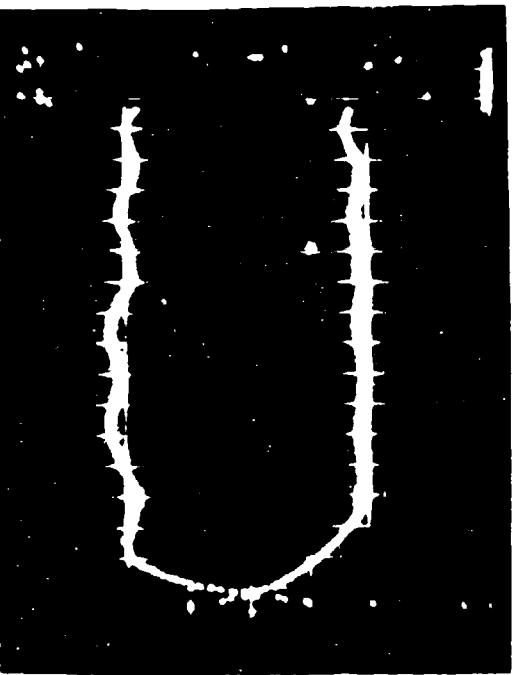
CALL #3



CALL #7



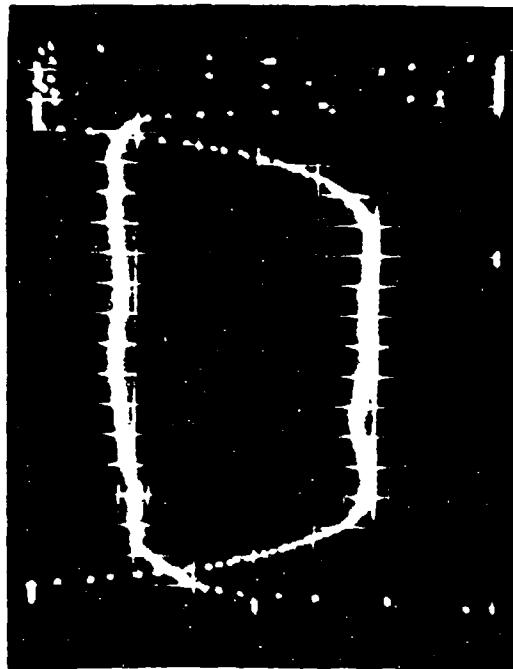
CALL #8



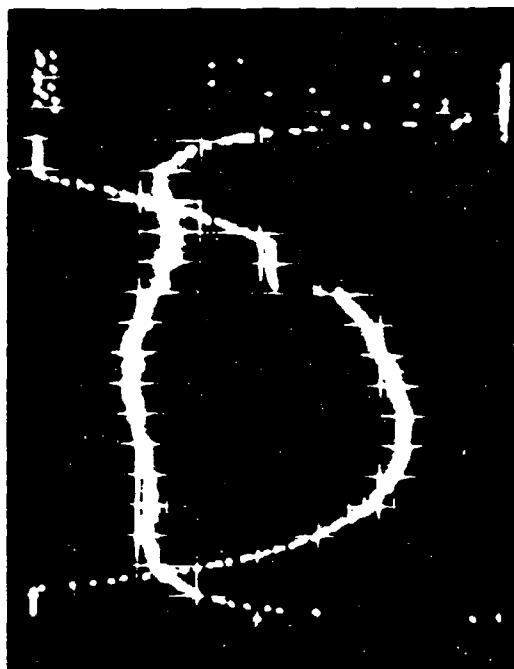
CALL #5



CALL #6



CALL #12



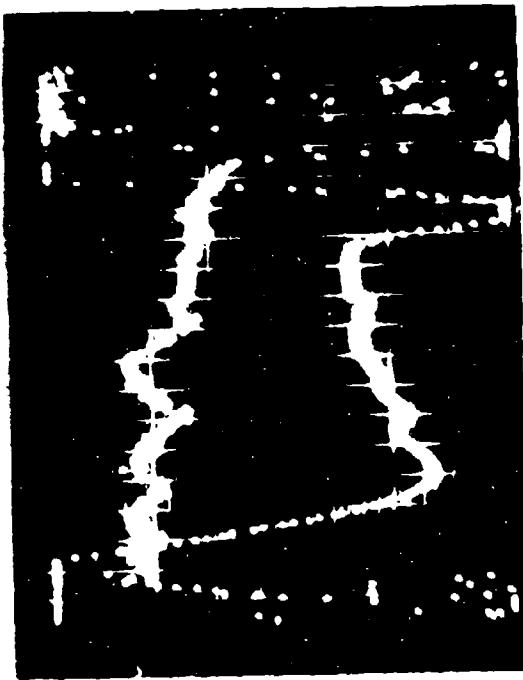
CALL #13



CALL #9



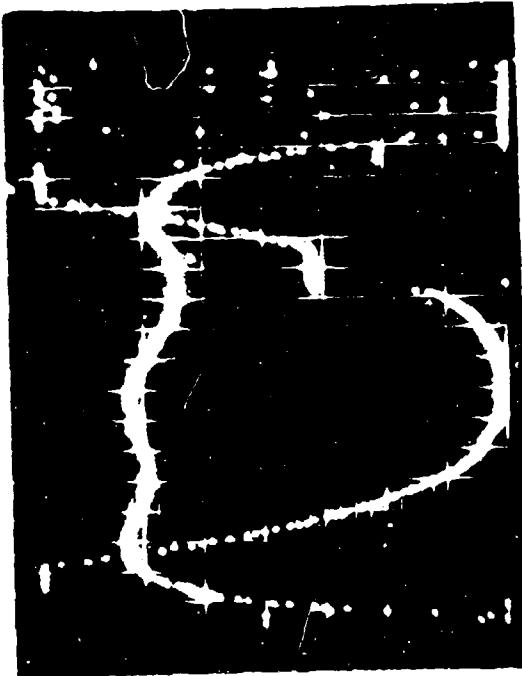
CALL #10



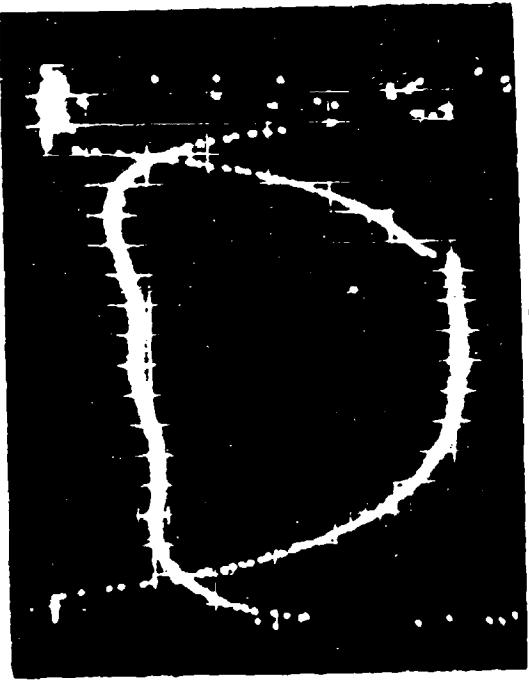
CALL #16



CALL #20



CALL #14



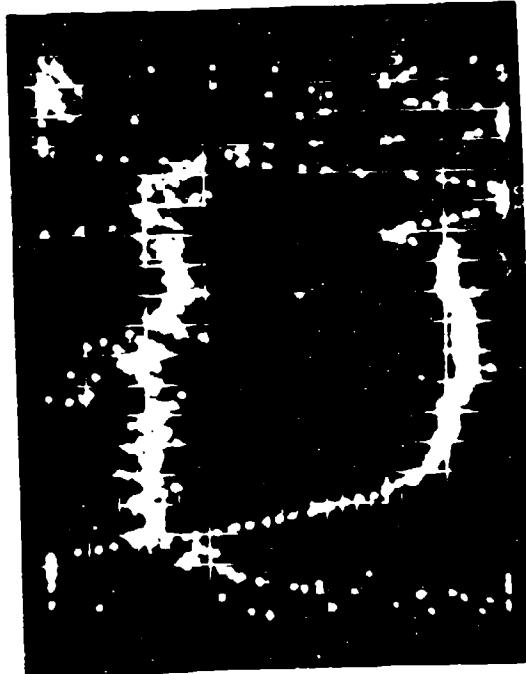
CALL #18



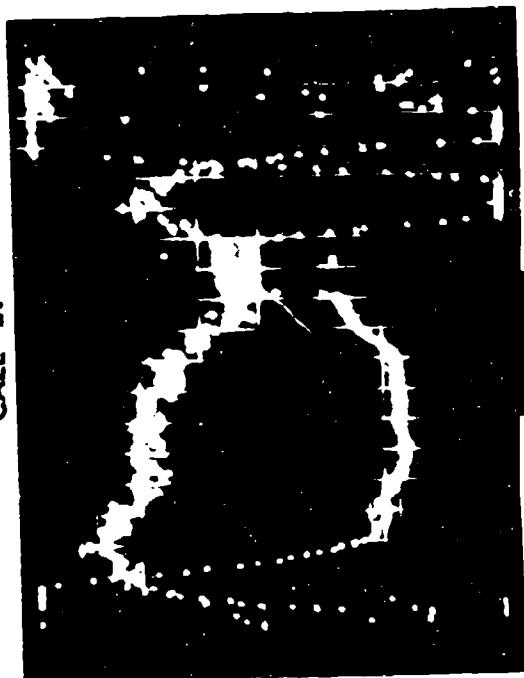
CALL #22



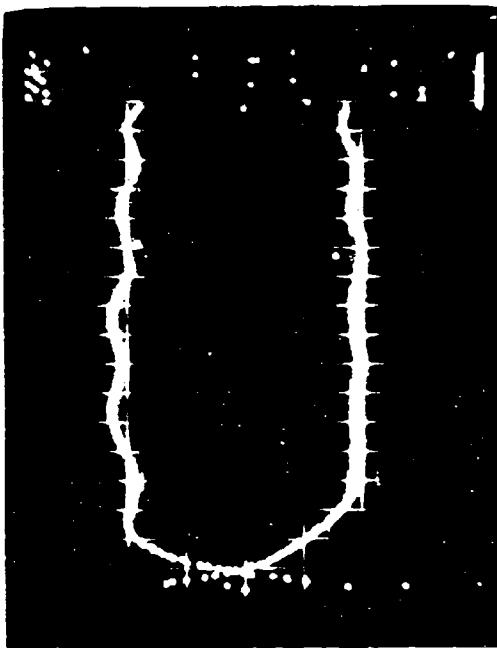
CALL #24



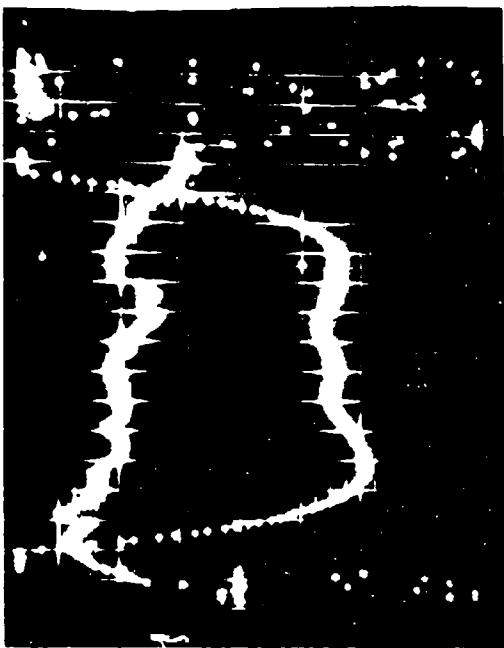
CALL #21



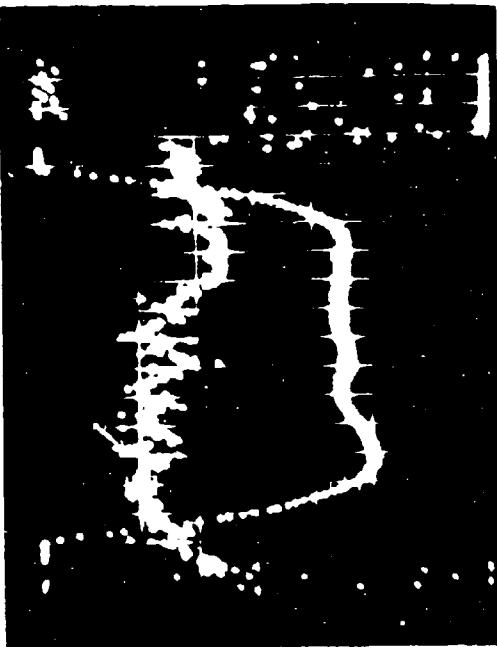
CALL #23



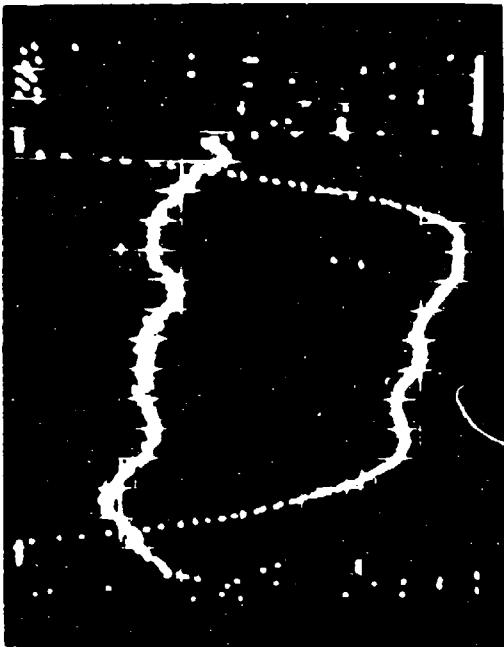
CALL #26



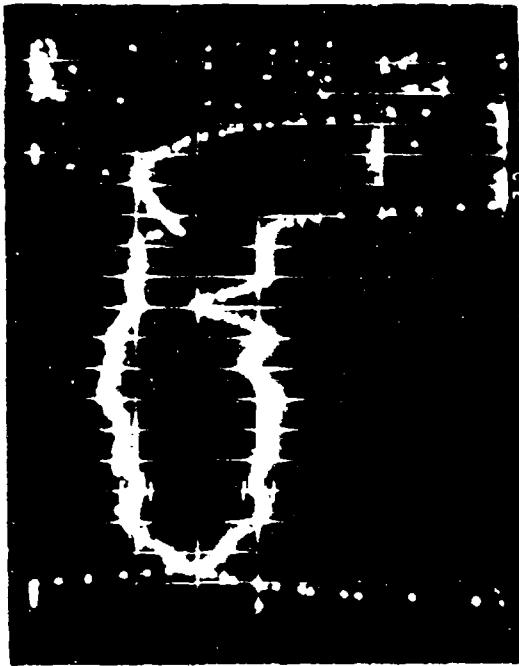
CALL #28



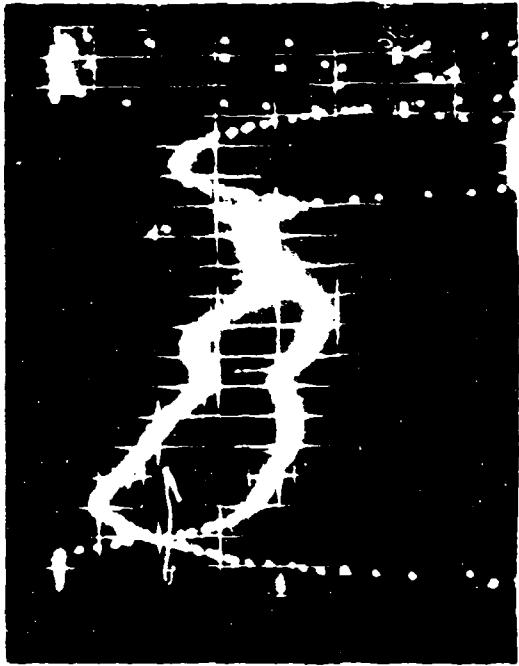
CALL #25



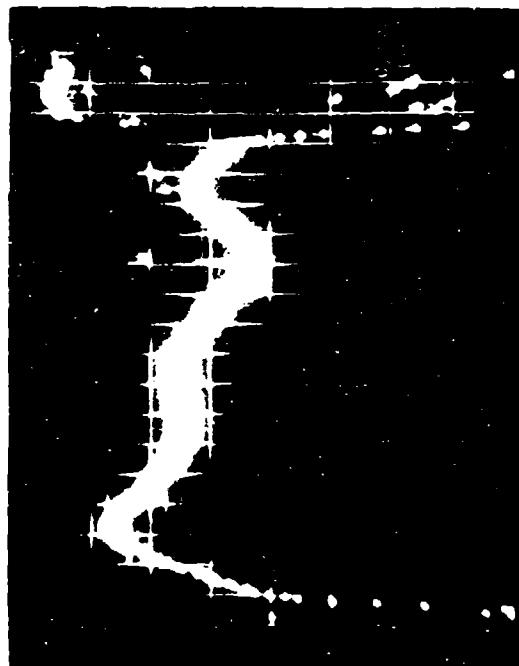
CALL #27



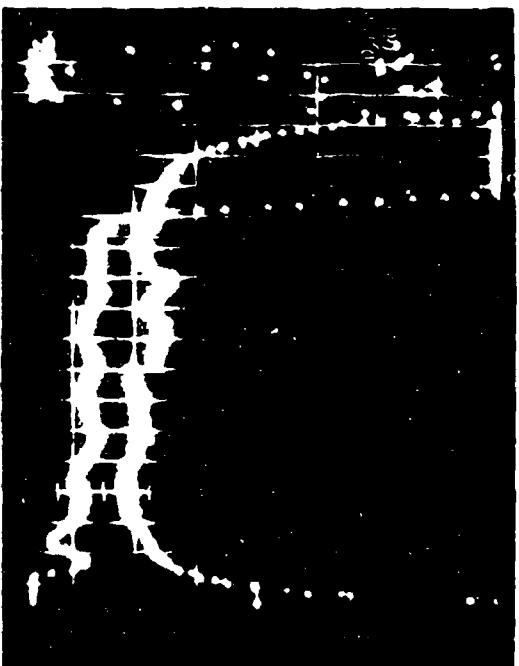
CALL #30



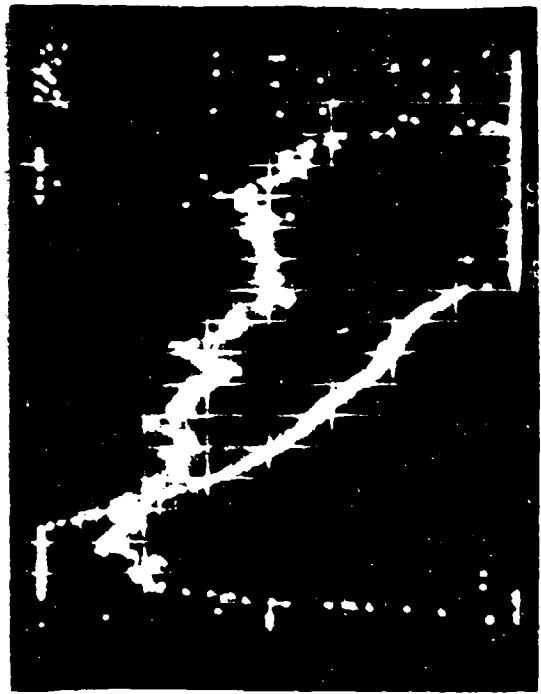
CALL #33



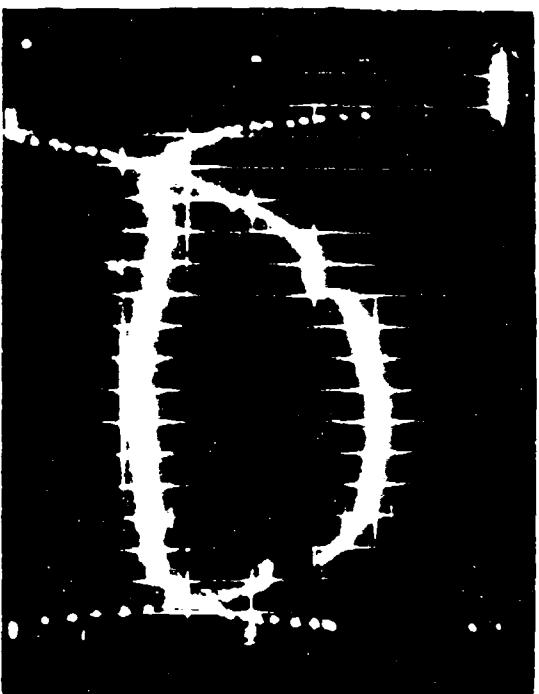
CALL #29



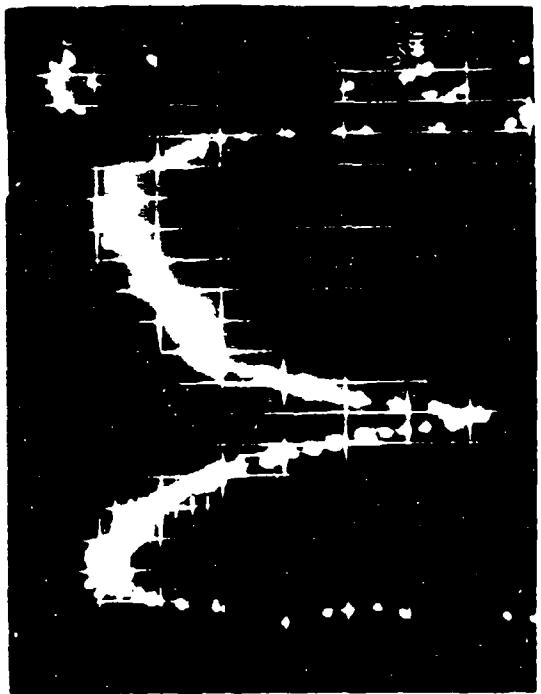
CALL #31



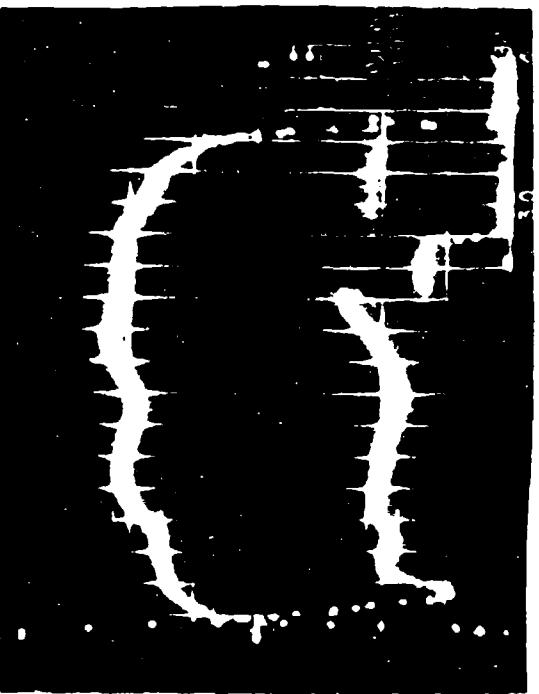
CALL #35



CALL #37



CALL #34



CALL #36



CALL #39



CALL #41



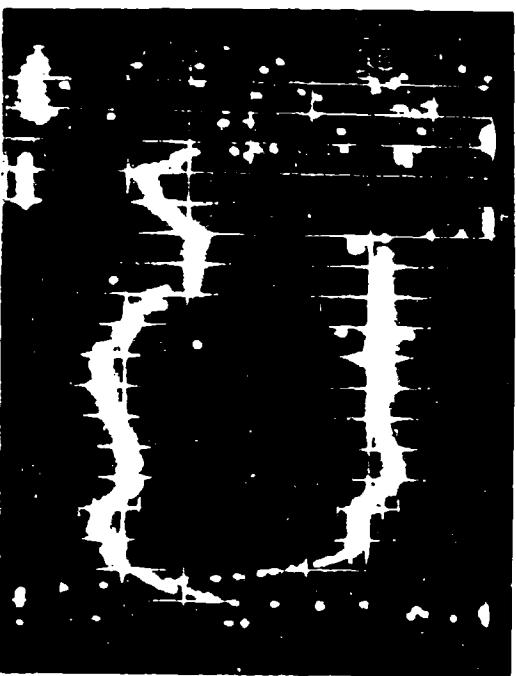
CALL #38



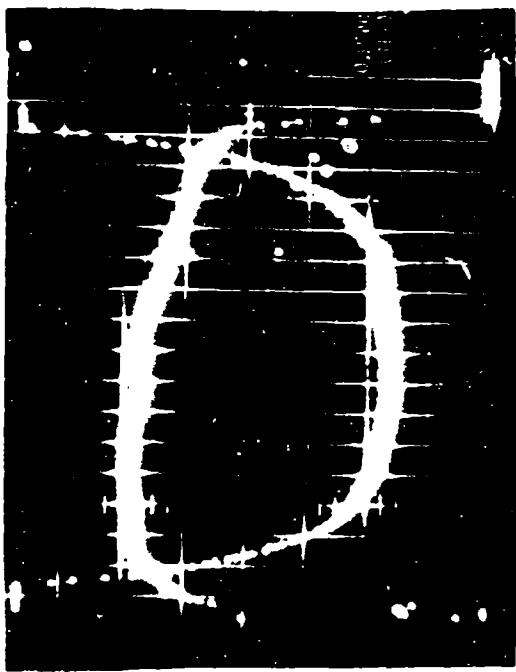
CALL #40



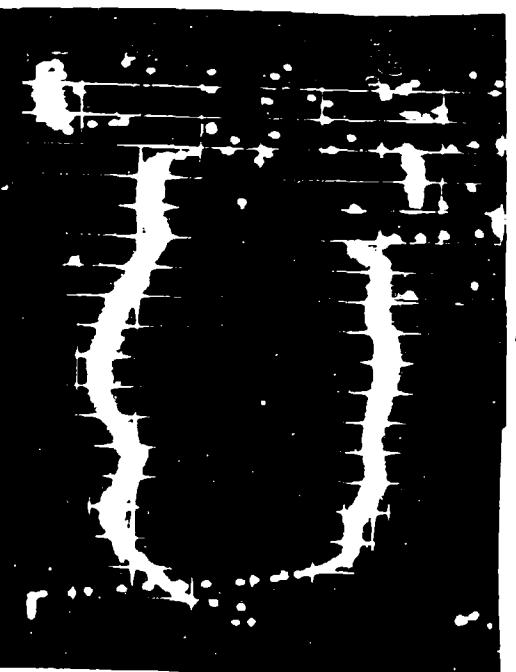
CALL #43



CALL #45



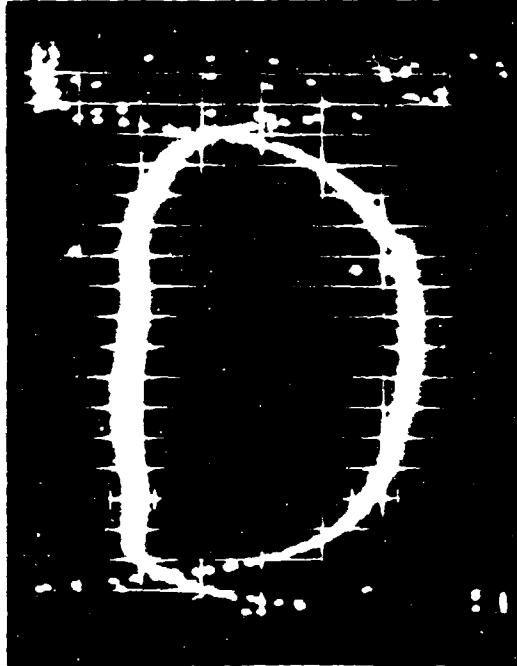
CALL #42



CALL #44



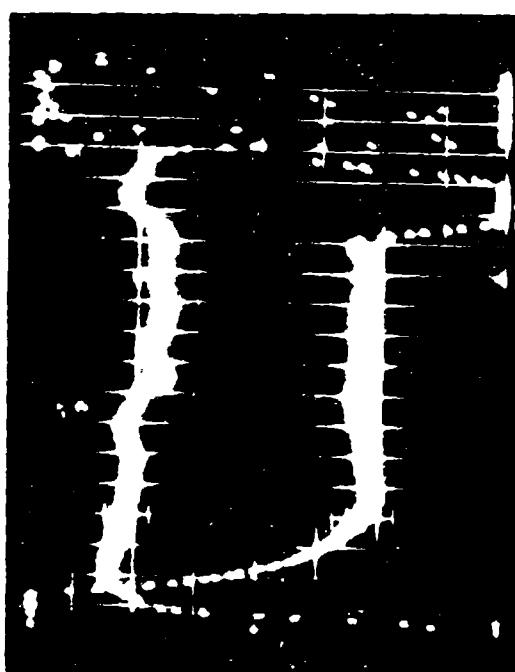
CALL #47



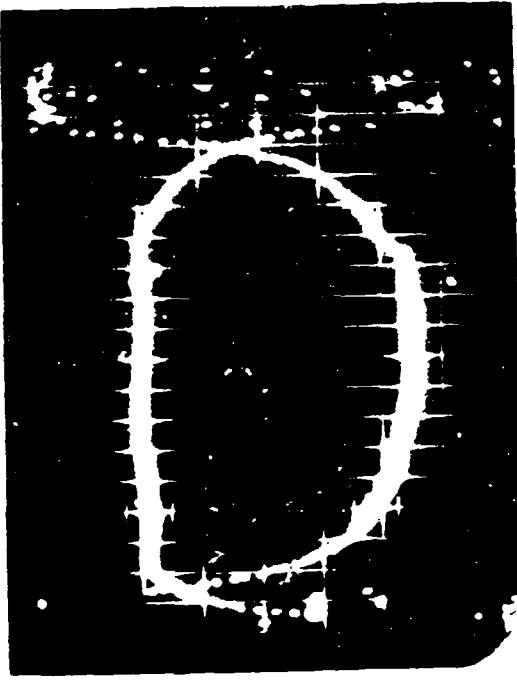
CALL #50 AD



CALL #46



CALL #48



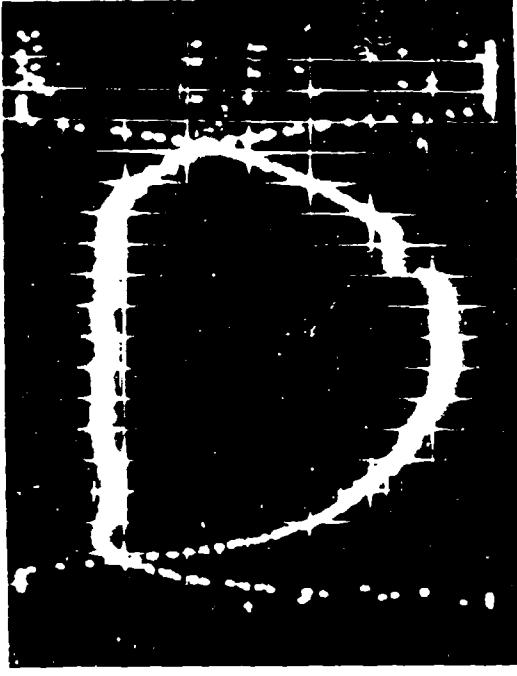
CALL #52



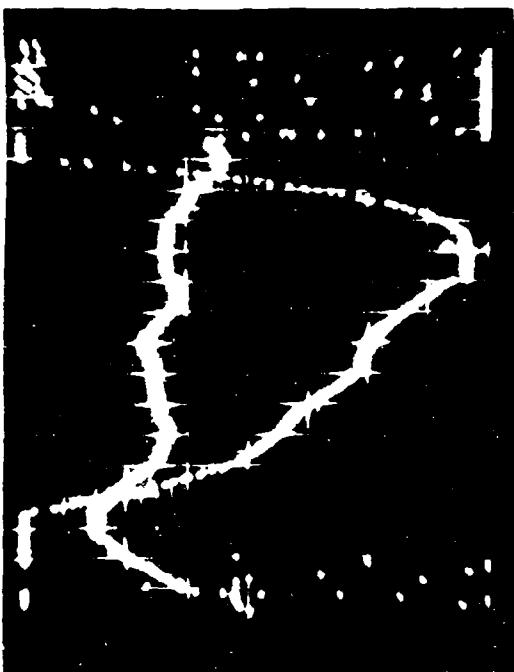
CALL #54



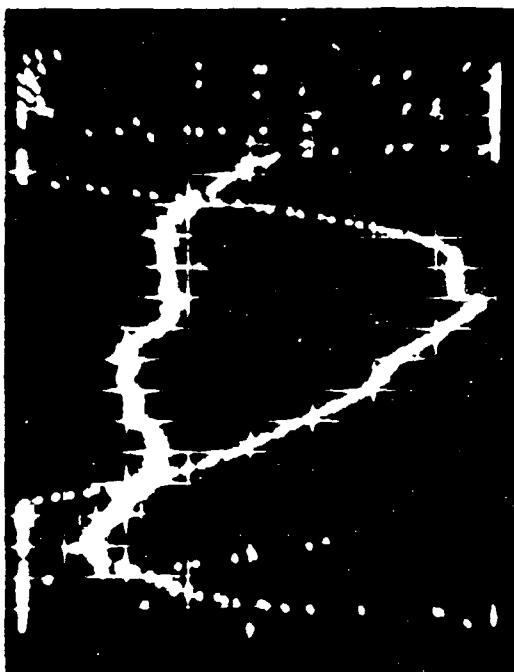
CALL #51



CALL #53



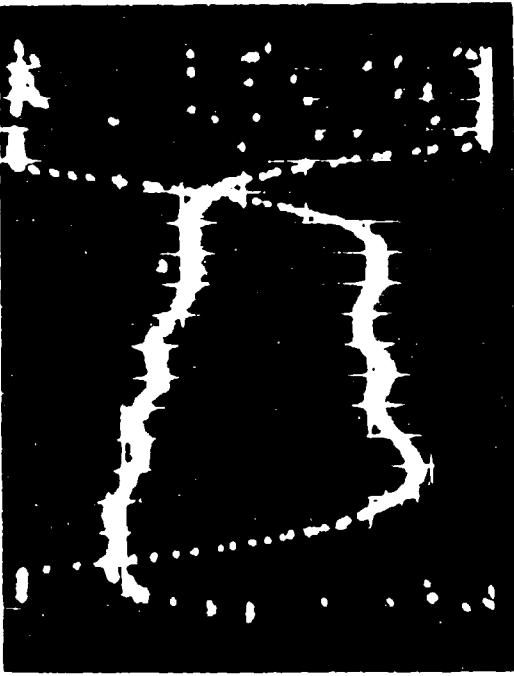
CALL #56



CALL #58



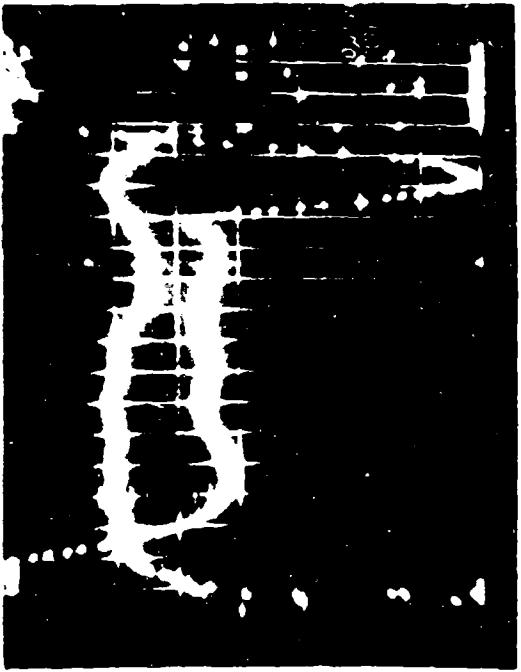
CALL #55



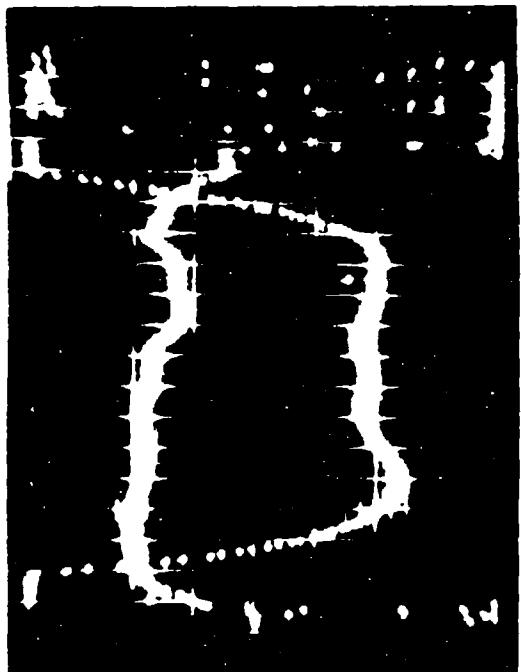
CALL #57



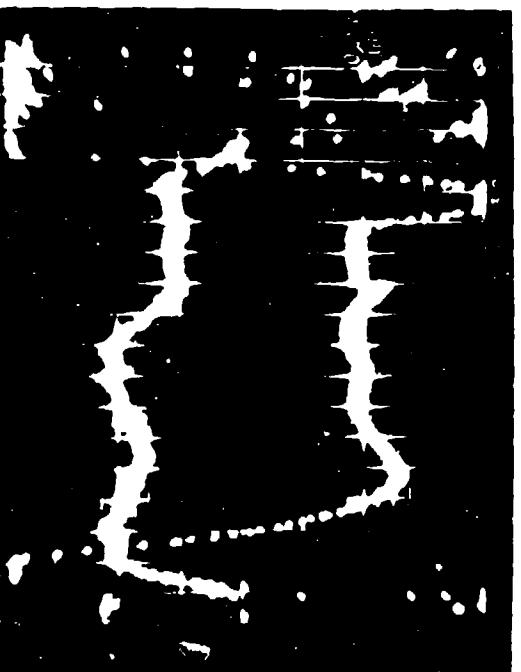
CALL #60



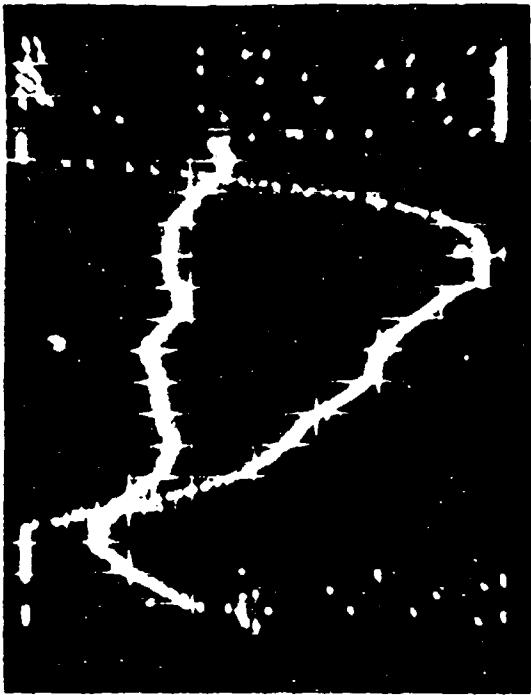
CALL #62



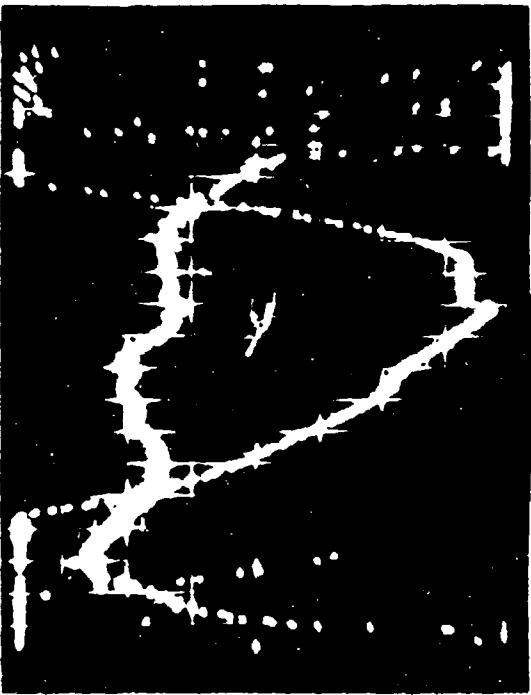
CALL #59



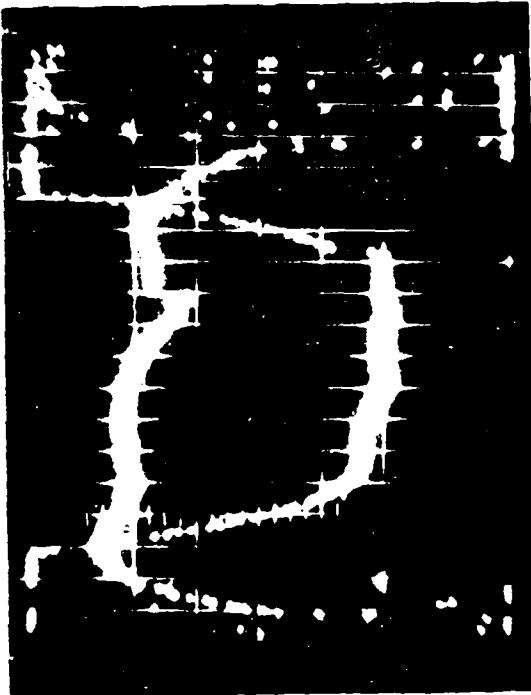
CALL #61



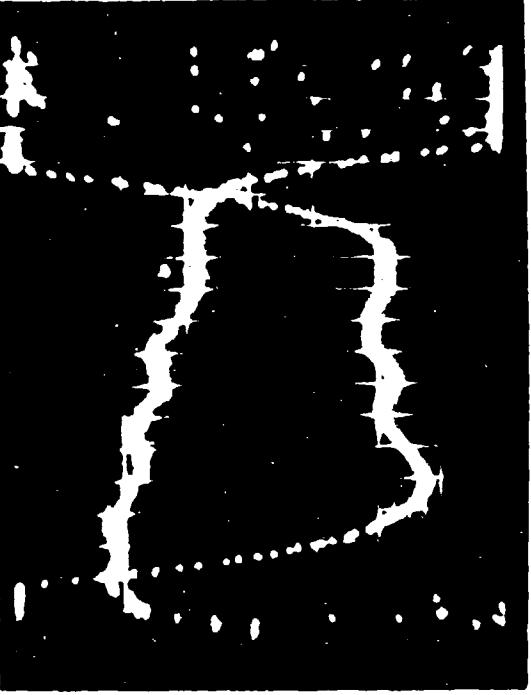
CALL #56



CALL #58



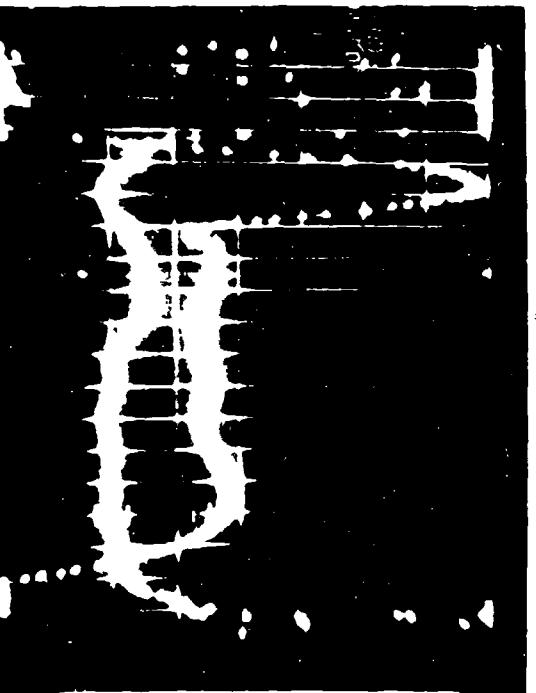
CALL #55



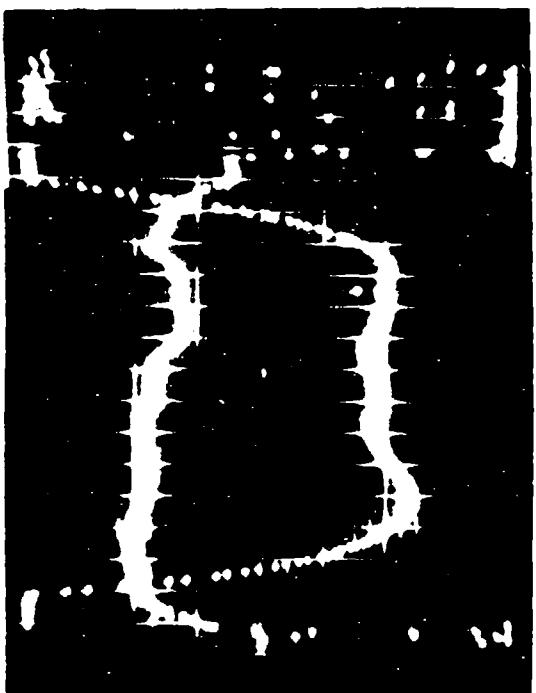
CALL #57



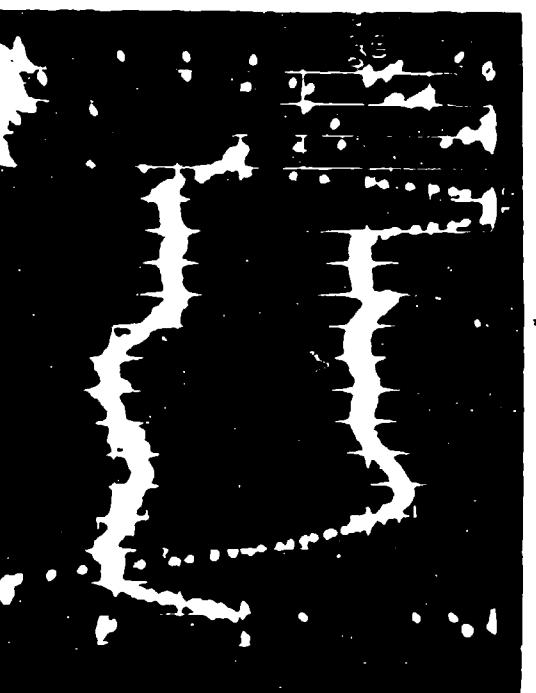
CALL #60



CALL #62



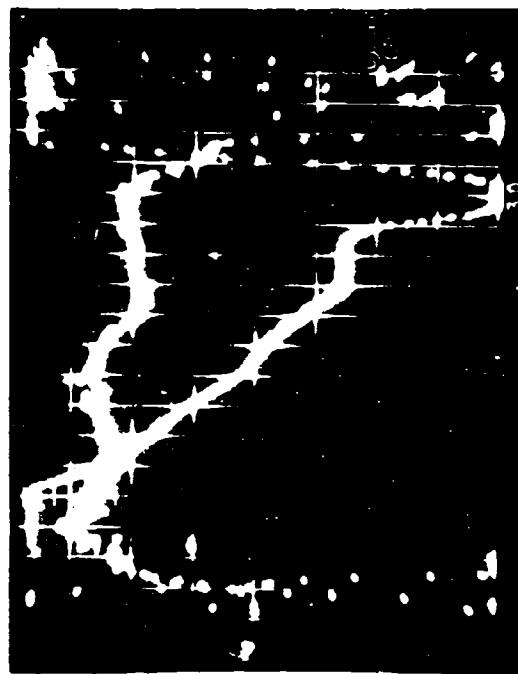
CALL #59



CALL #61



CALL #64



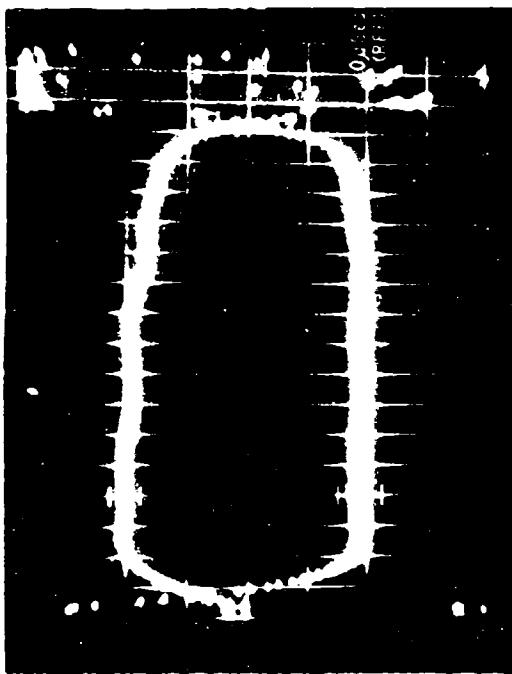
CALL #67



CALL #63



CALL #66



CALL #69



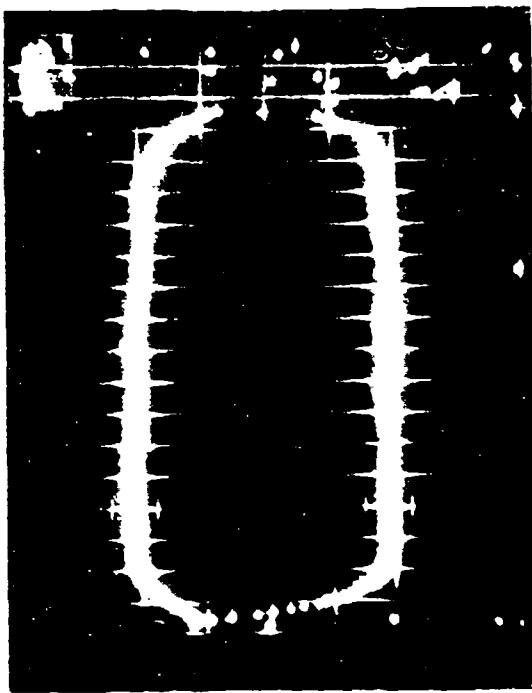
CALL #70



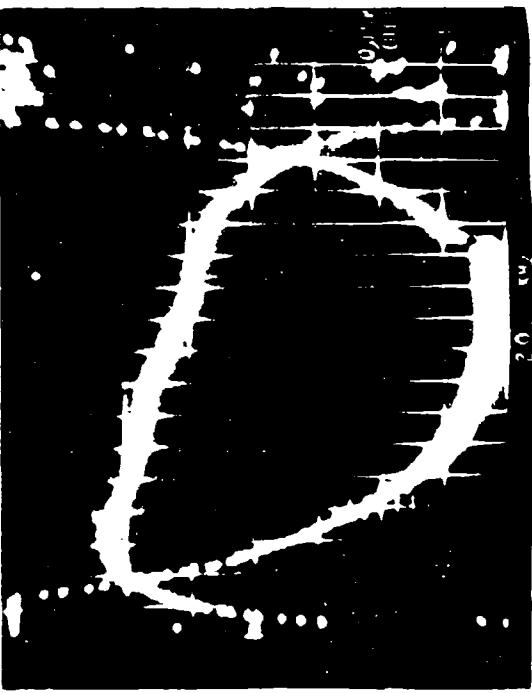
CALL #68



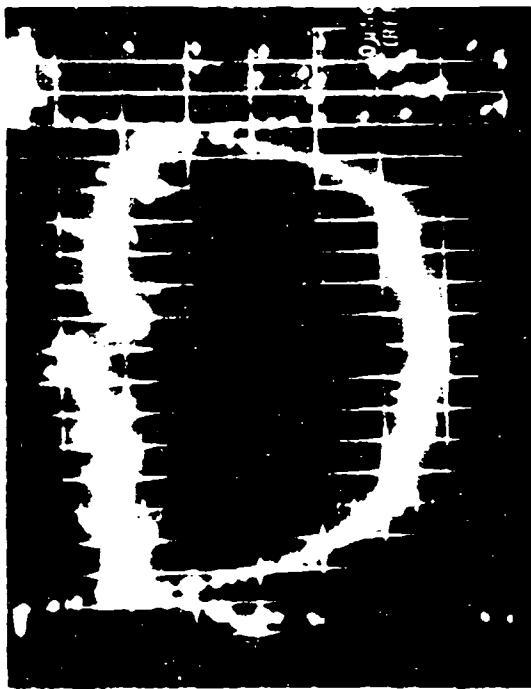
CALL #69 A



CALL #72



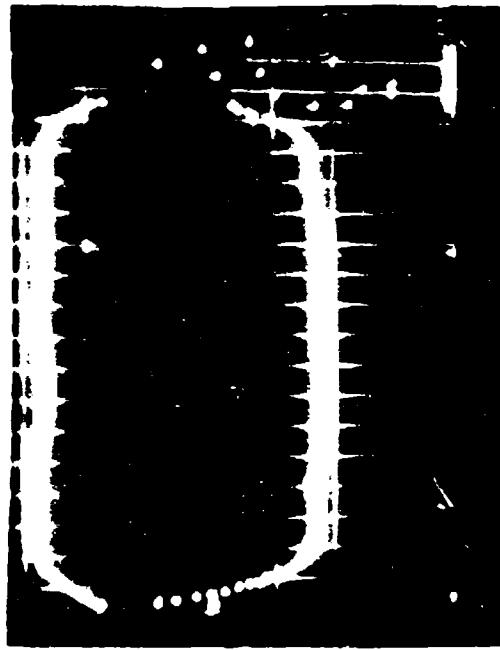
CALL #74



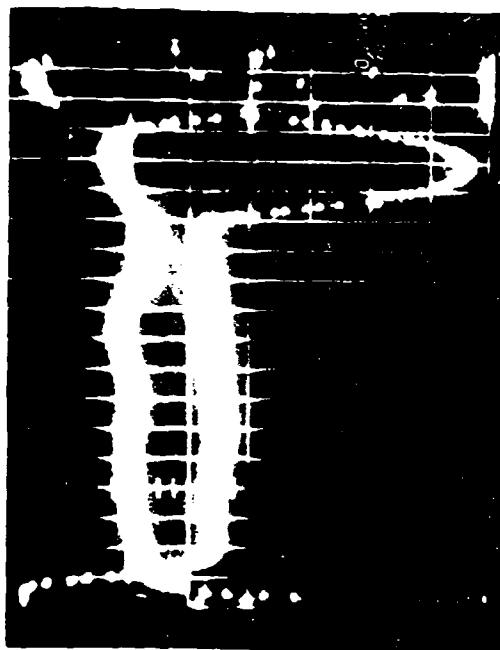
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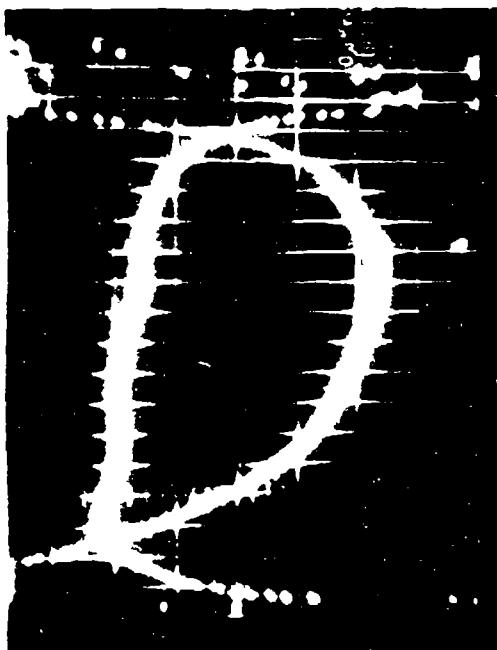
CALL #73



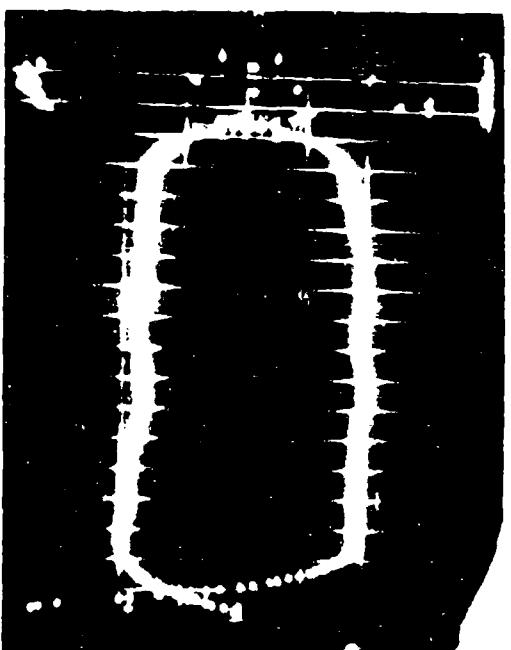
CALL #76



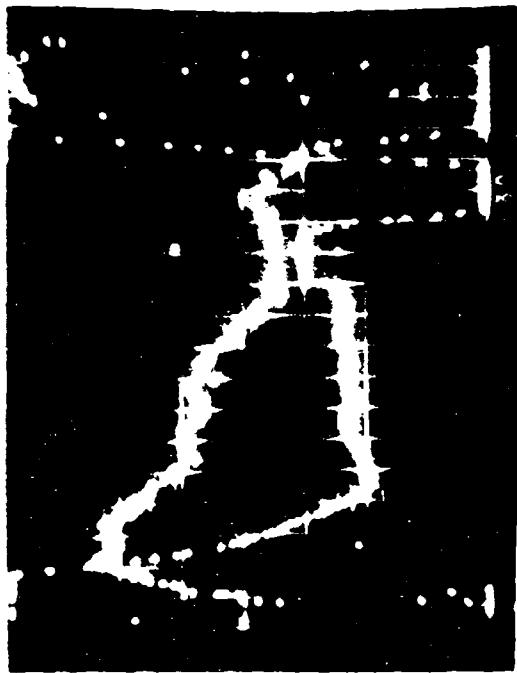
CALL #78



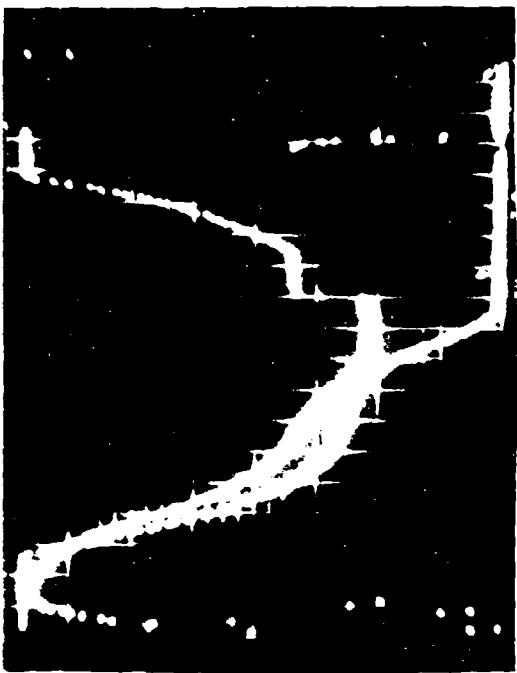
CALL #75



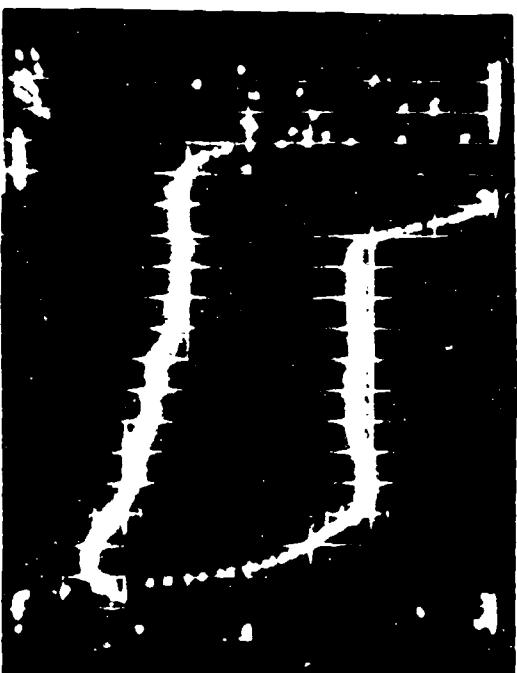
CALL #77



CALL #81



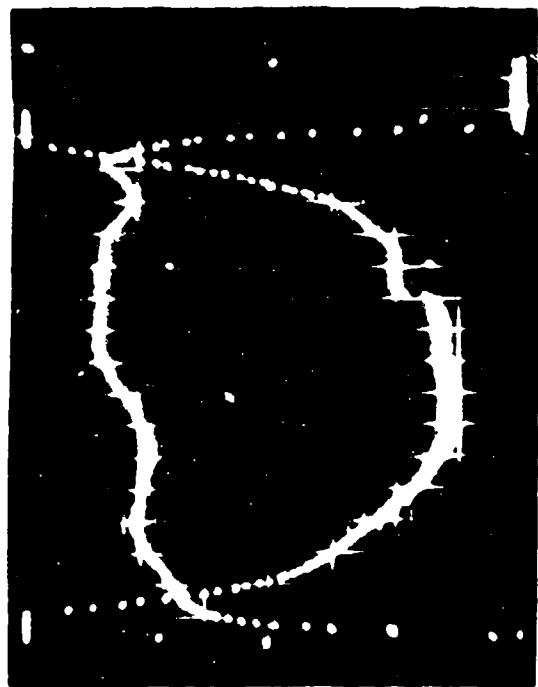
CALL #83



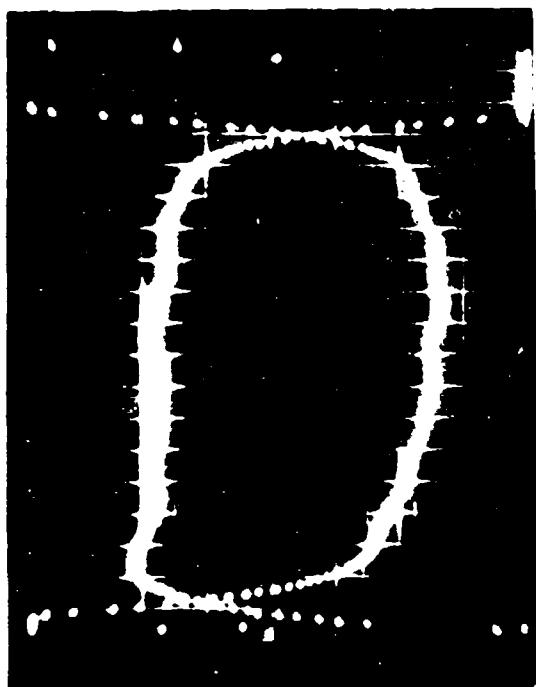
CALL #80



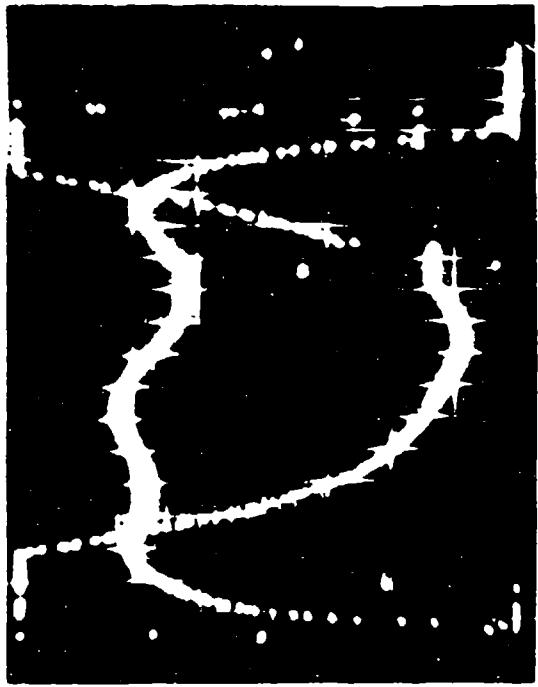
CALL #82



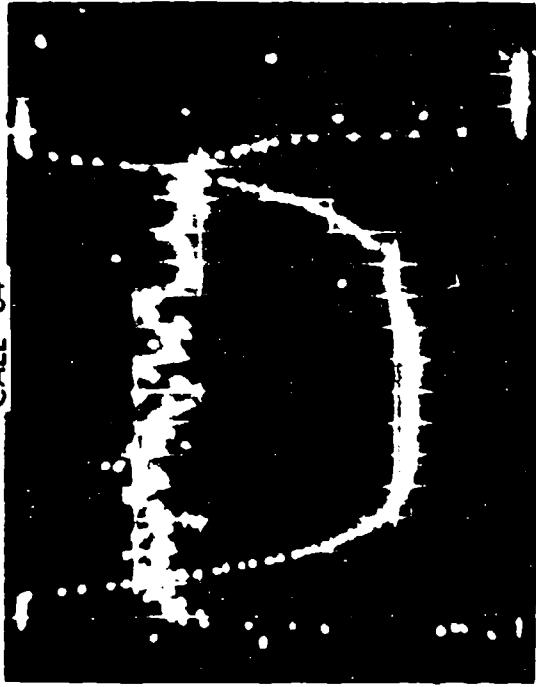
CALL #85



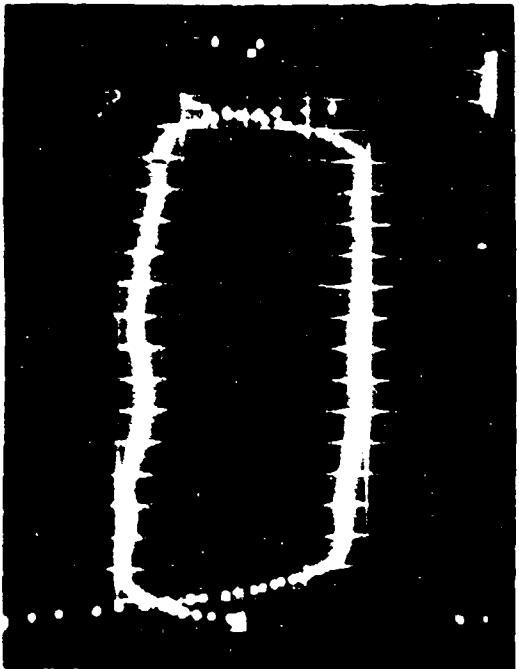
CALL #87



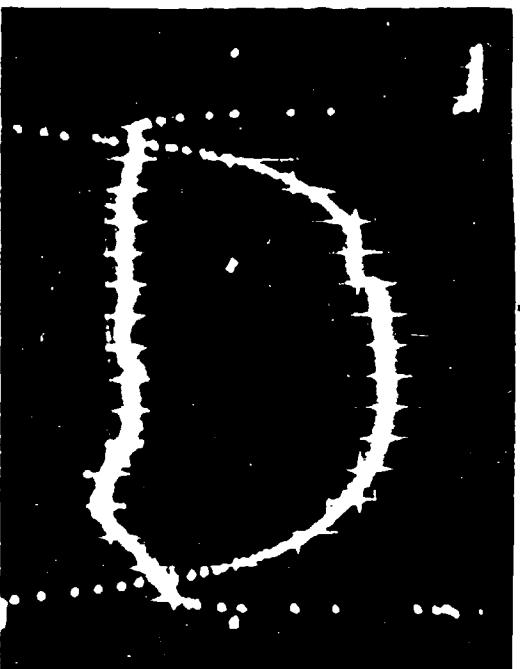
CALL #84



CALL #86



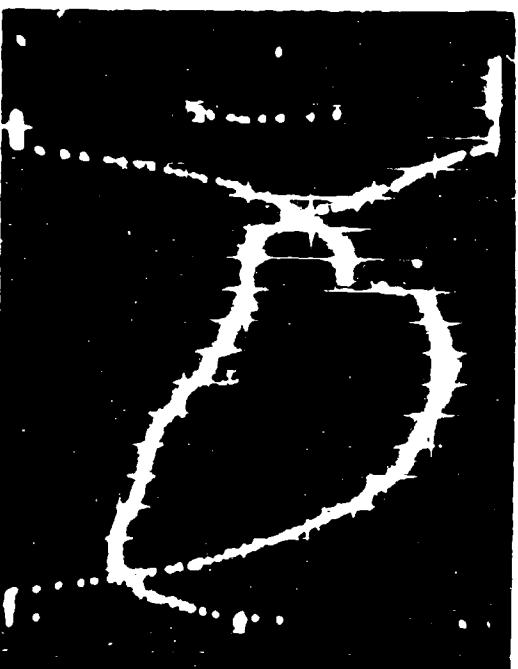
CALL #89



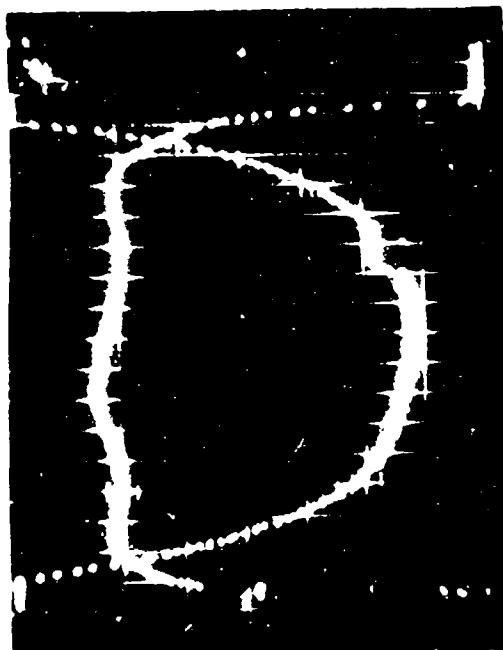
CALL #91



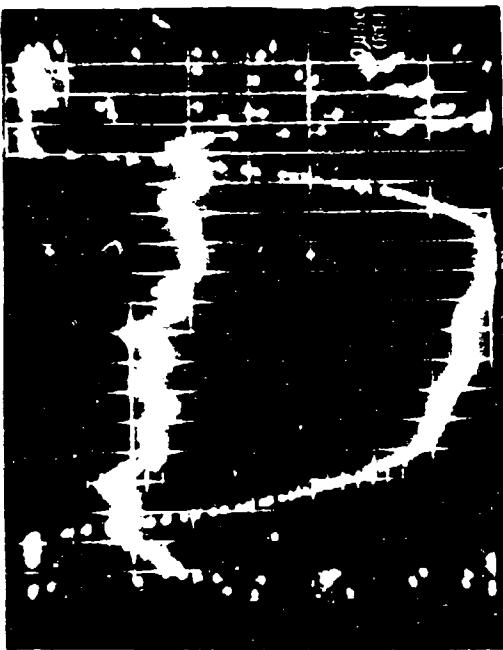
CALL #88



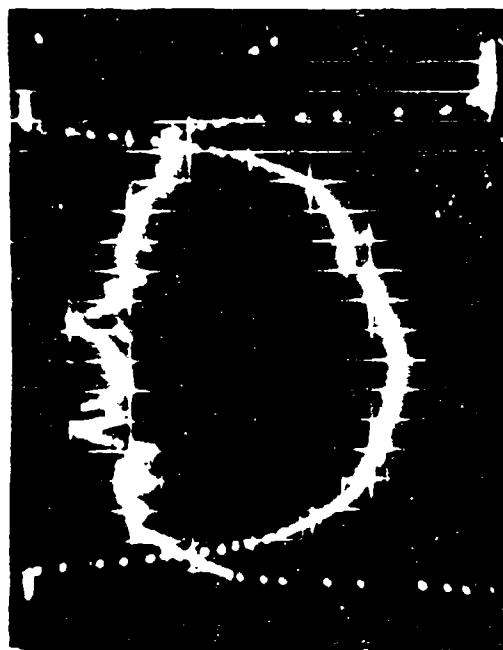
CALL #90



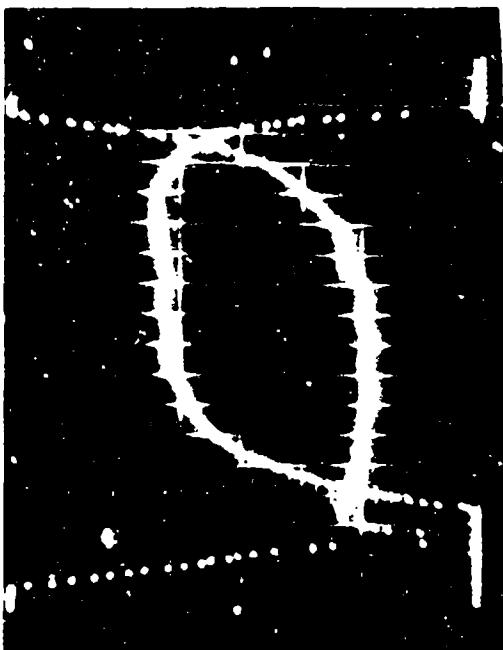
CALL #93



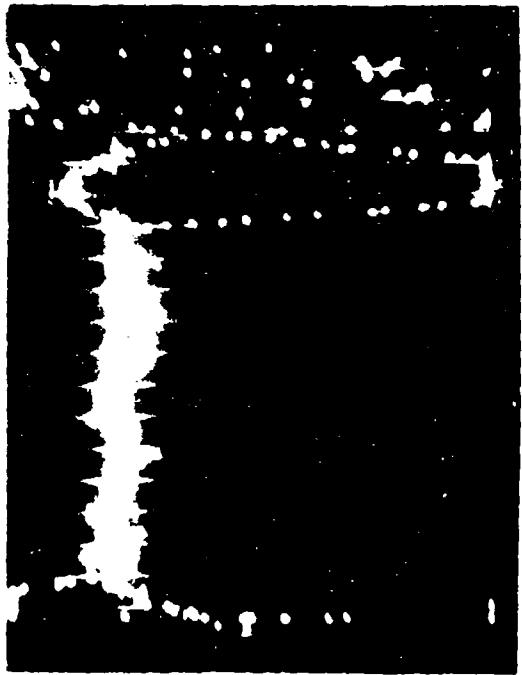
CALL #95



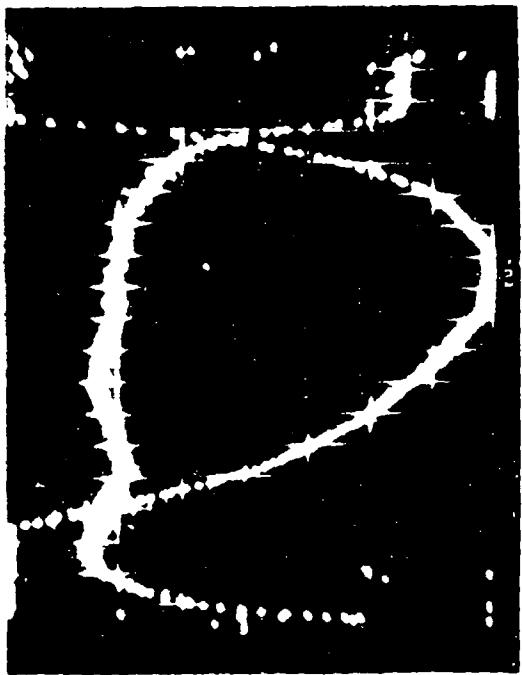
CALL #92



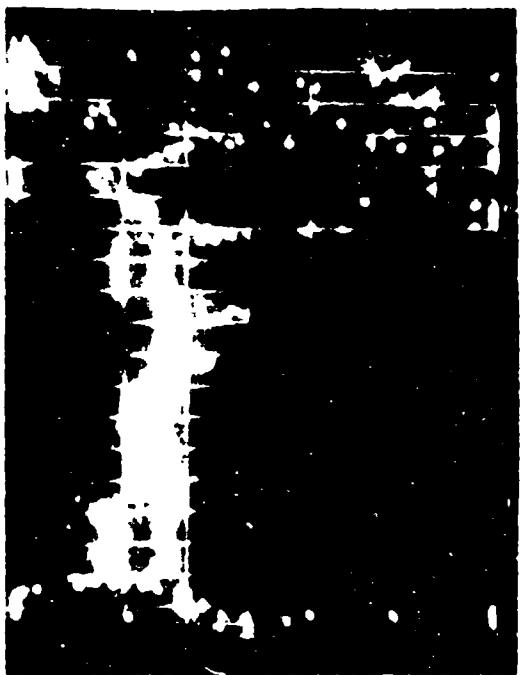
CALL #94



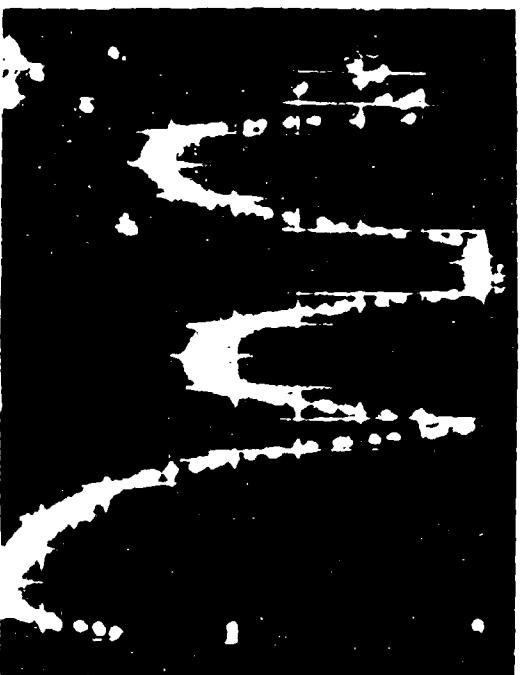
CALL #97



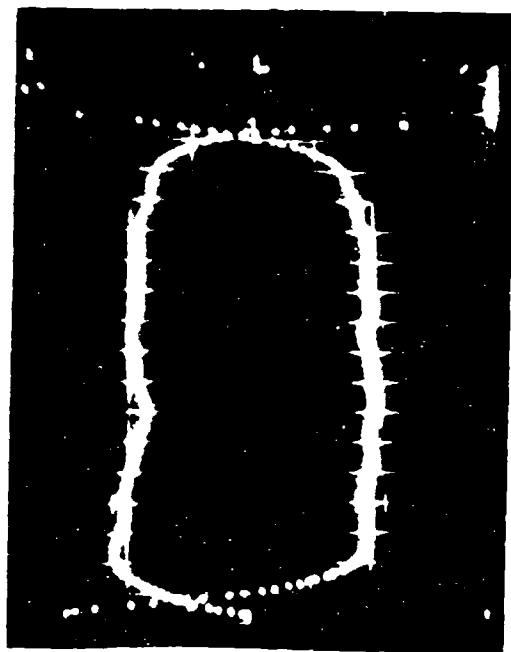
CALL #99



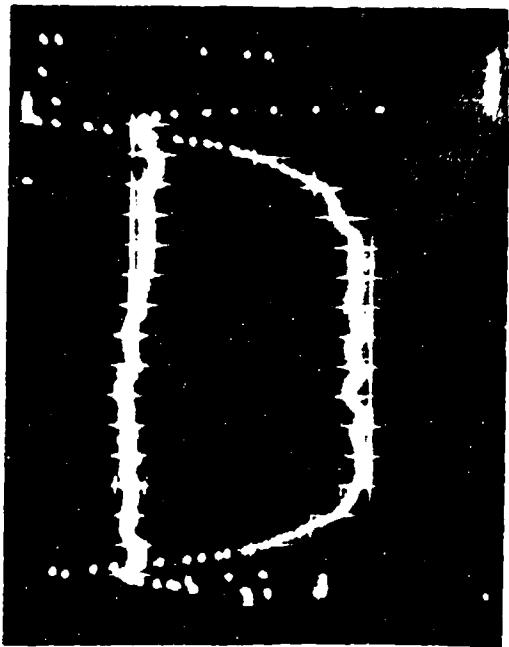
CALL #96



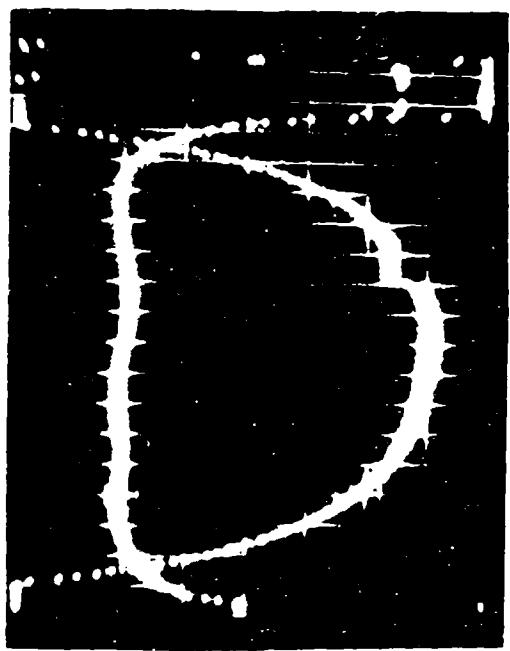
CALL #98 X (AMP)



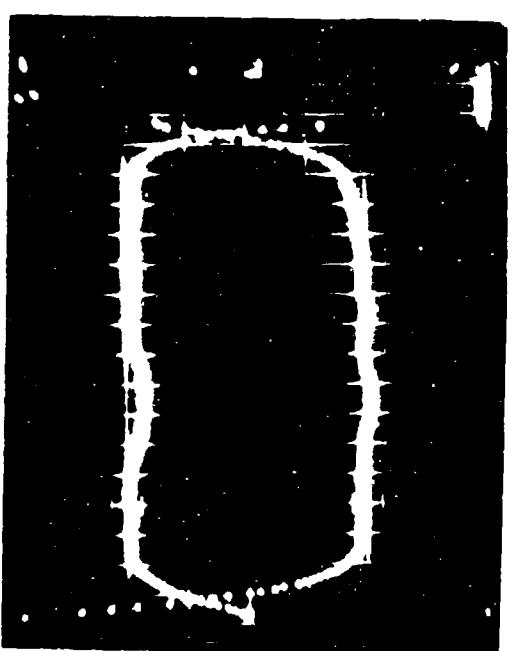
CALL #101



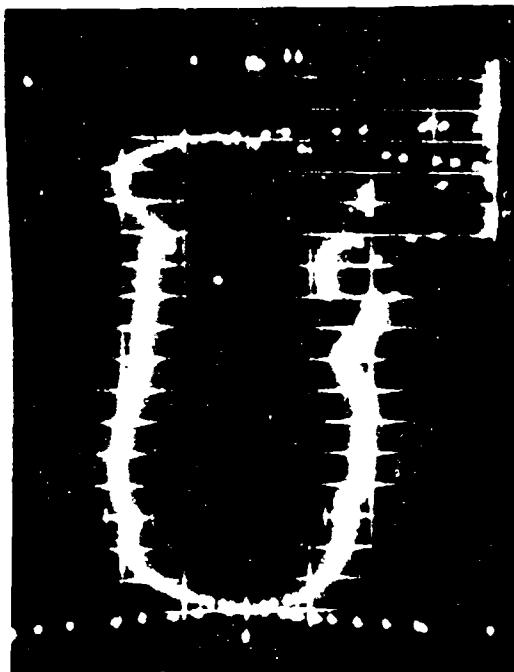
CALL #103



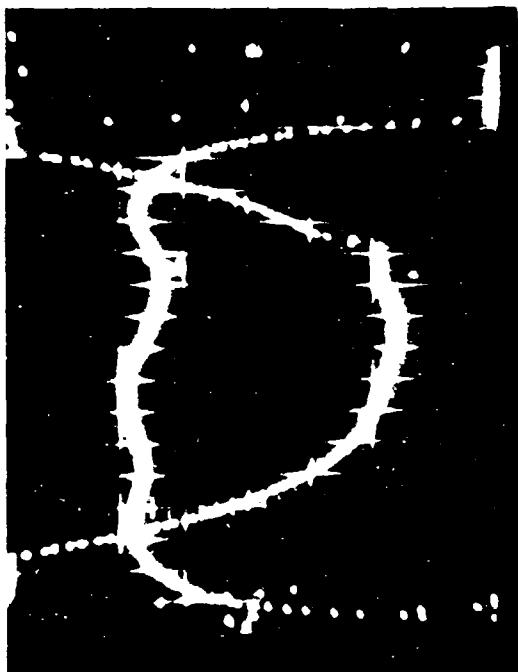
CALL #100



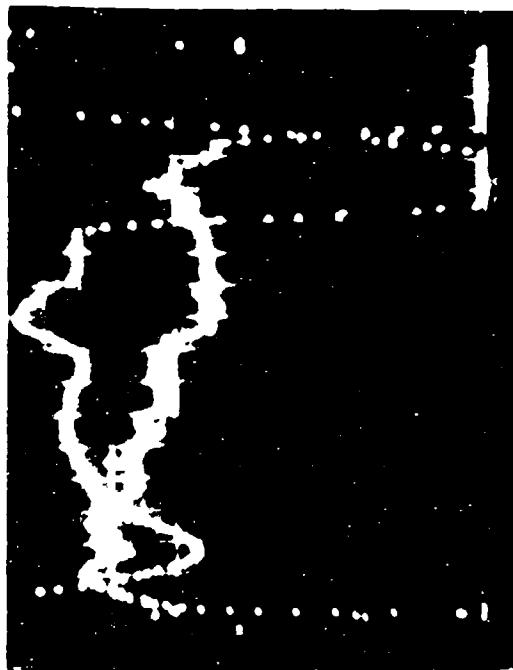
CALL #102



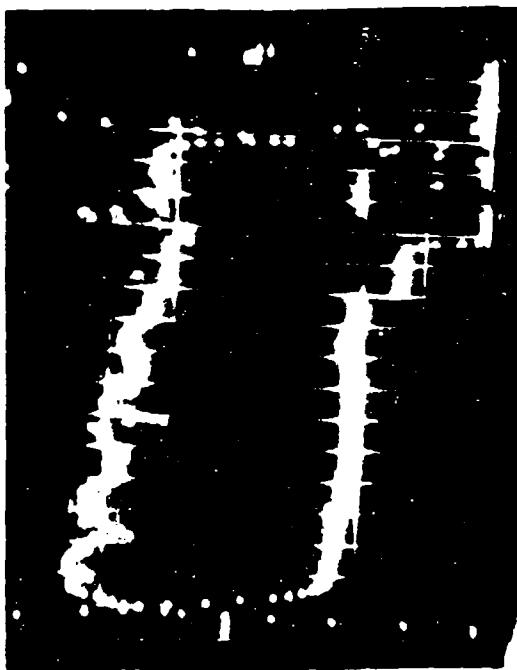
CALL #106



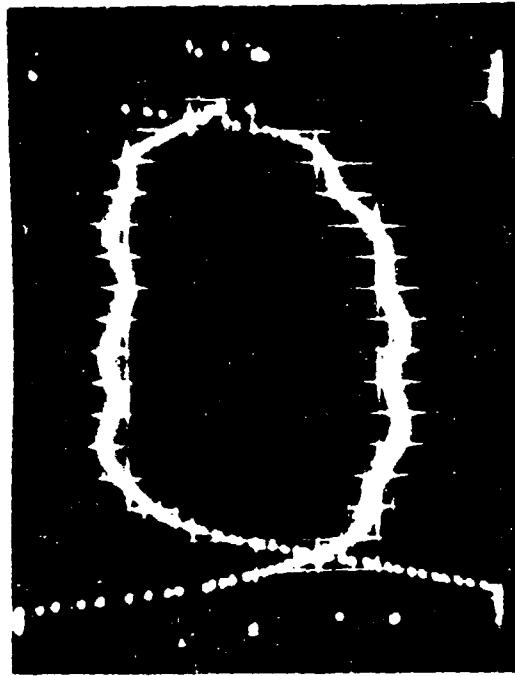
CALL #108



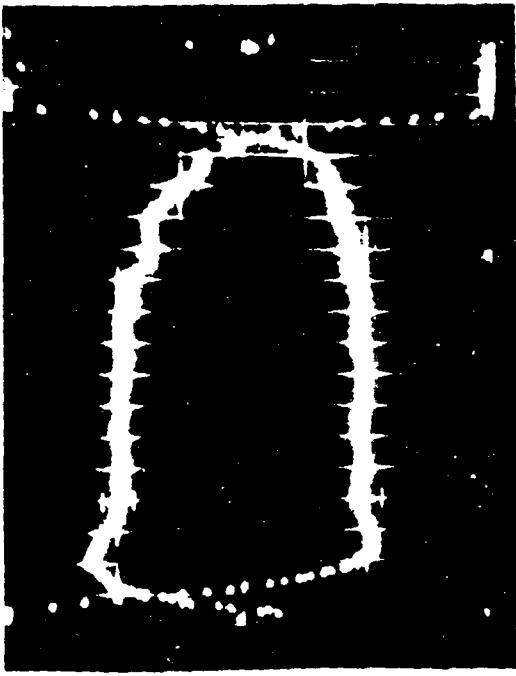
CALL #104



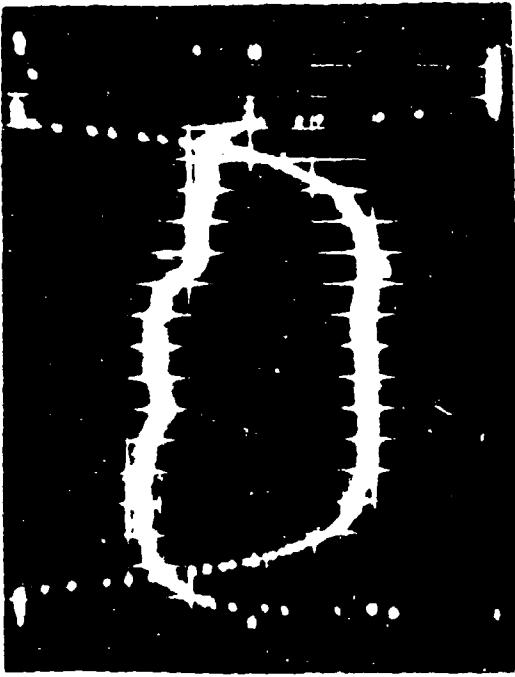
CALL #107



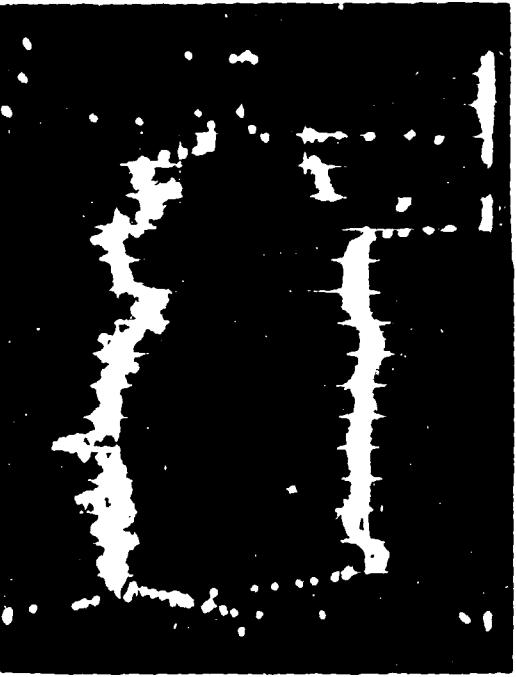
CALL #110



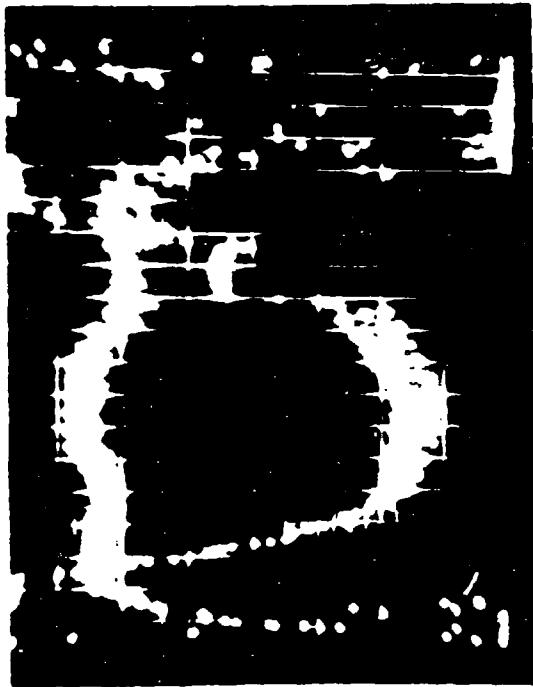
CALL #112



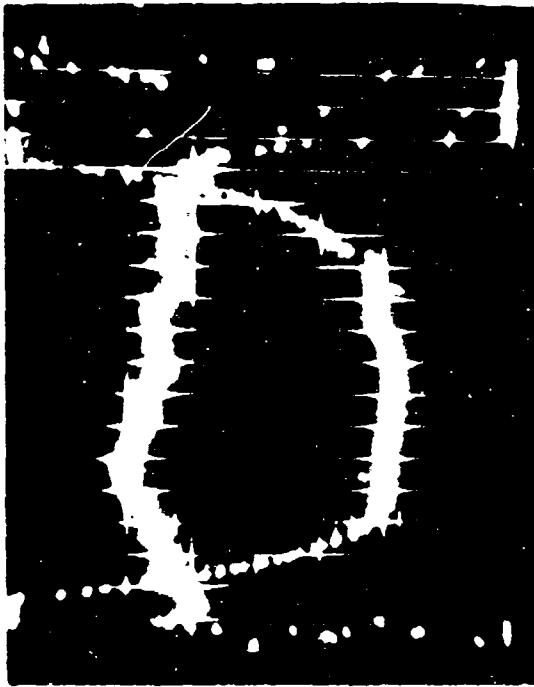
CALL #109



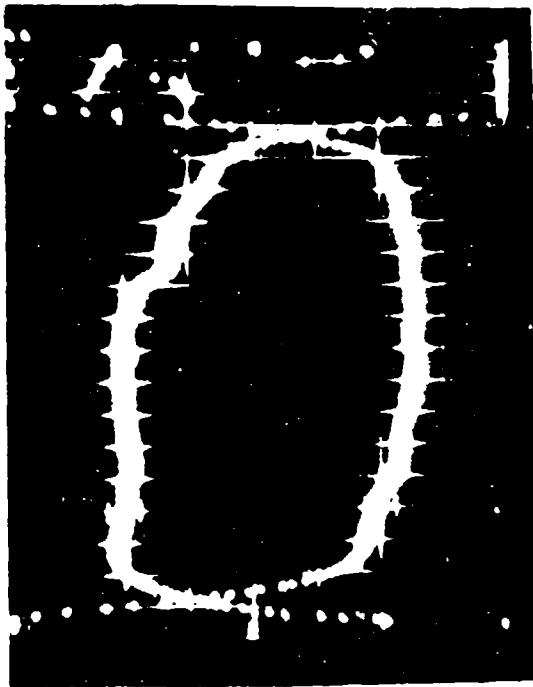
CALL #111



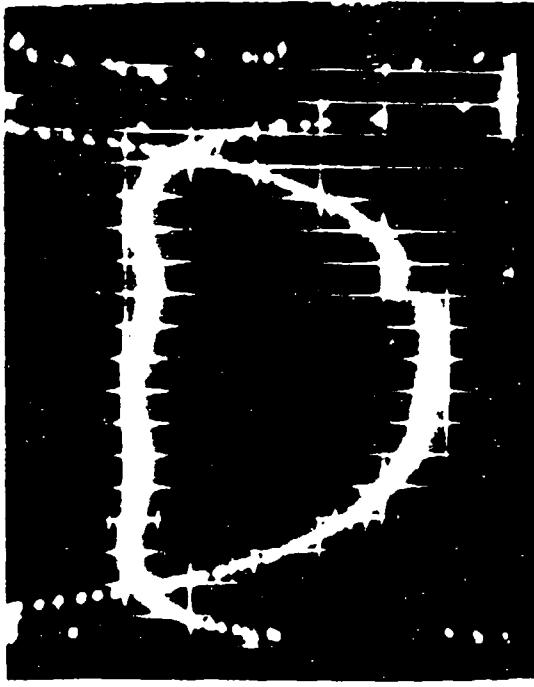
CALL #115



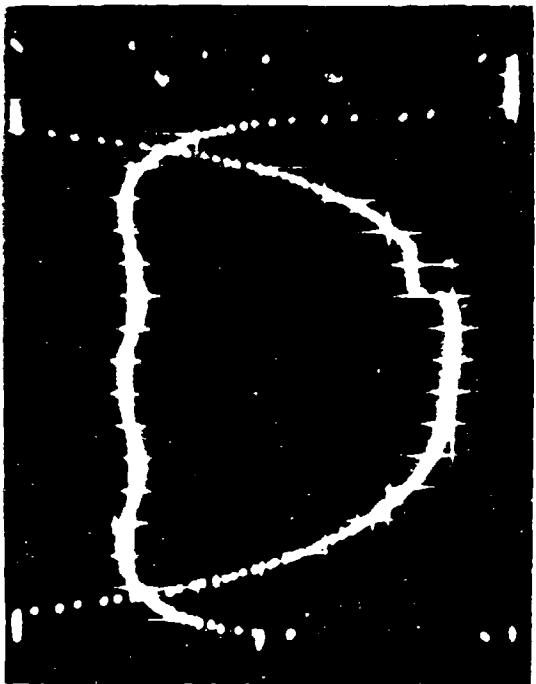
CALL #117



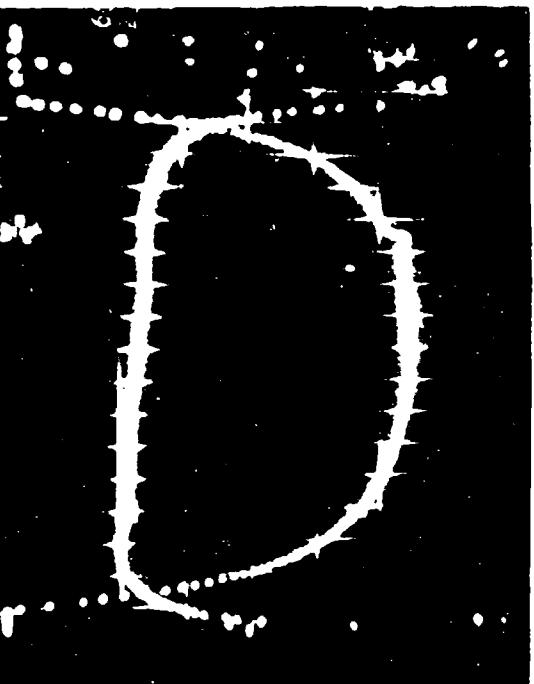
CALL #113



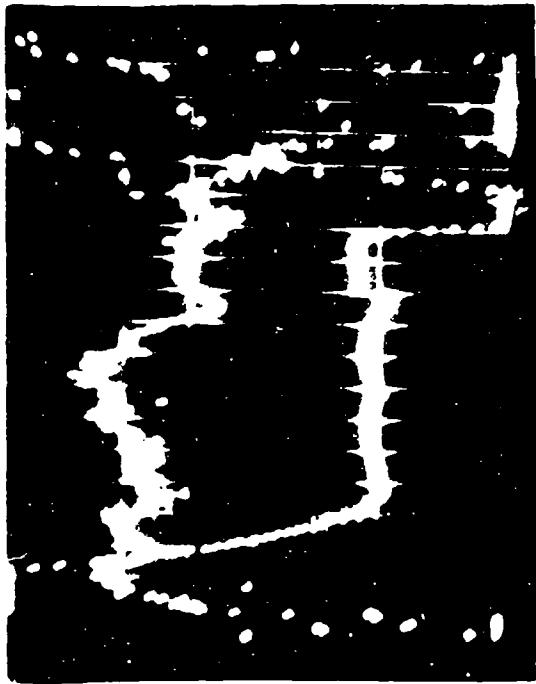
CALL #116



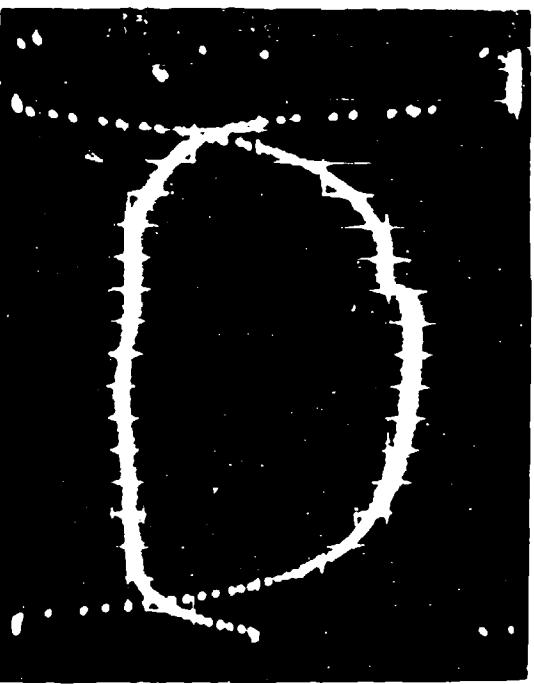
CALL #123



CALL #125



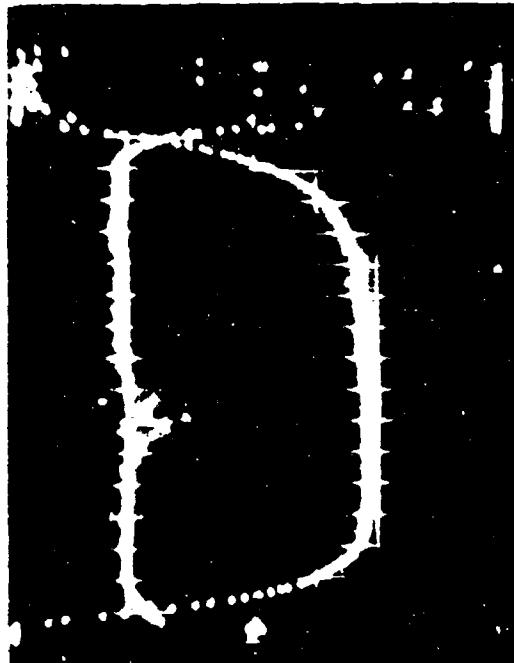
CALL #120



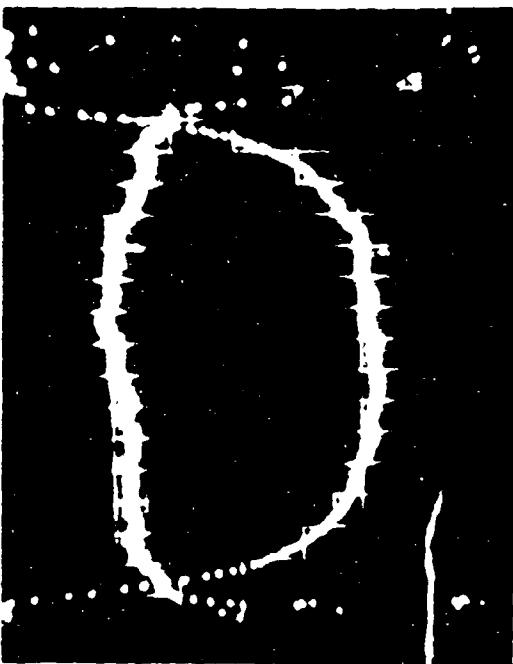
CALL #124



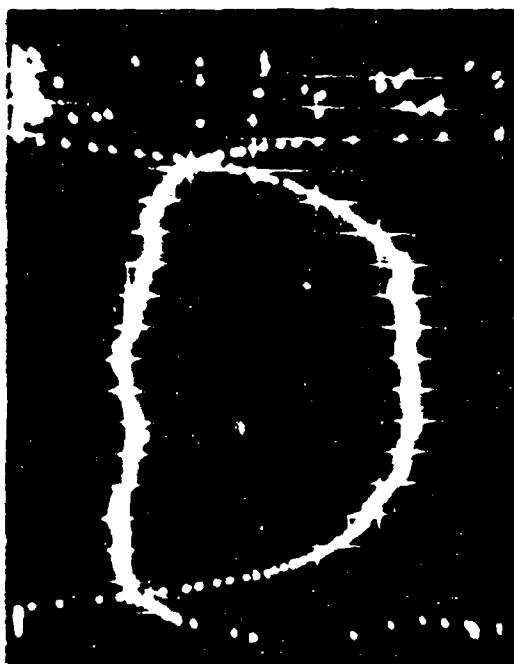
CALL #127



CALL #129



CALL #126



CALL #128



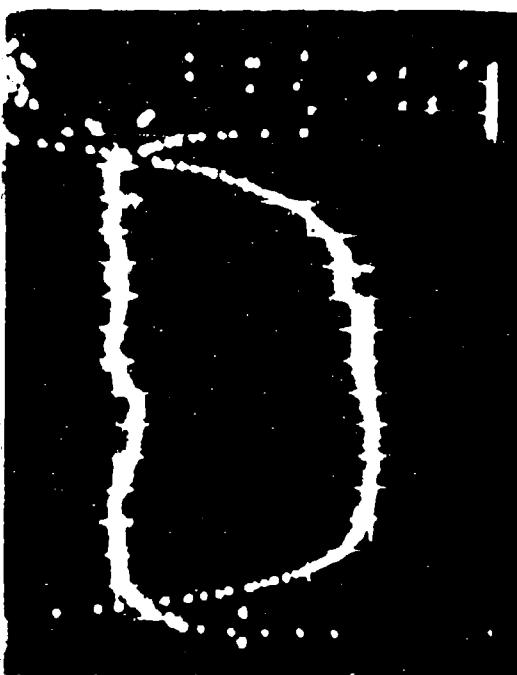
CALL #129B



CALL #131



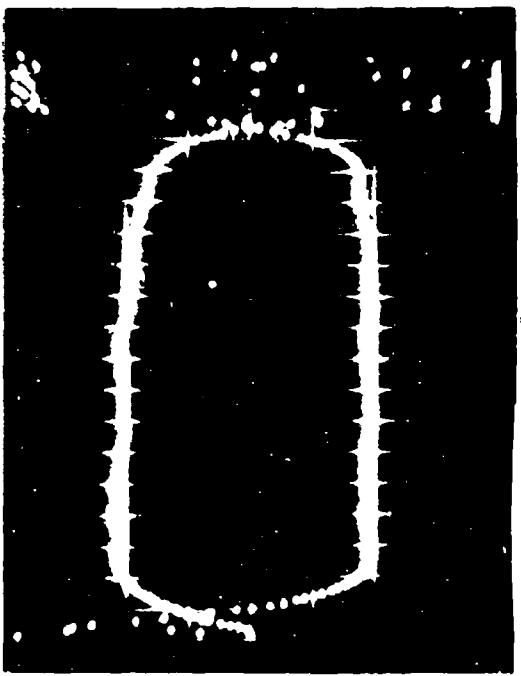
CALL #129A



CALL #130



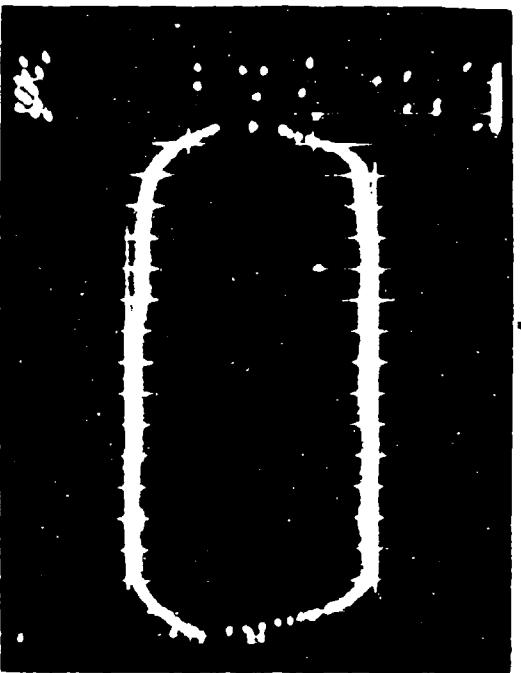
CALL #133



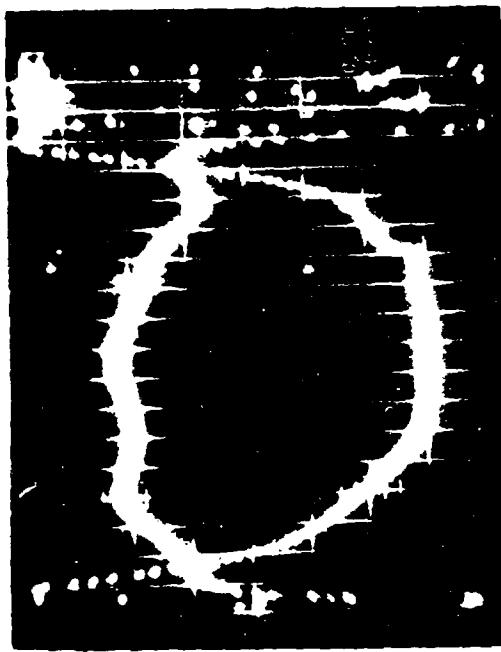
CALL #136



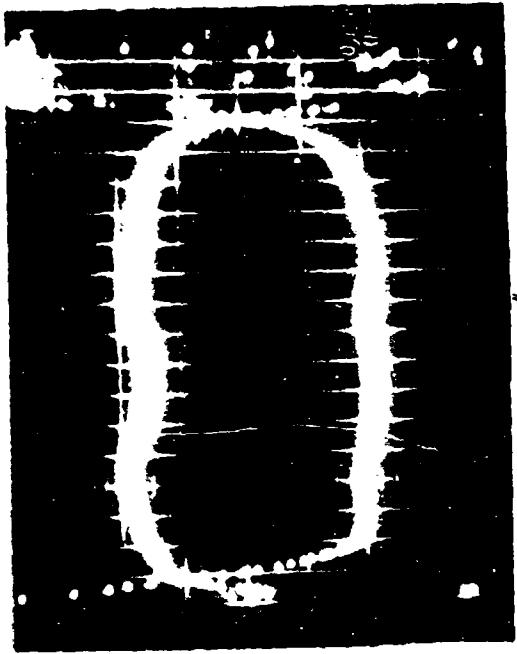
CALL #132



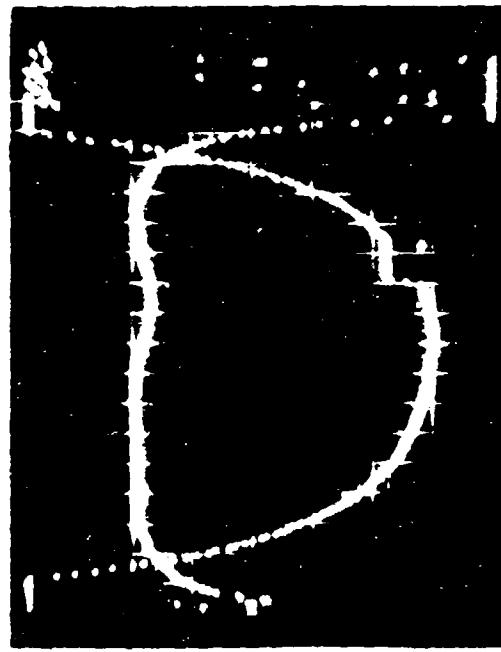
CALL #135



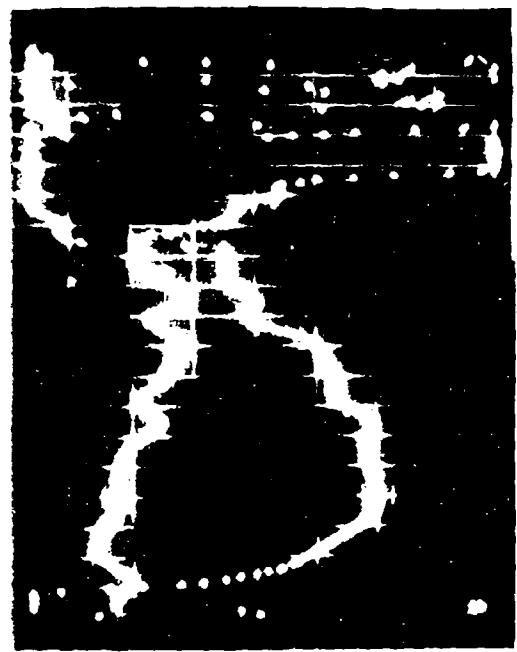
CALL #138



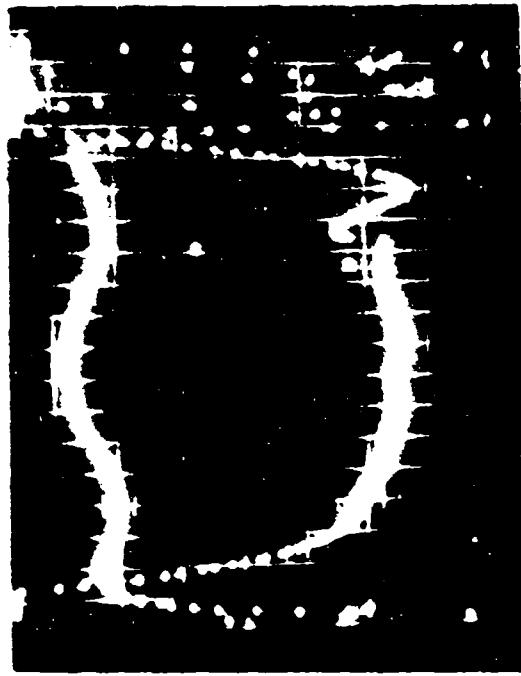
CALL #140



CALL #137



CALL #139



CALL #142



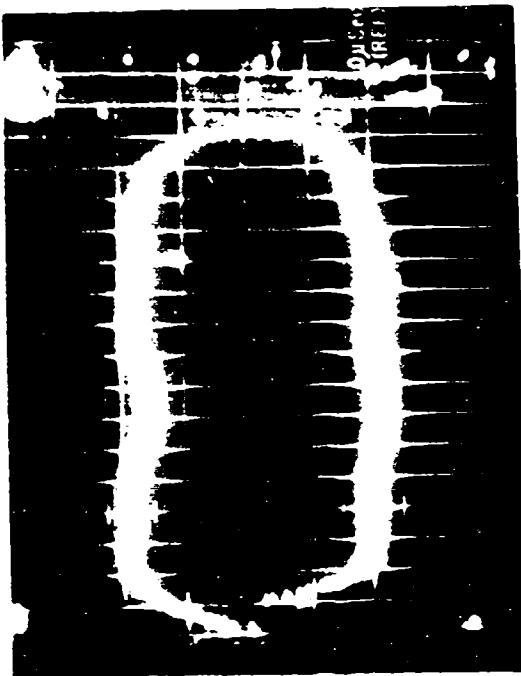
CALL #144



CALL #141



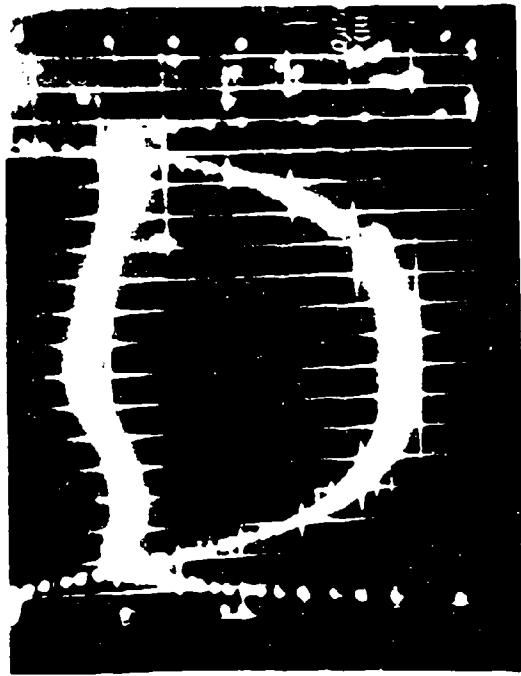
CALL #143



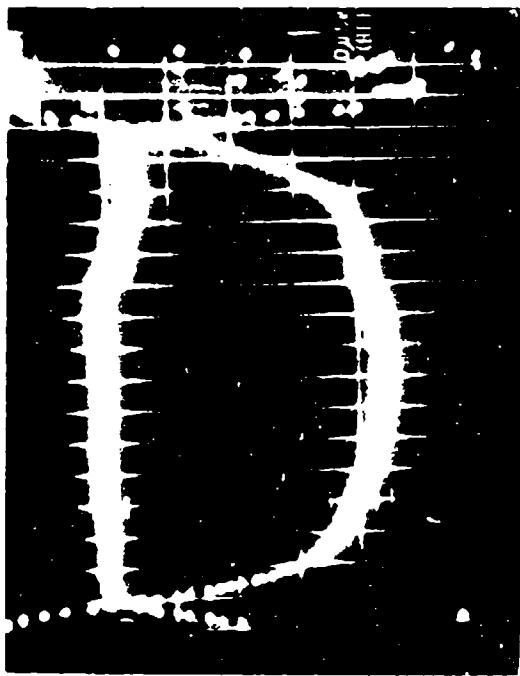
CALL #146



CALL #148



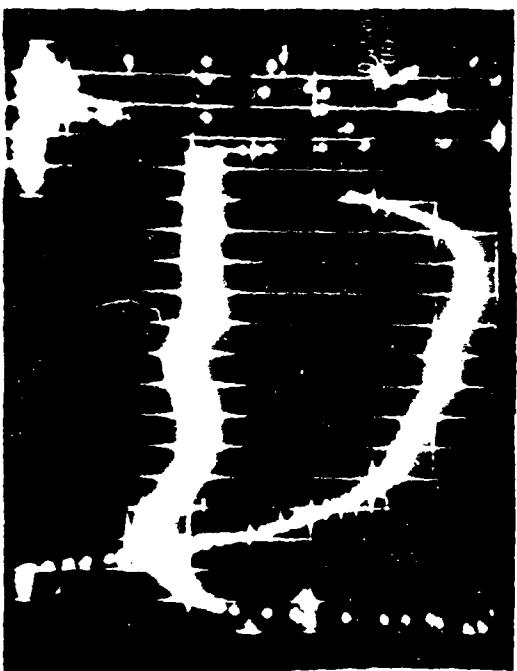
CALL #145



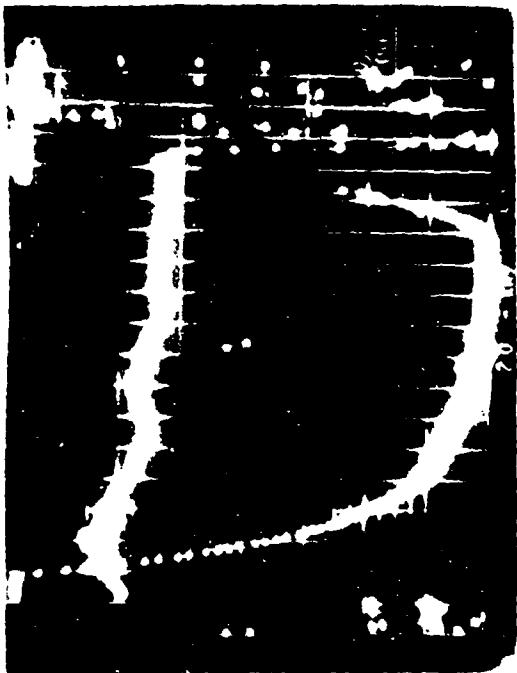
CALL #147



CALL #151



CALL #153



CALL #149



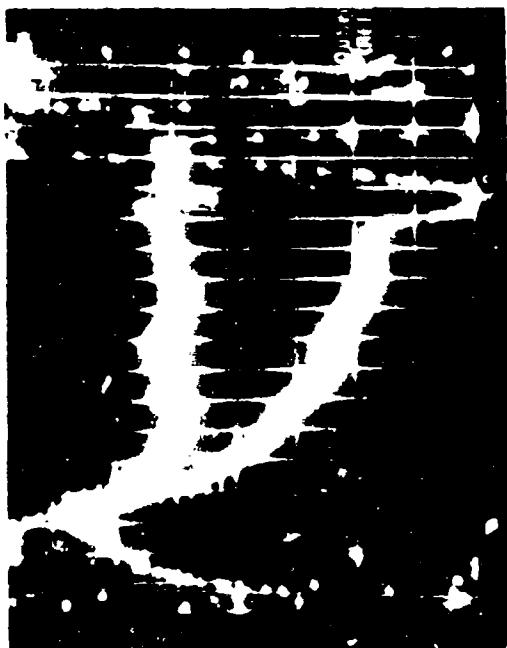
CALL #152



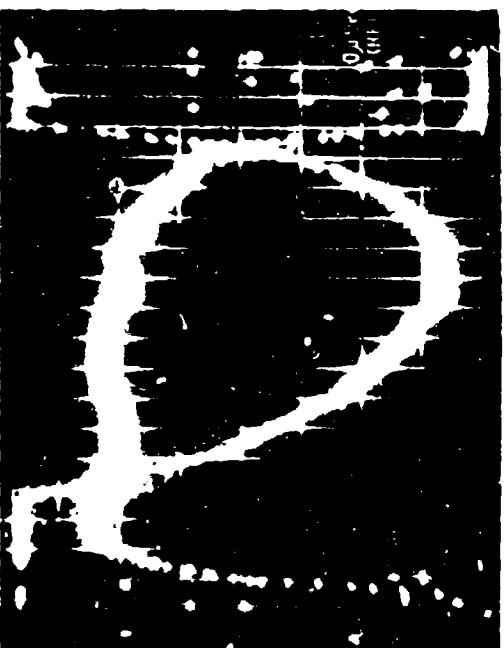
CALL #155



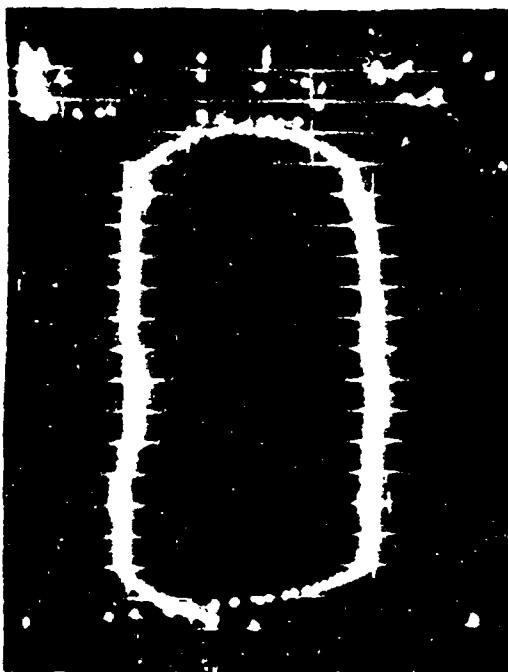
CALL #157



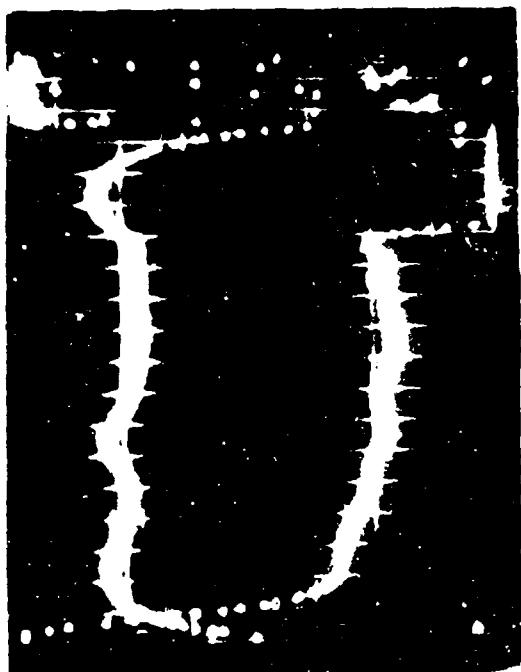
CALL #154



CALL #156



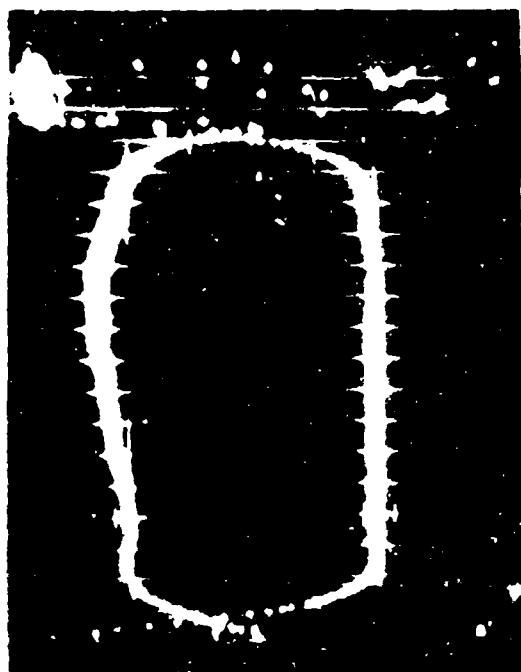
CALL #159



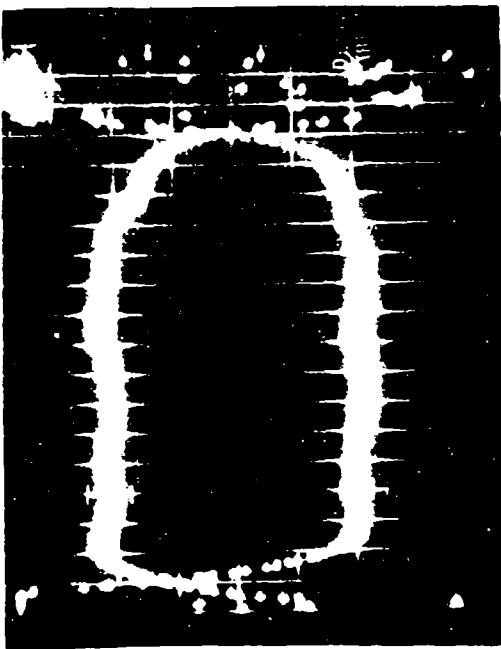
CALL #161



CALL #158



CALL #160



CALL #164



CALL #167



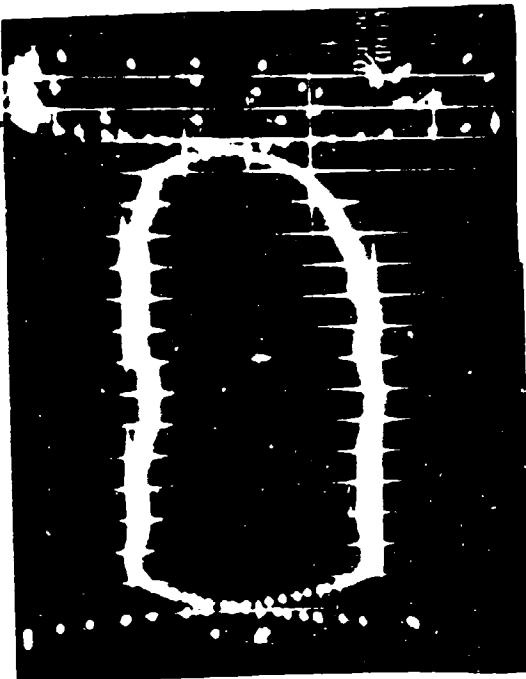
CALL #162



CALL #165



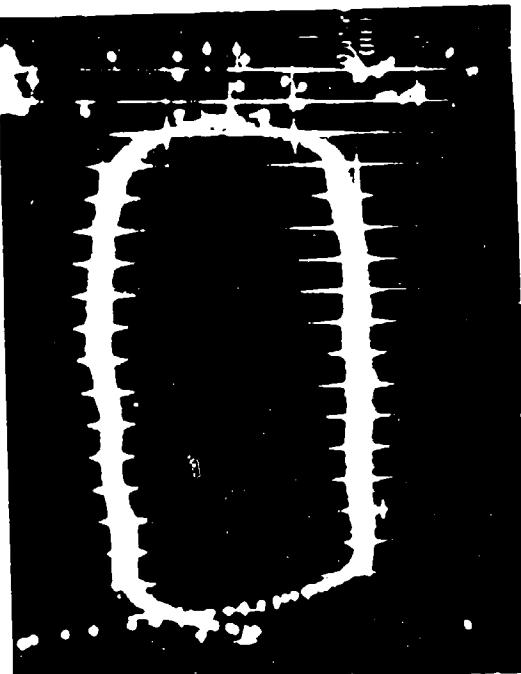
CALL #169



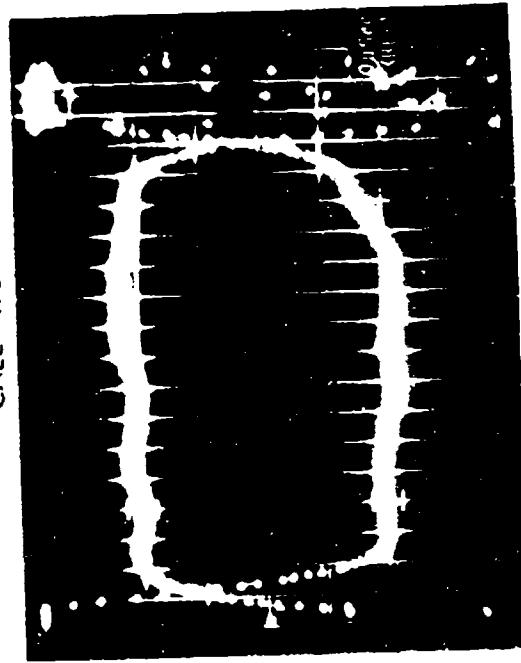
CALL #171



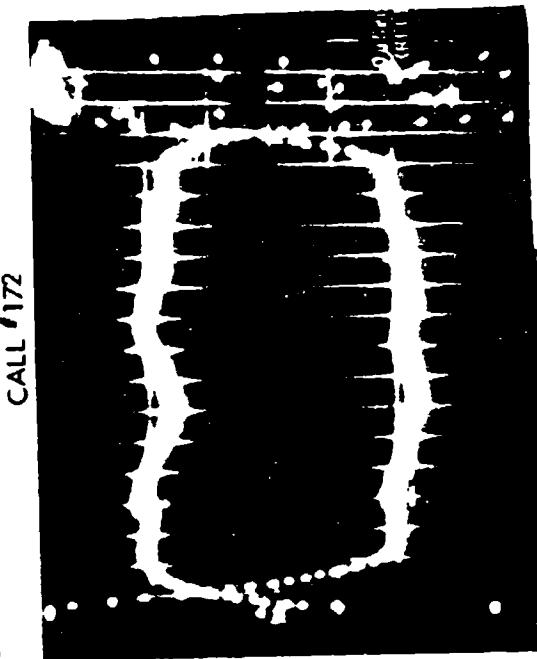
CALL #168



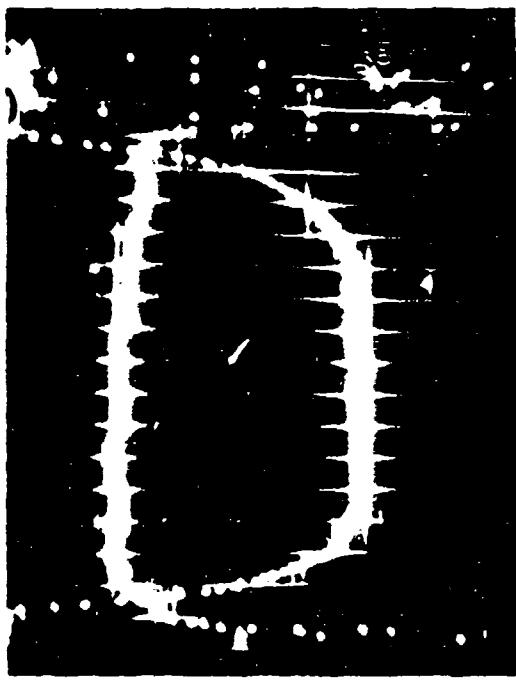
CALL #170



CALL #175



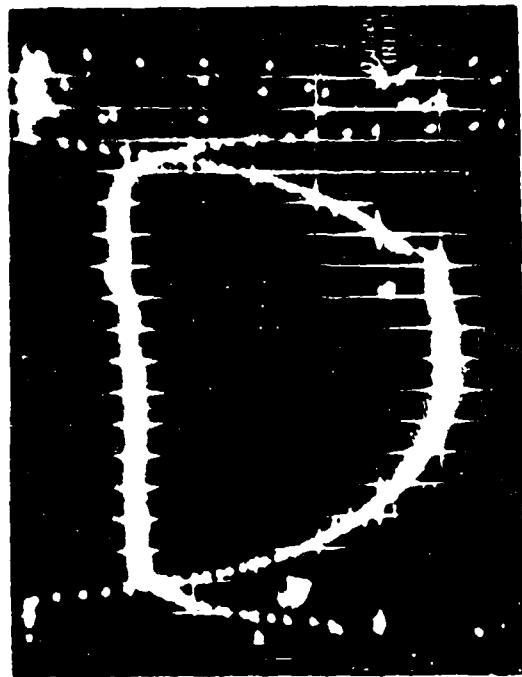
CALL #174



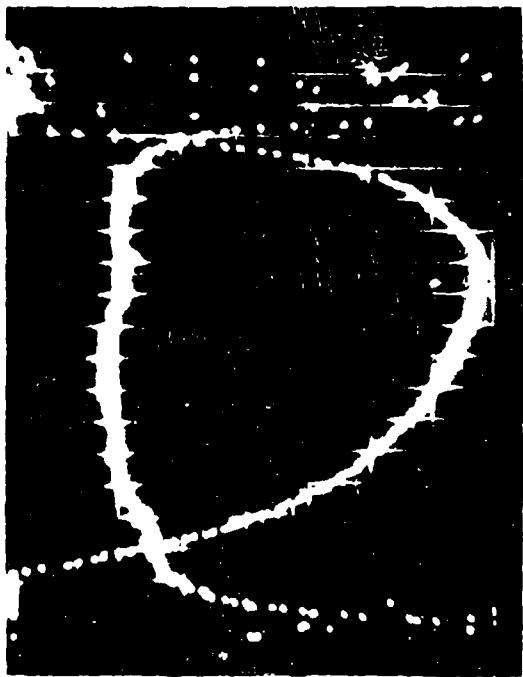
CALL #178



CALL #180



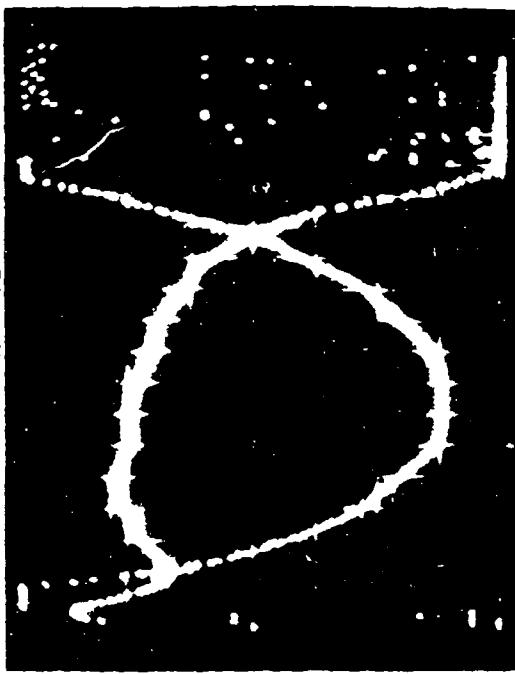
CALL #177



CALL #179



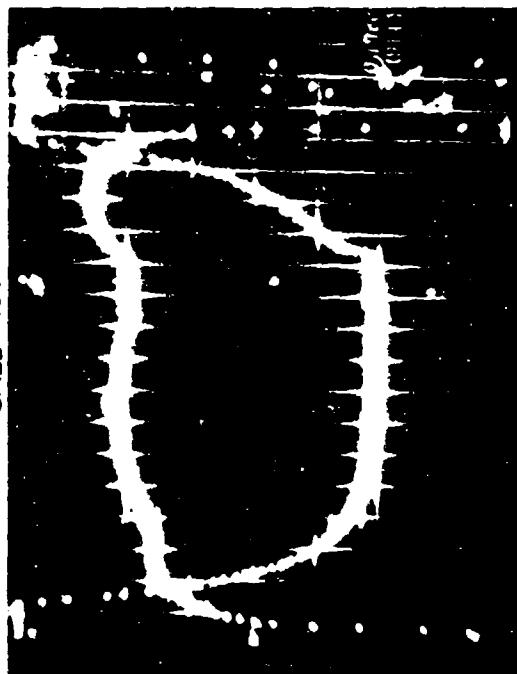
CALL #182



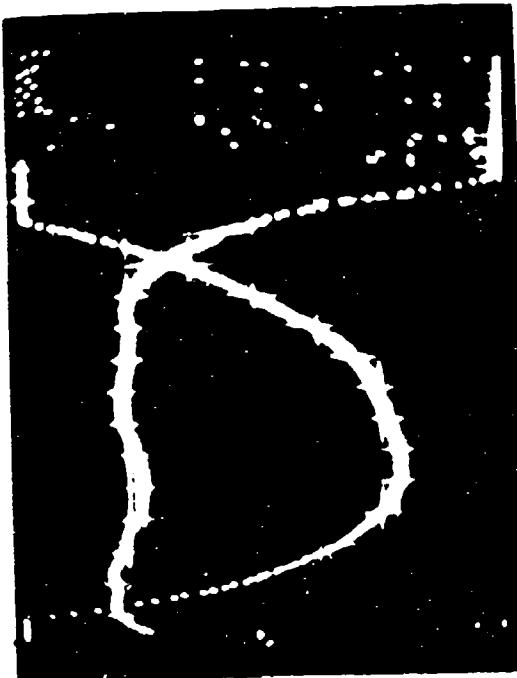
CALL #183A

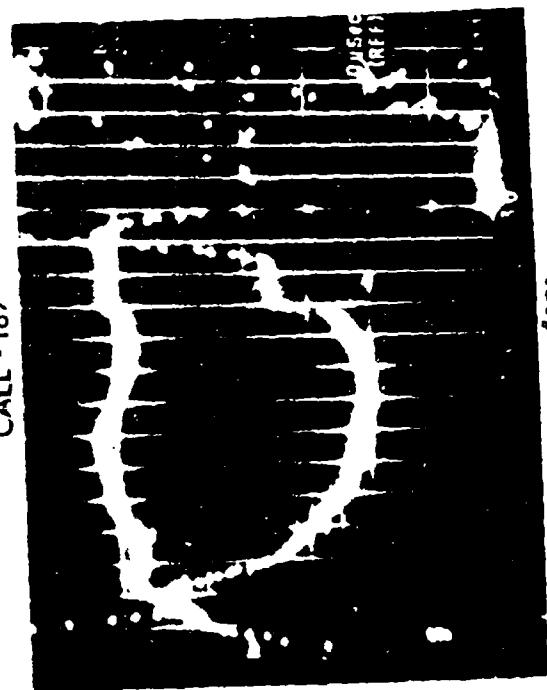
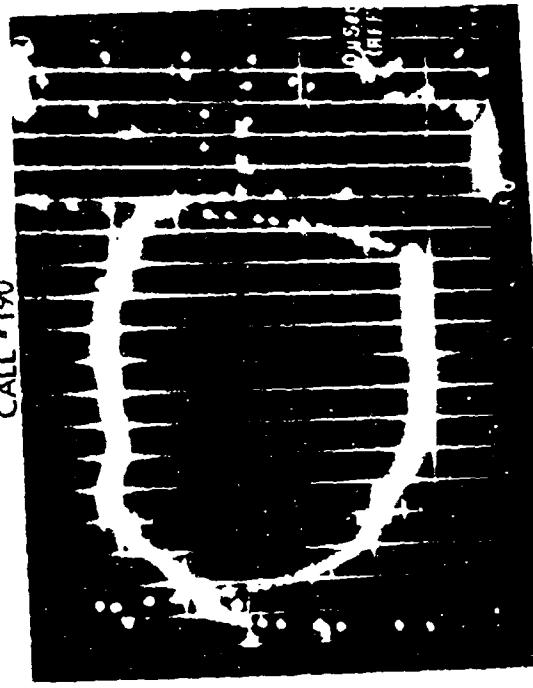


CALL #181

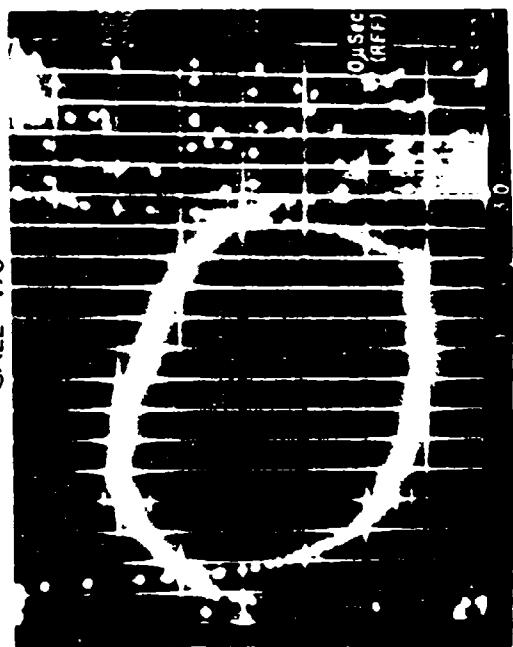
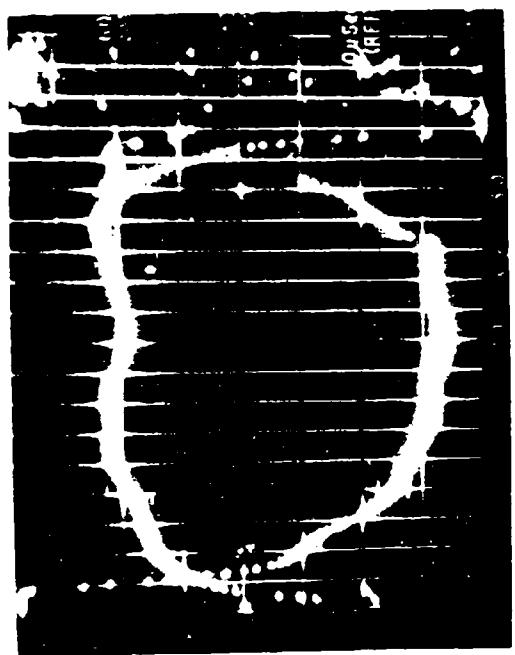


CALL #183

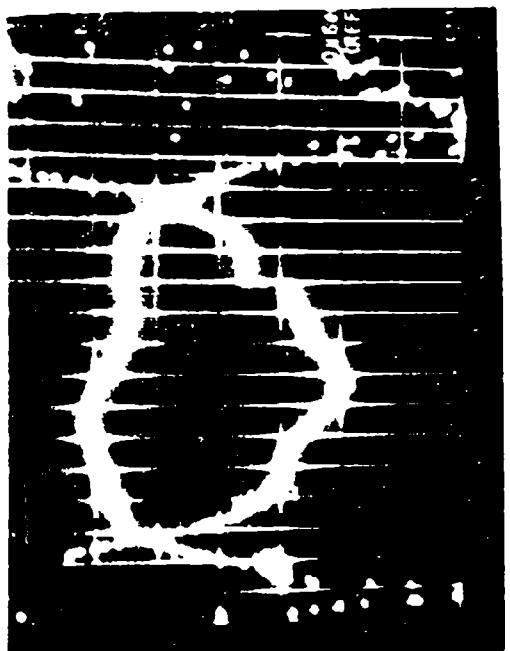








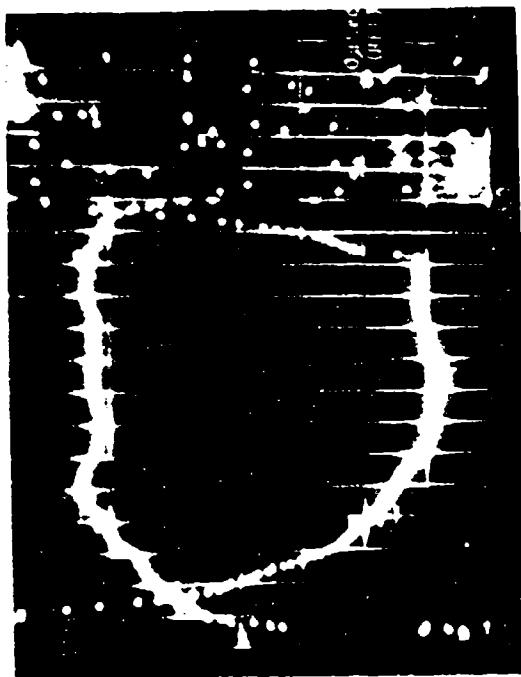
CALL #198



CALL #197



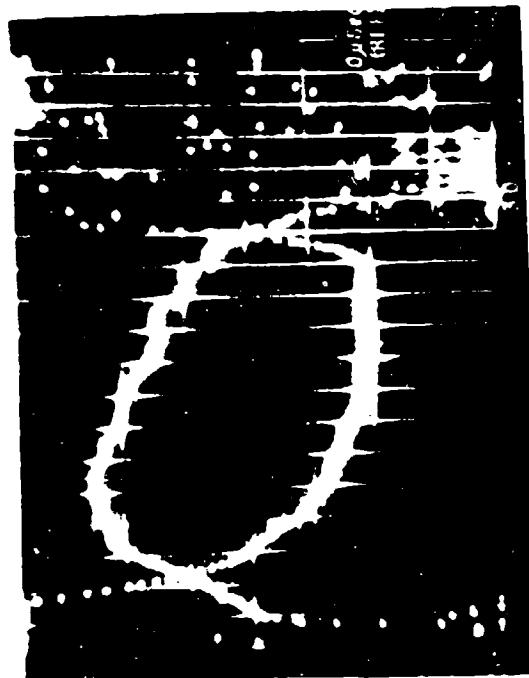
CALL #199



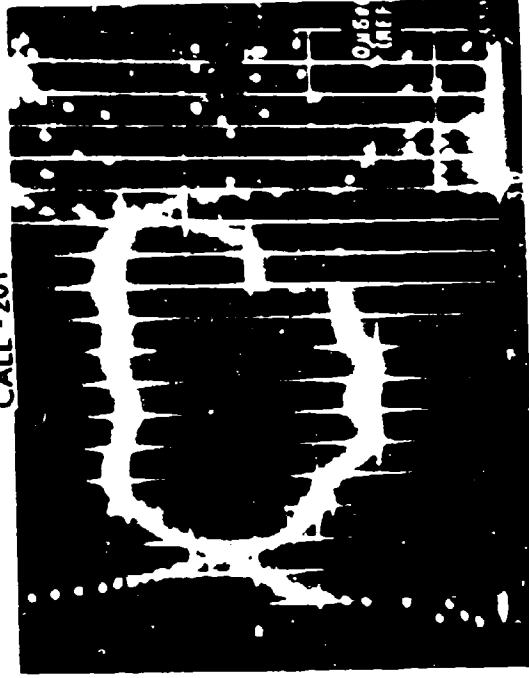
CALL #202



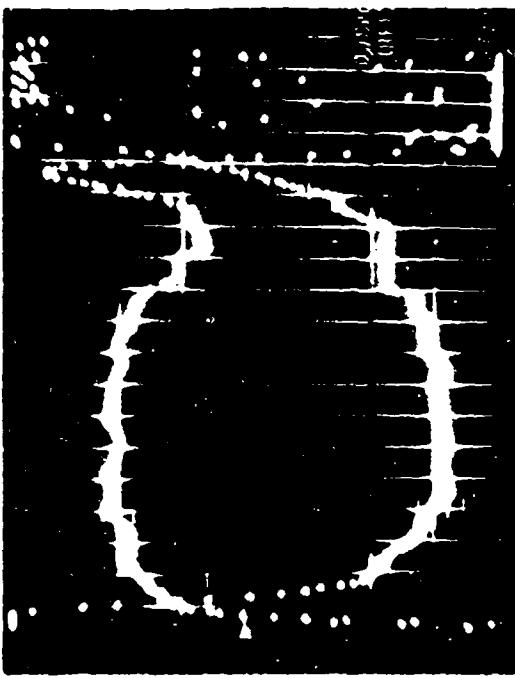
CALL #204



CALL #201

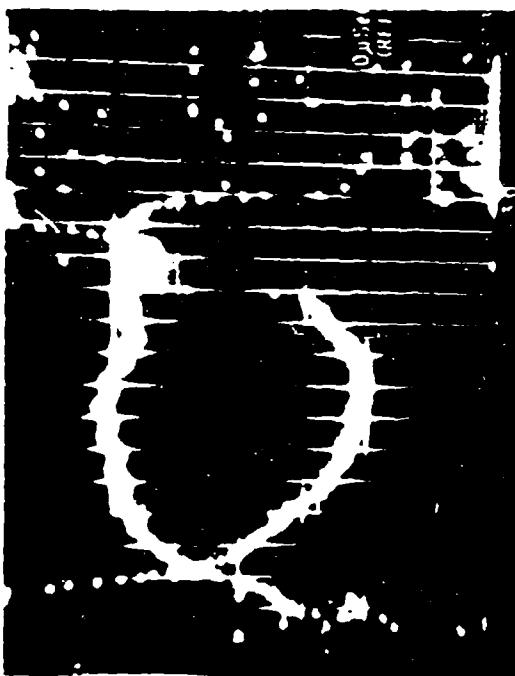


CALL #203



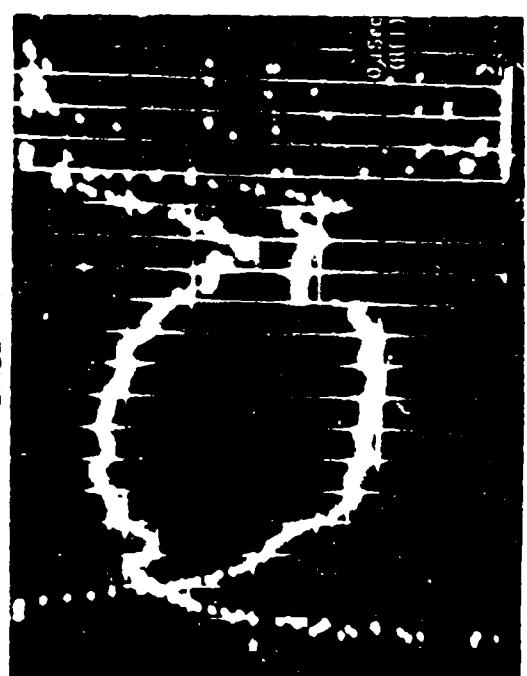
CALL #206

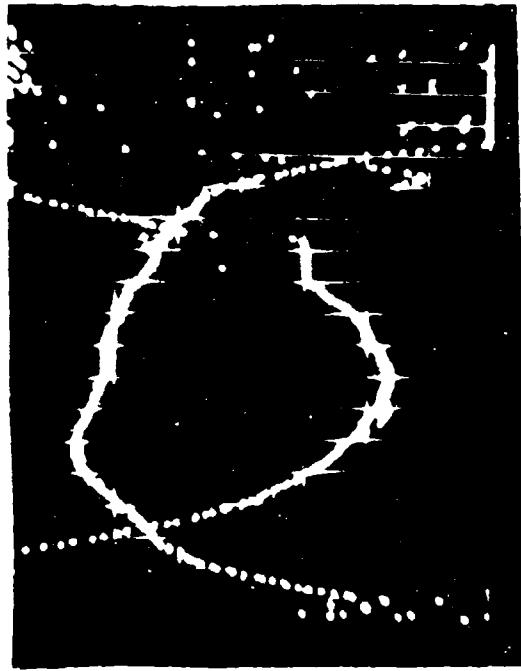
CALL #208



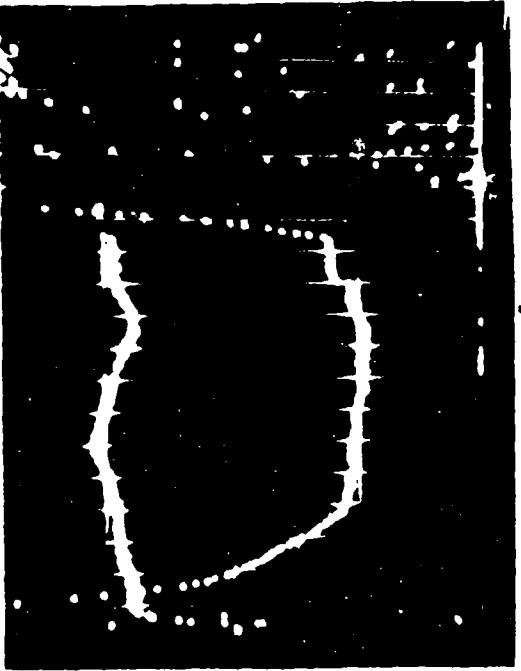
CALL #205

CALL #207





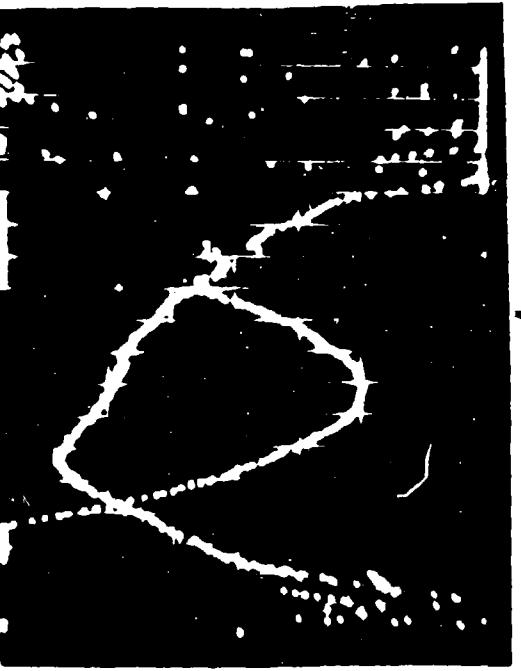
CALL #210



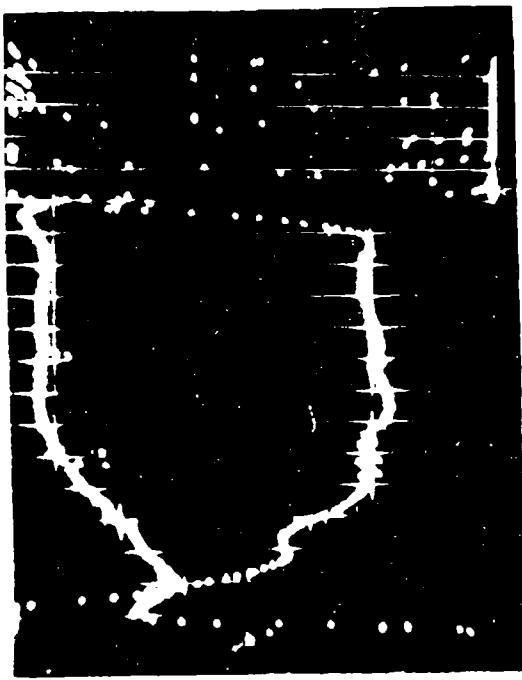
CALL #212



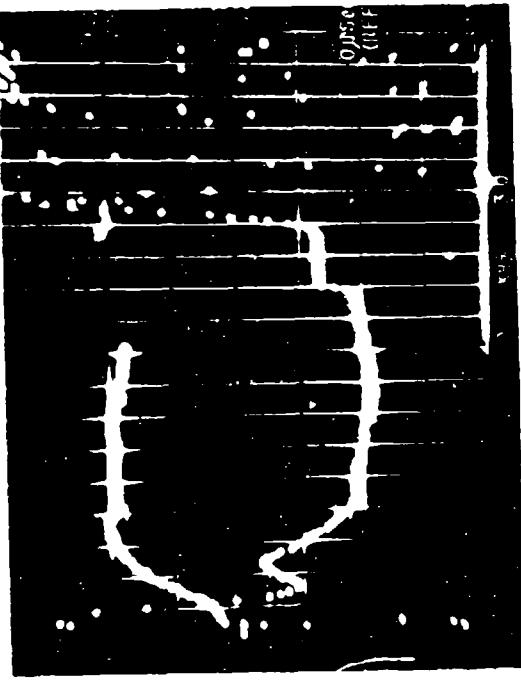
CALL #209



CALL #211



CALL #214



CALL #216



CALL #213



CALL #215



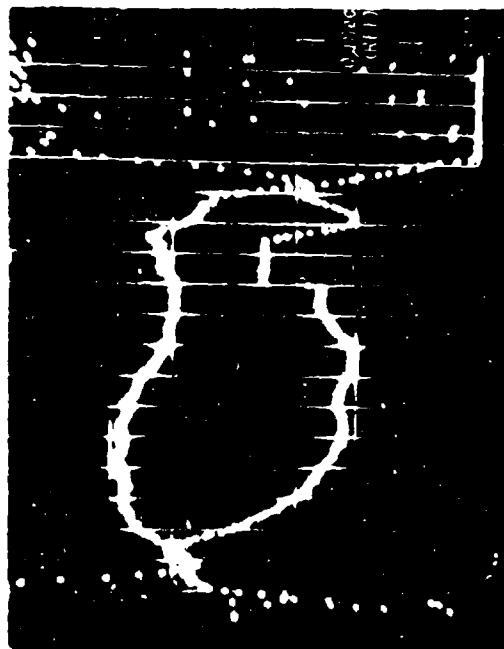
CALL #218



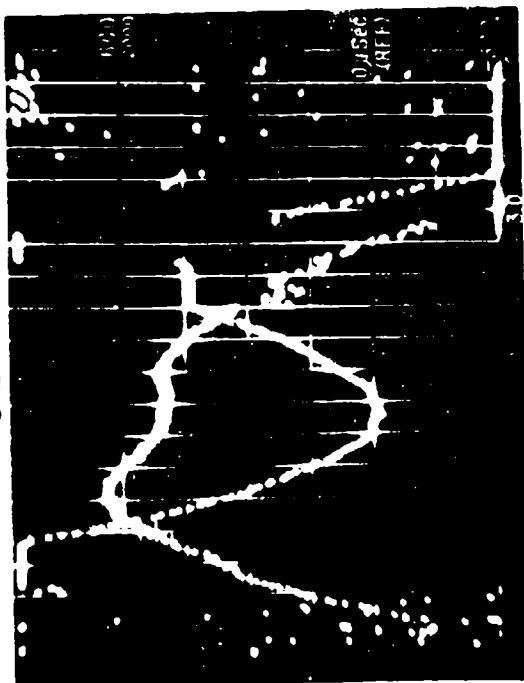
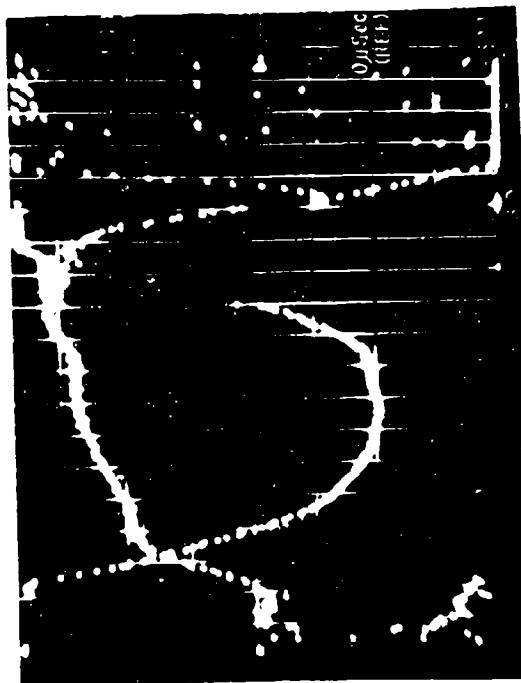
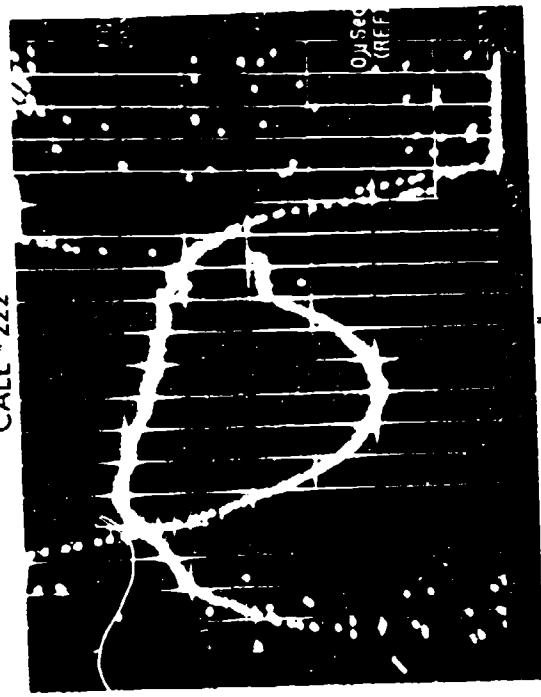
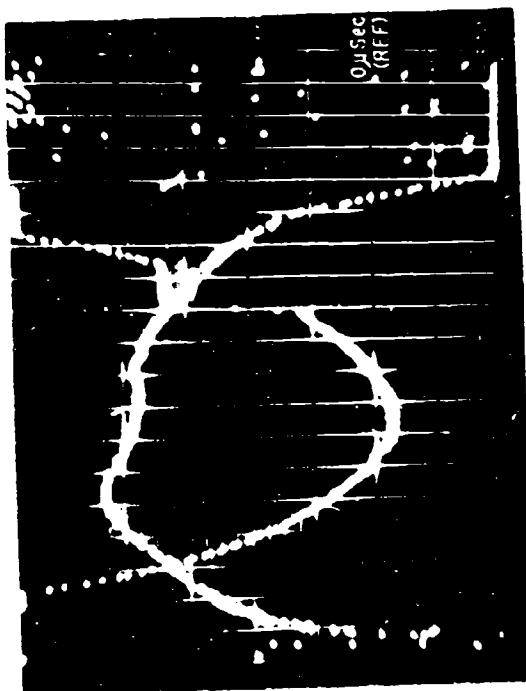
CALL #220

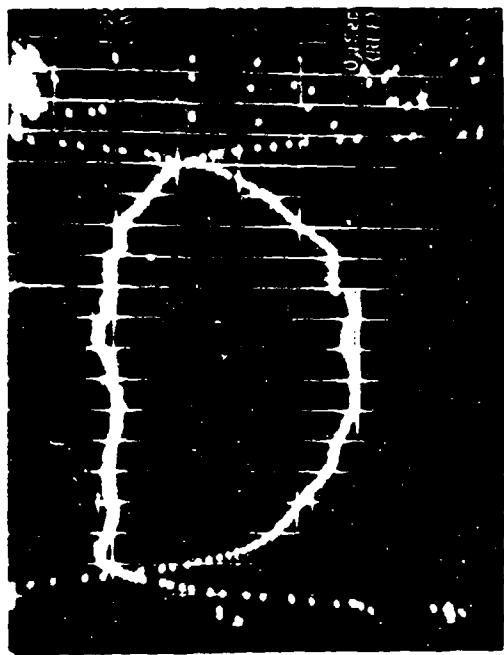


CALL #217

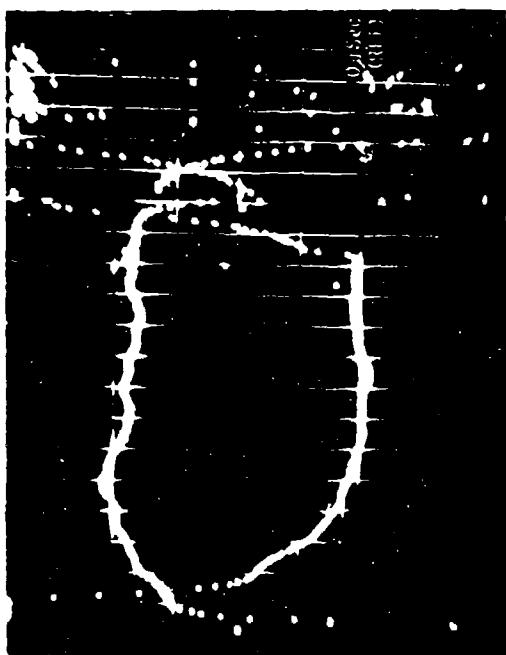


CALL #219

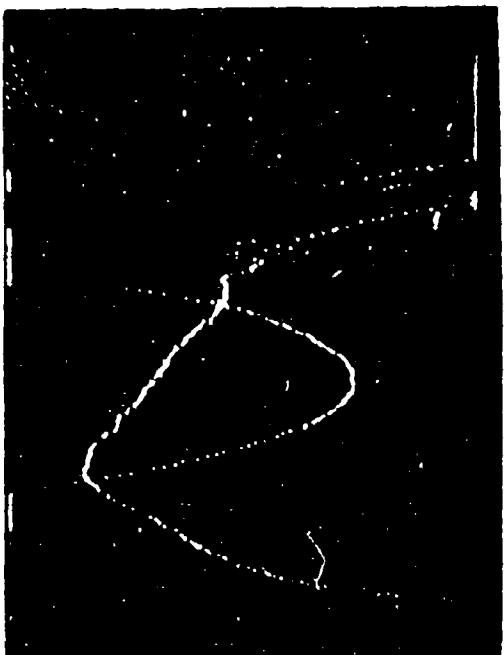




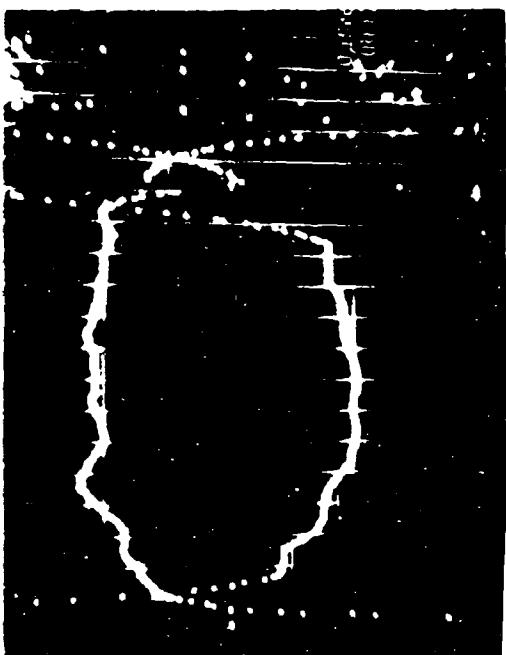
CALL #226



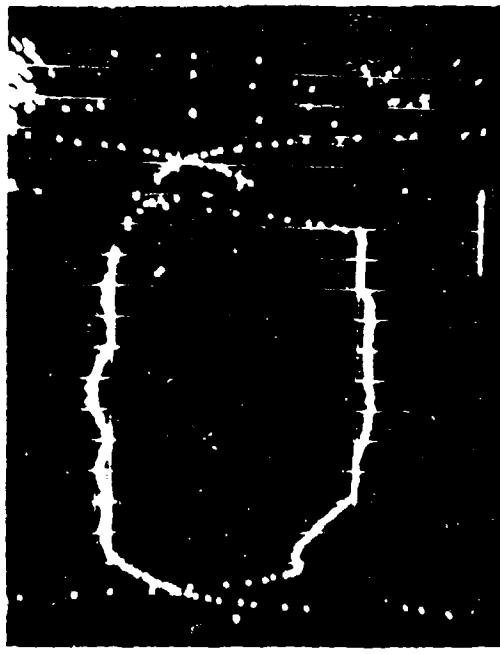
CALL #226



CALL #225



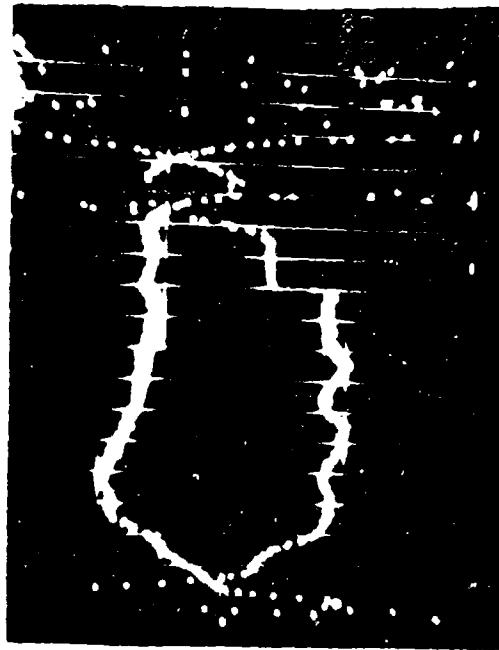
CALL #227



CALL #232



CALL #234



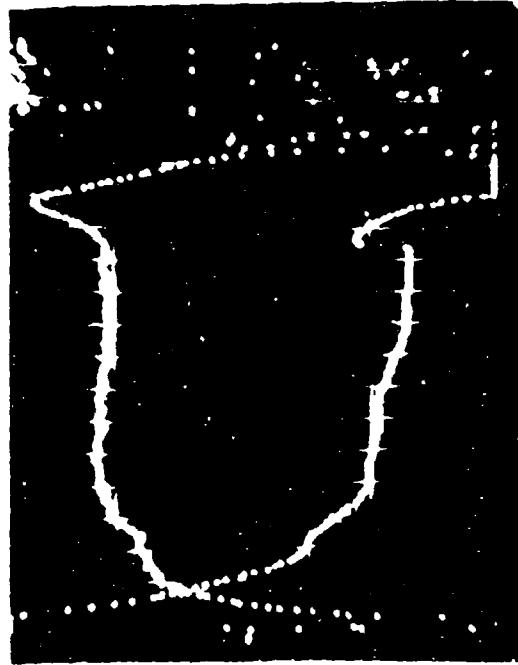
CALL #230



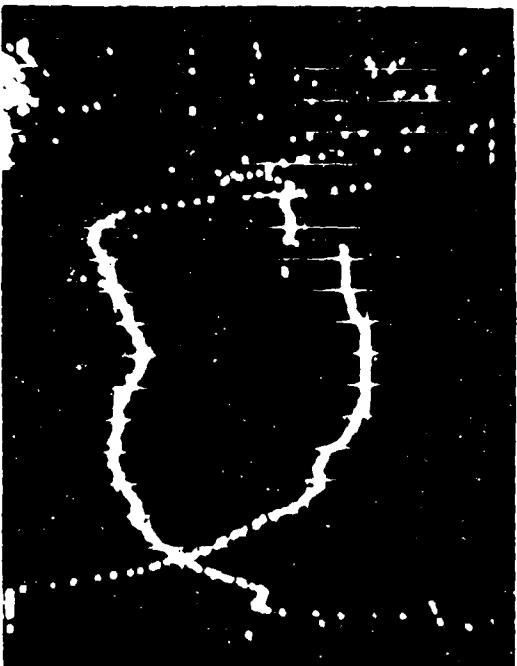
CALL #233



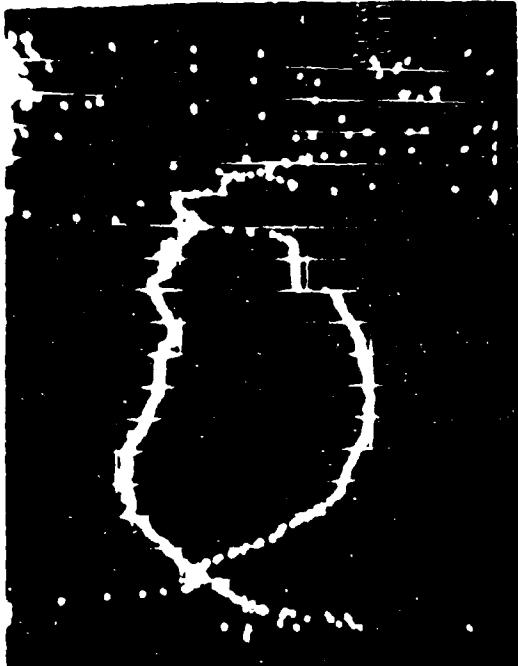
CALL #236



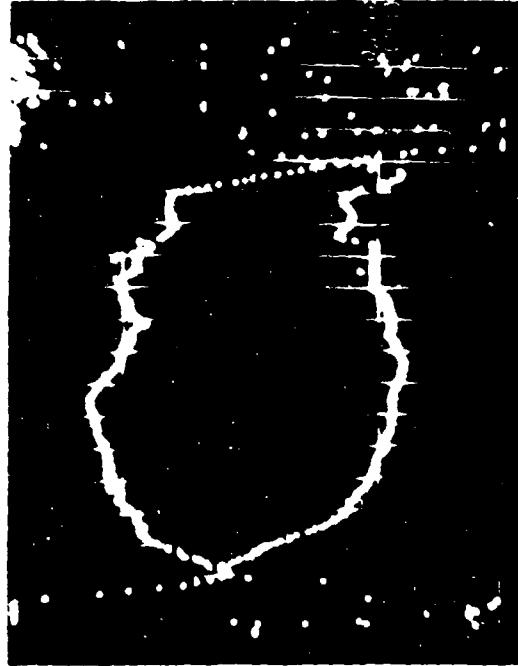
CALL #238



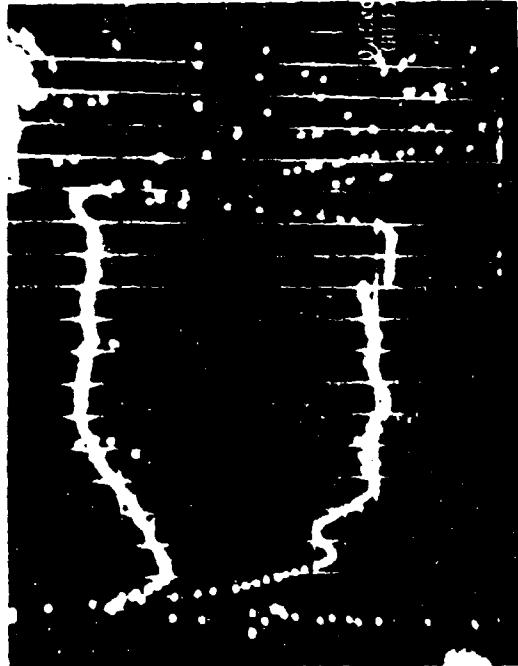
CALL #235



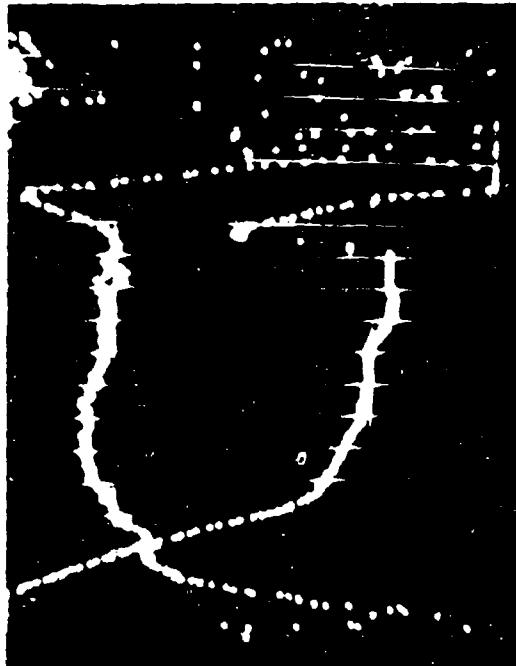
CALL #237



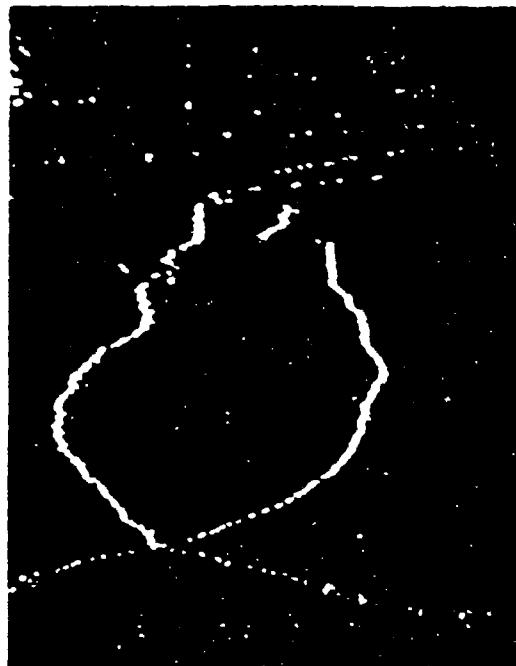
CALL #240



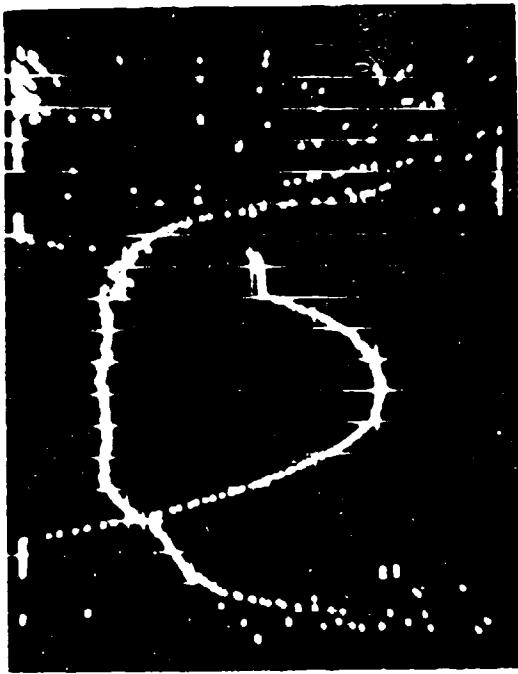
CALL #242



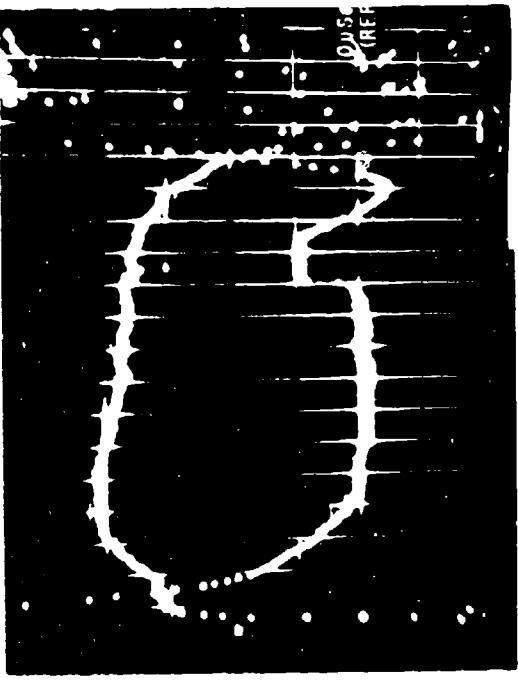
CALL #239



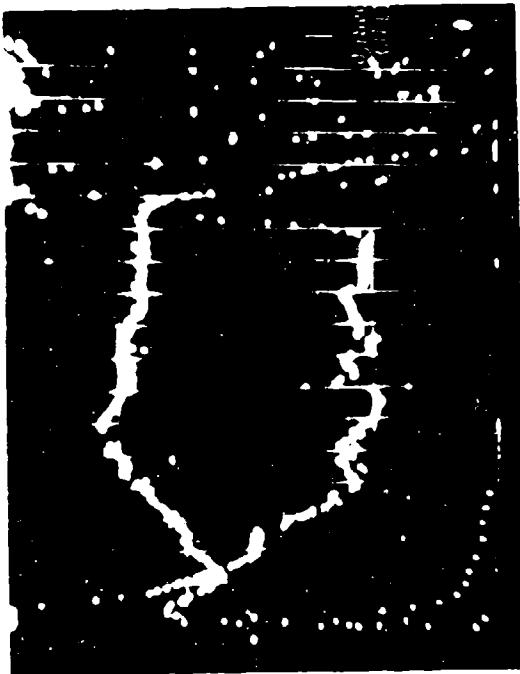
CALL #241



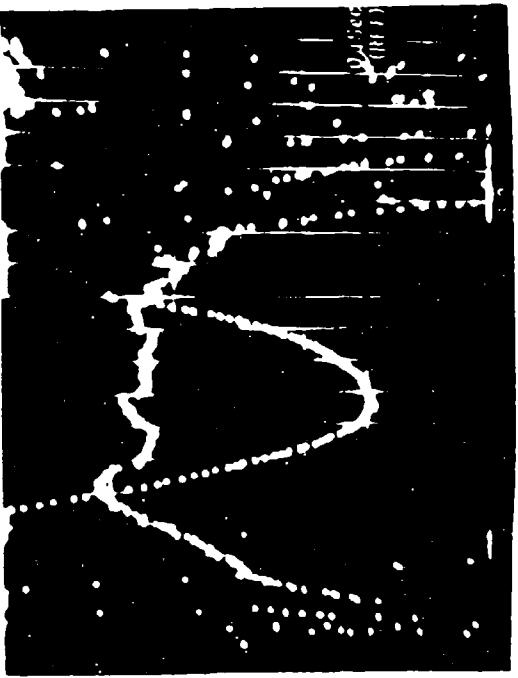
CALL #244



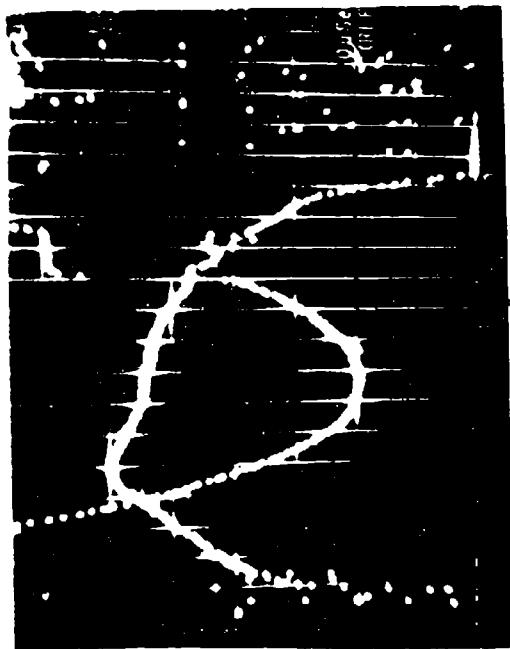
CALL #246



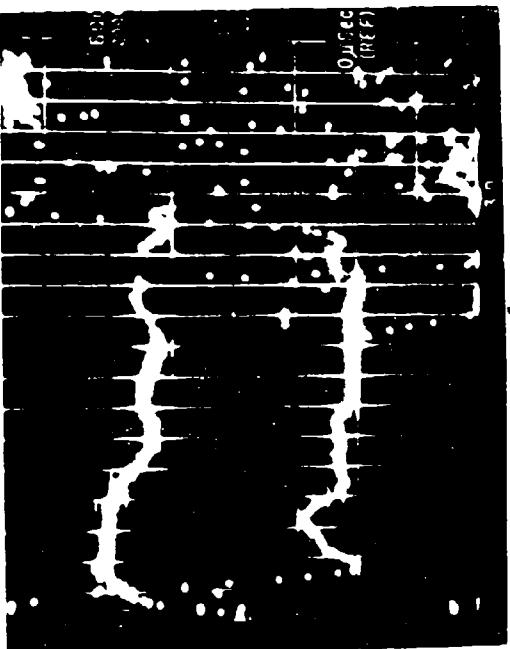
CALL #243



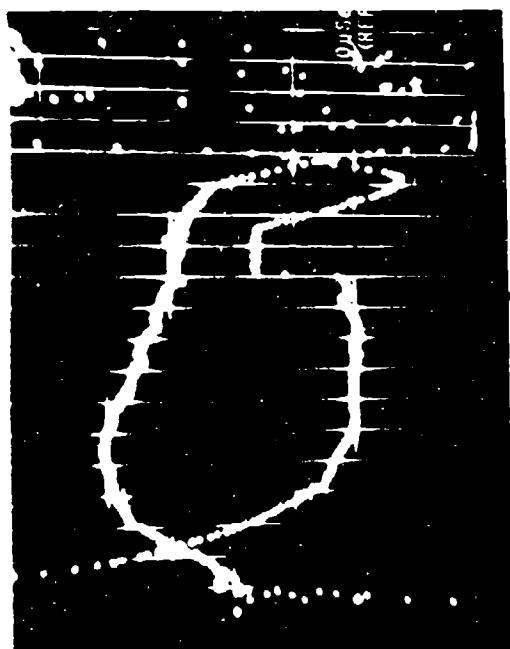
CALL #245



CALL #248



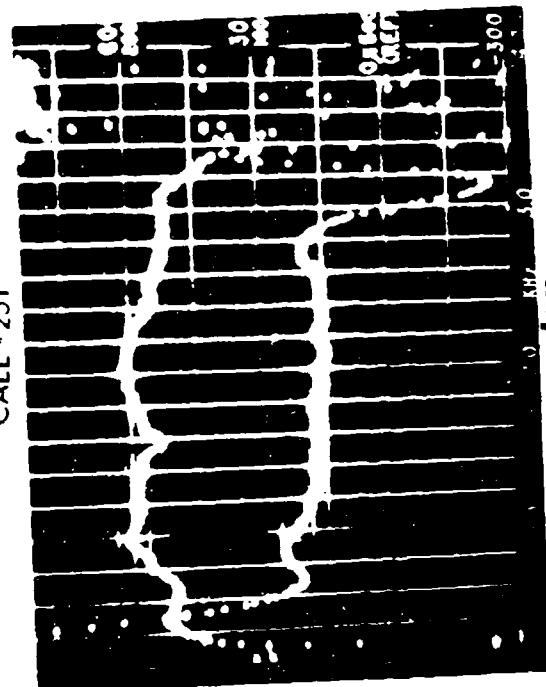
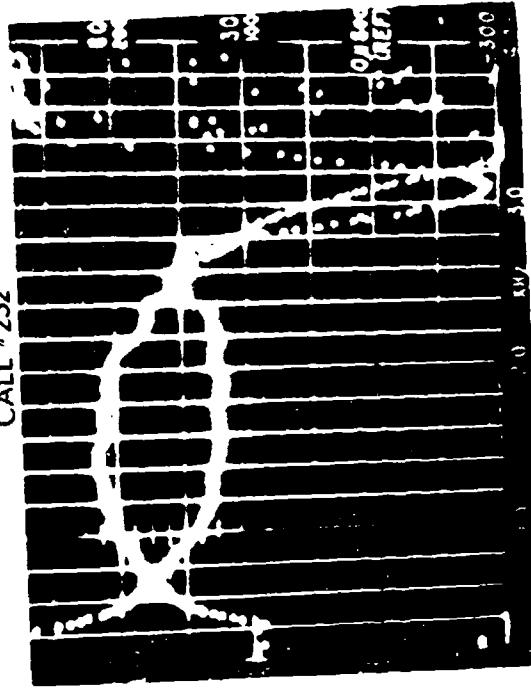
CALL #250

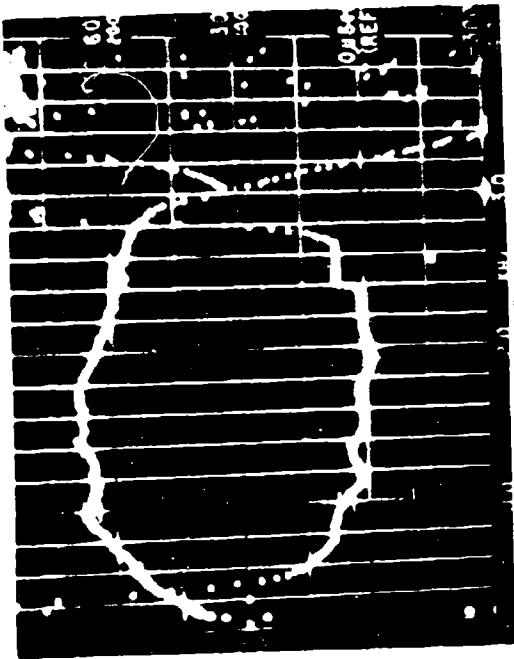


CALL #247

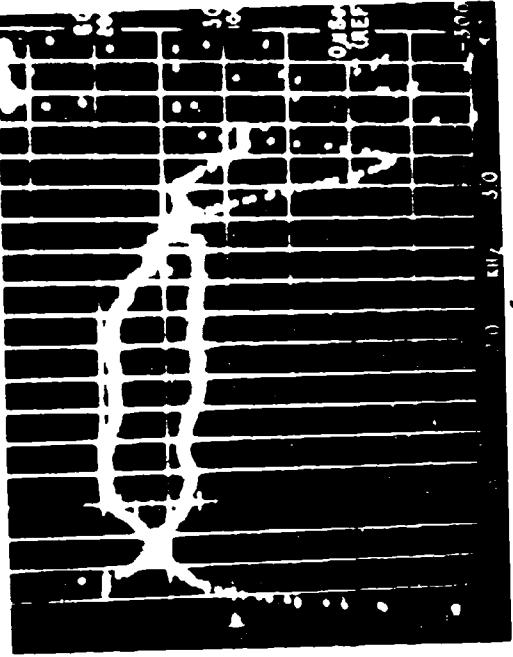


CALL #249

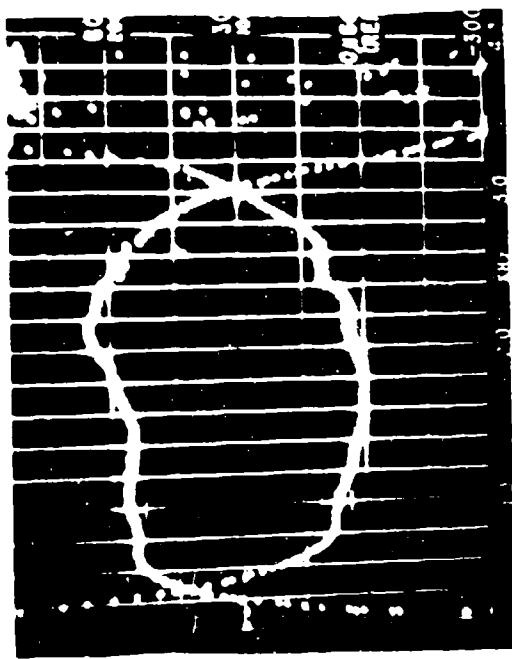




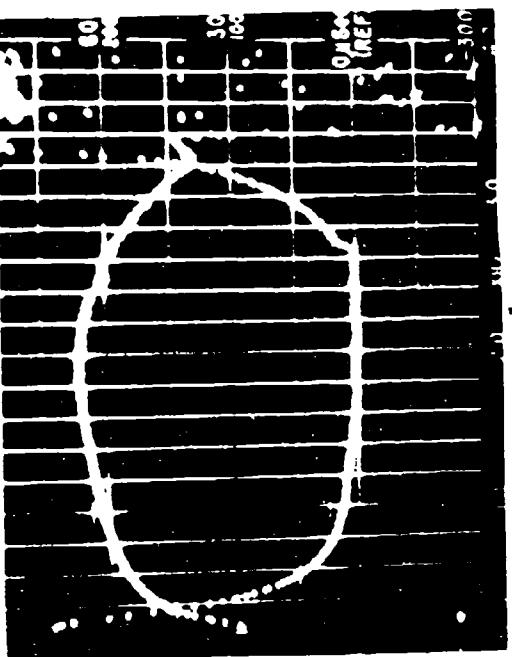
CALL #256



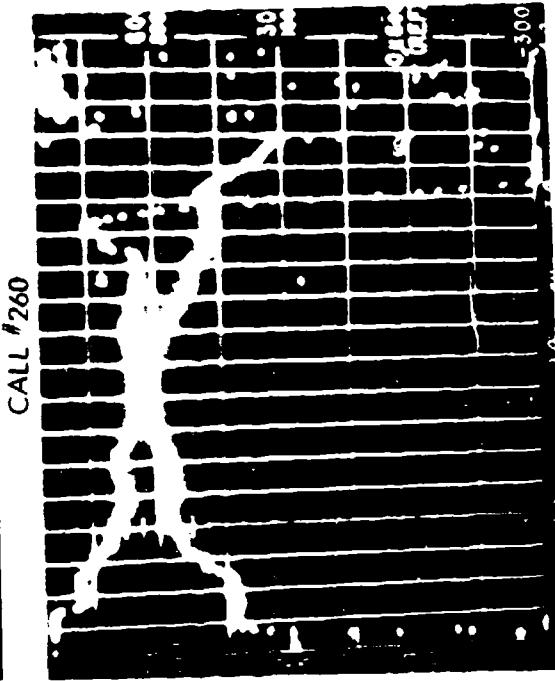
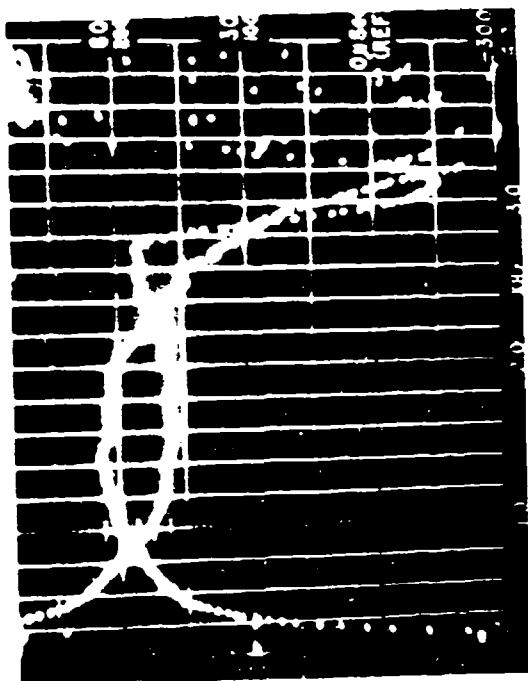
CALL #258



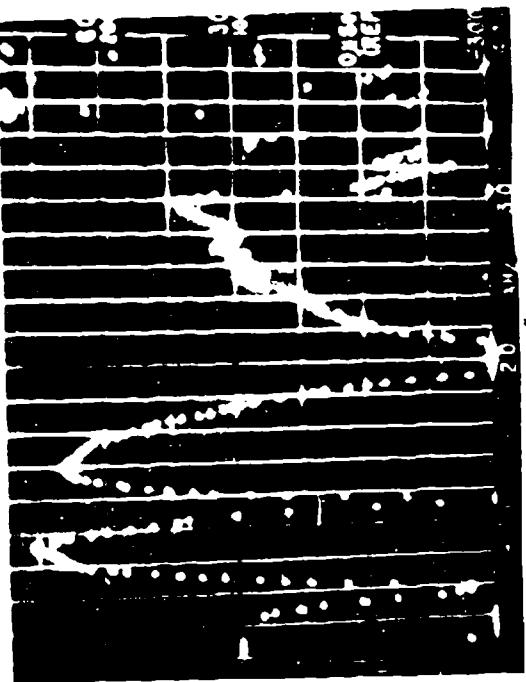
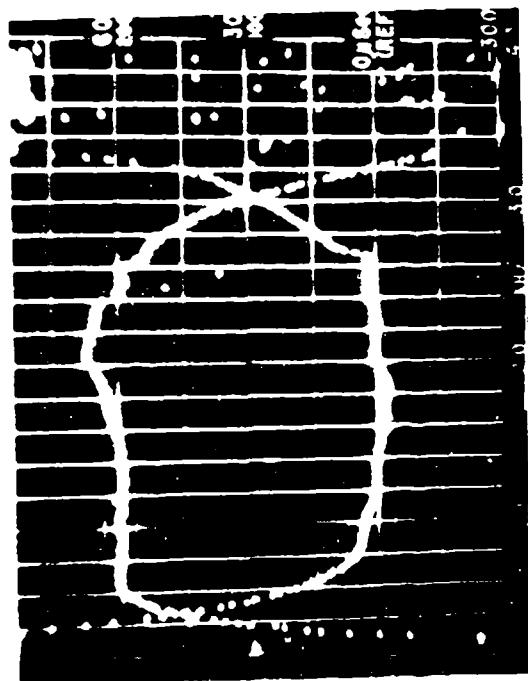
CALL #255

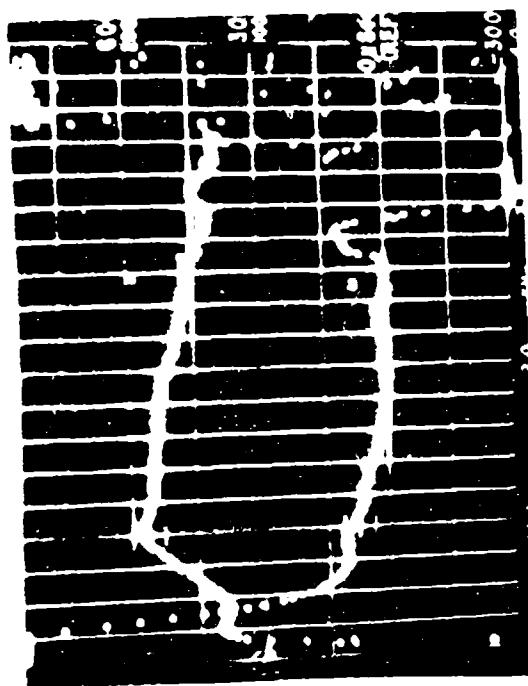


CALL #257

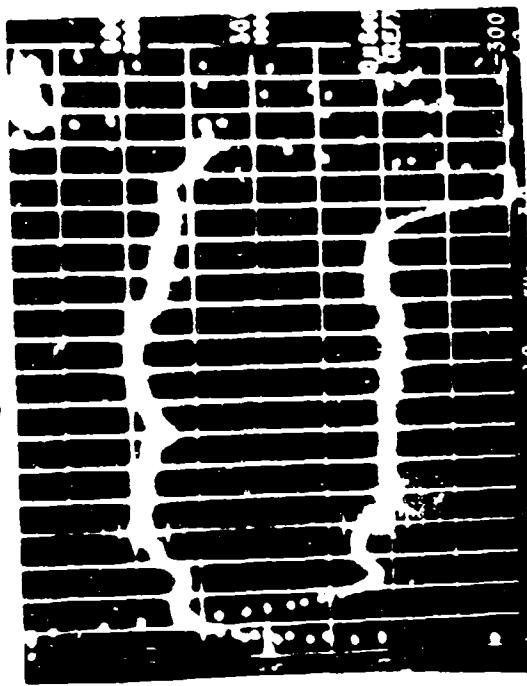


CALL #261

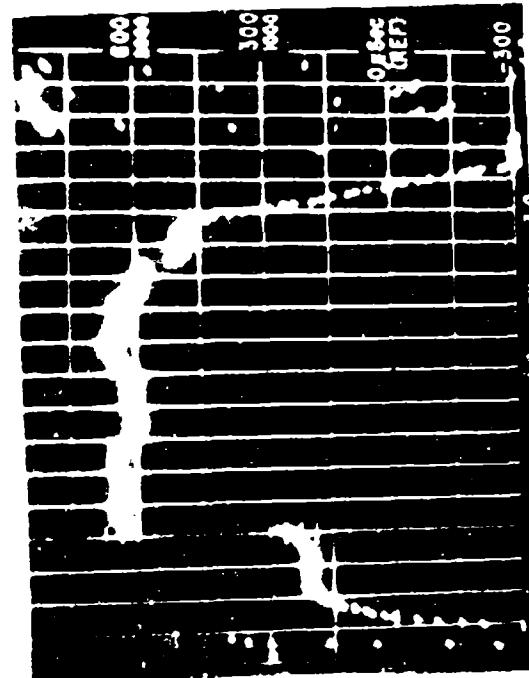




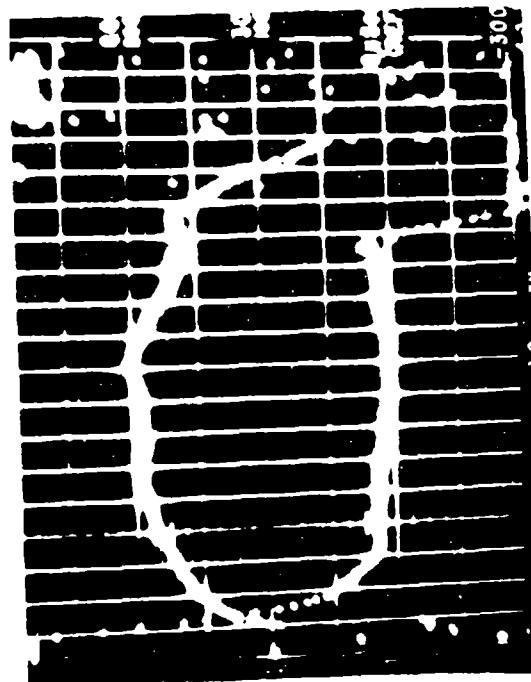
CALL #264



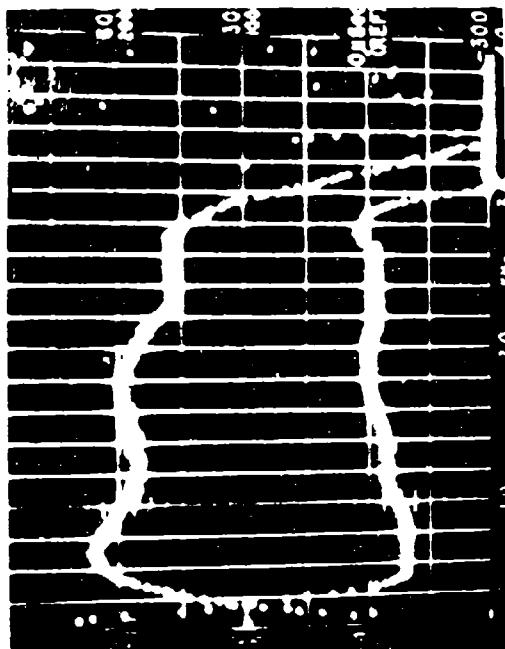
CALL #266



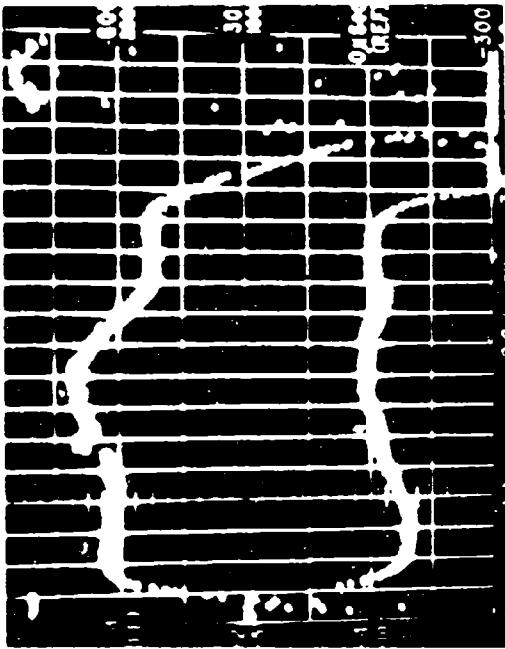
CALL #263



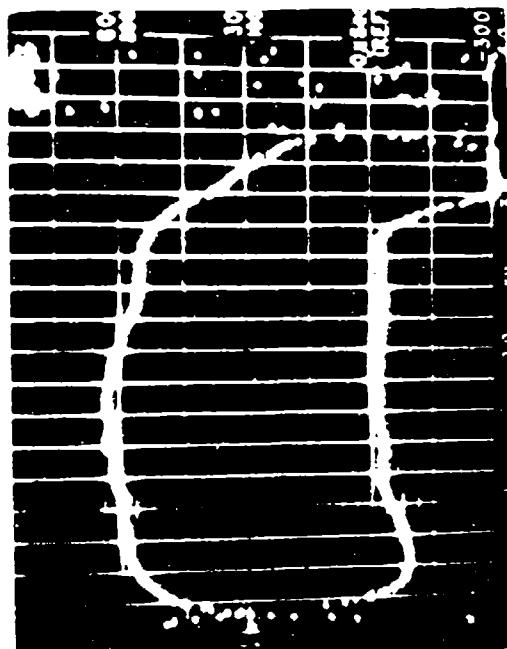
CALL #265



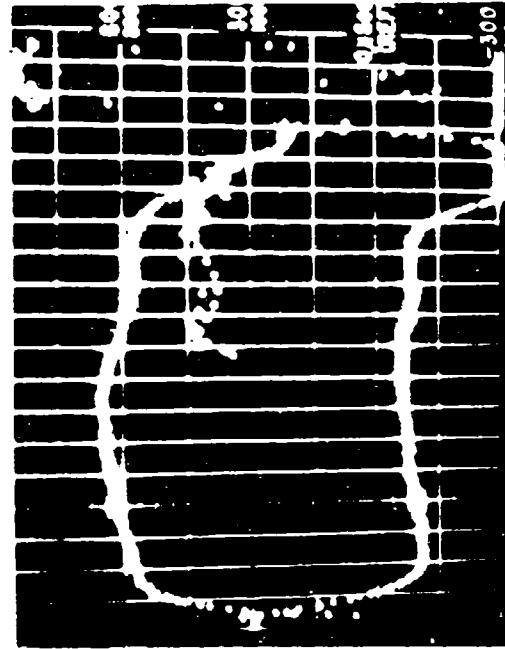
CALL #268



CALL #270



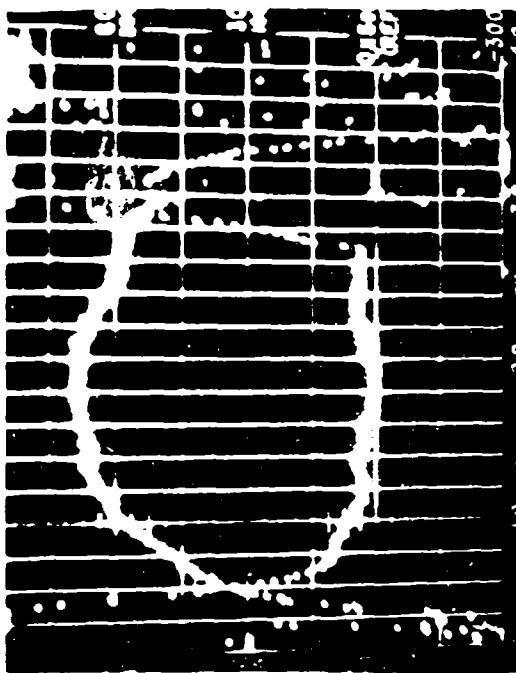
CALL #267



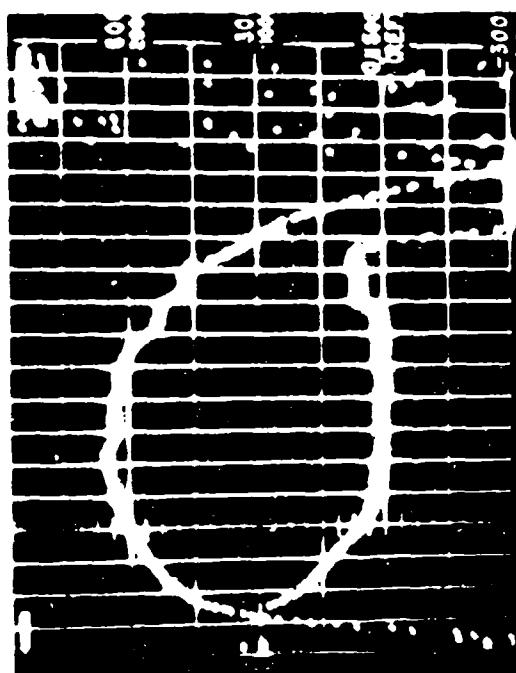
CALL #269



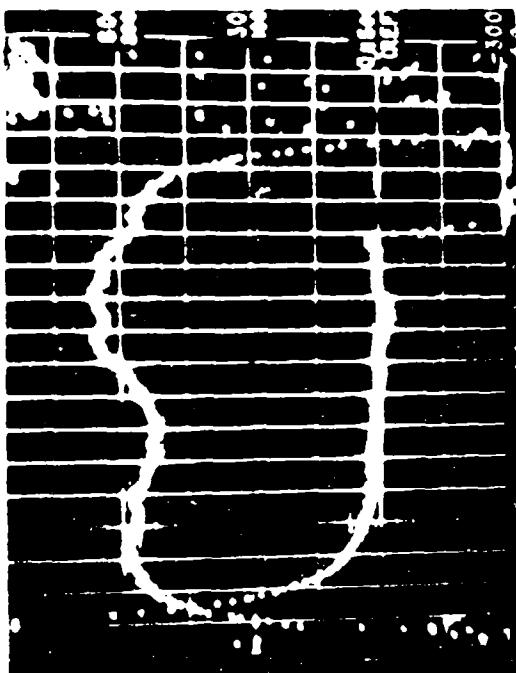
CALL #273



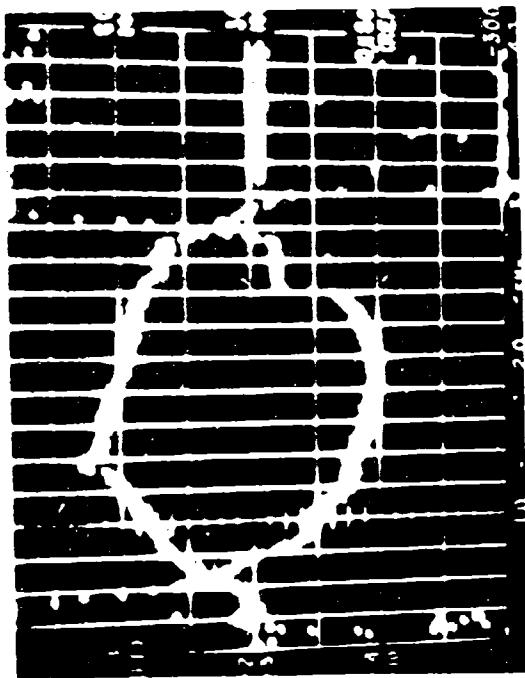
CALL #276



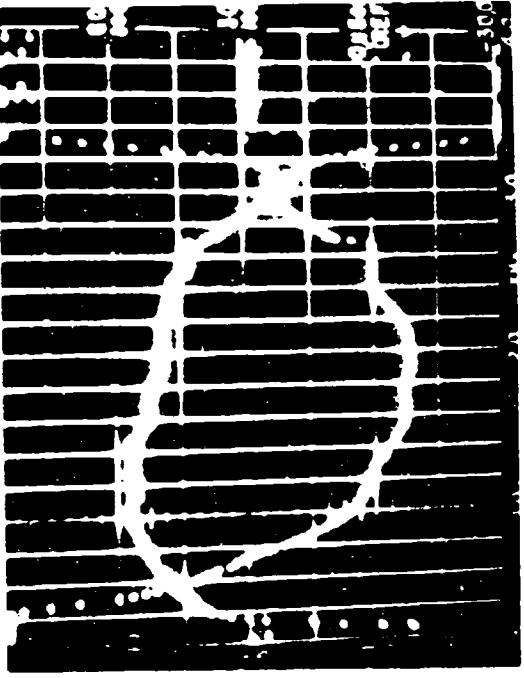
CALL #272



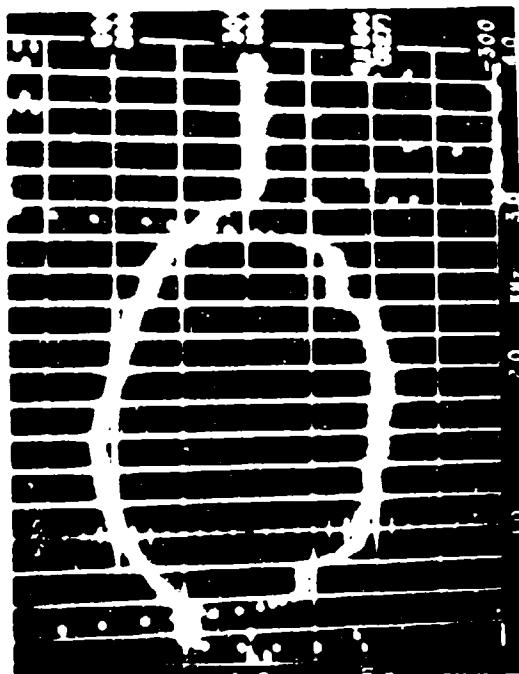
CALL #274



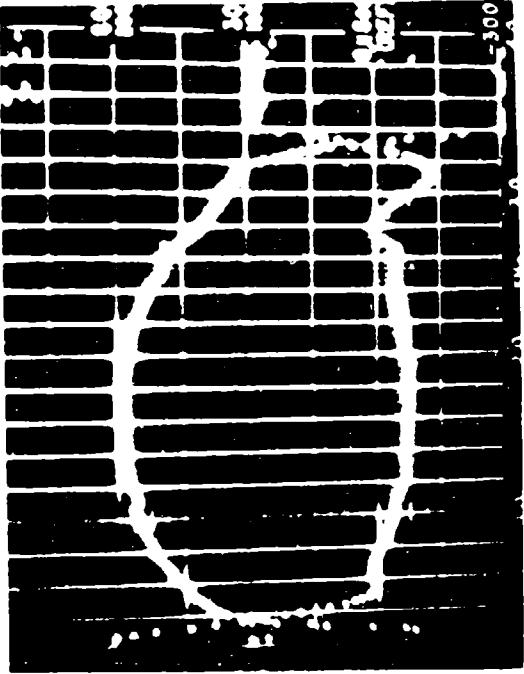
CALL #279



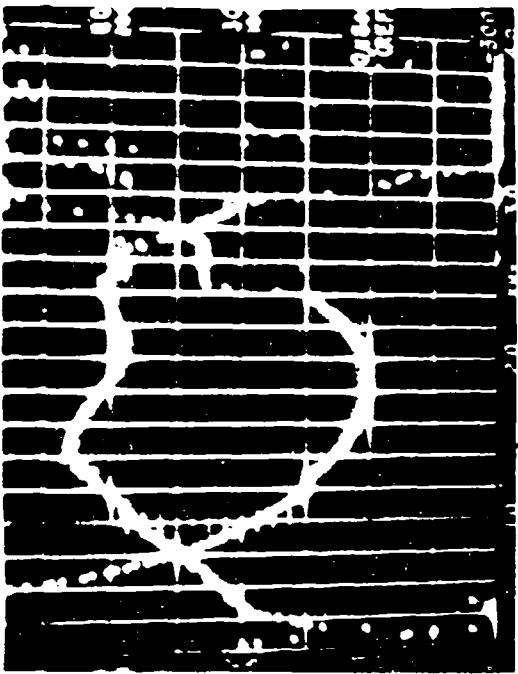
CALL #282



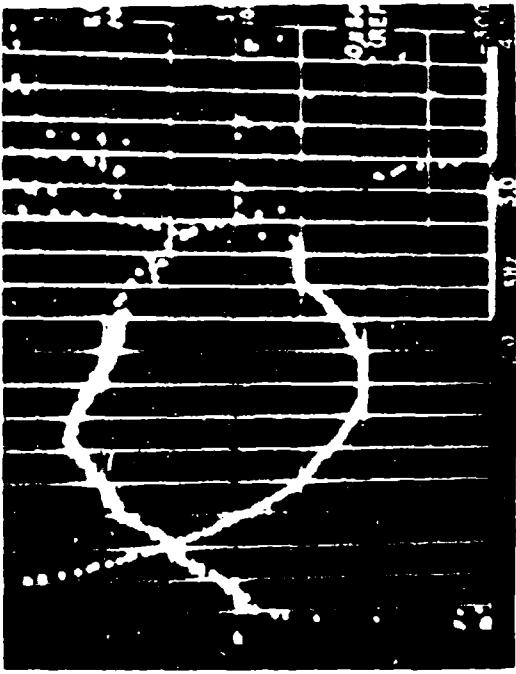
CALL #278



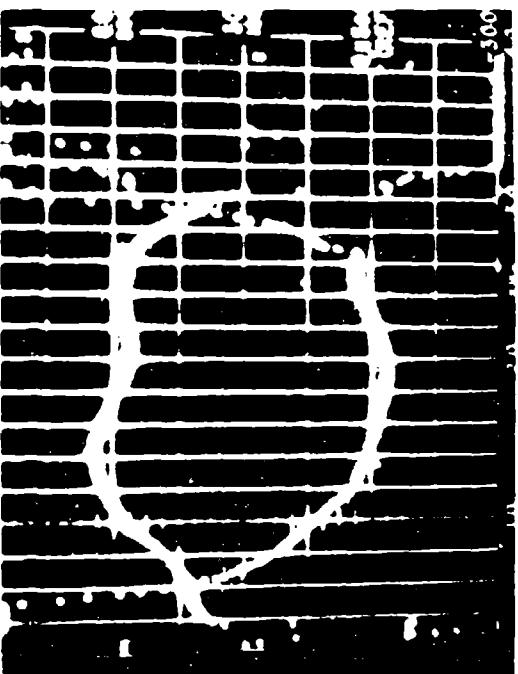
CALL #280



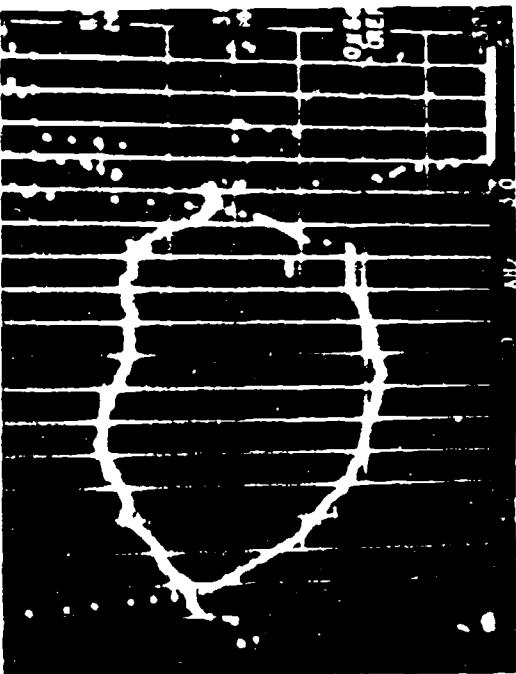
CALL #286



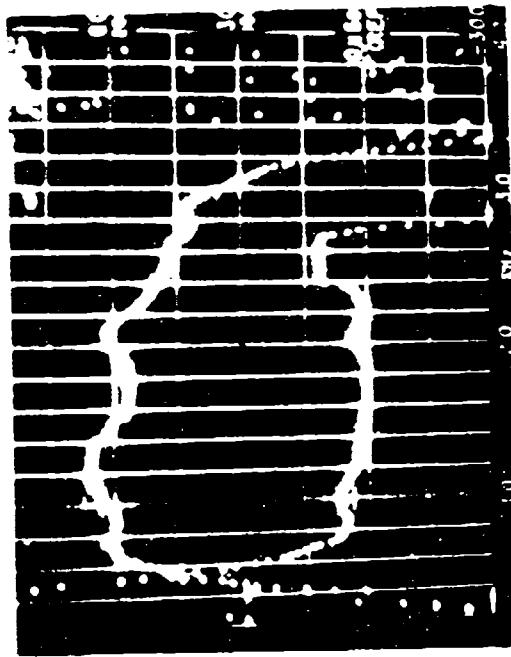
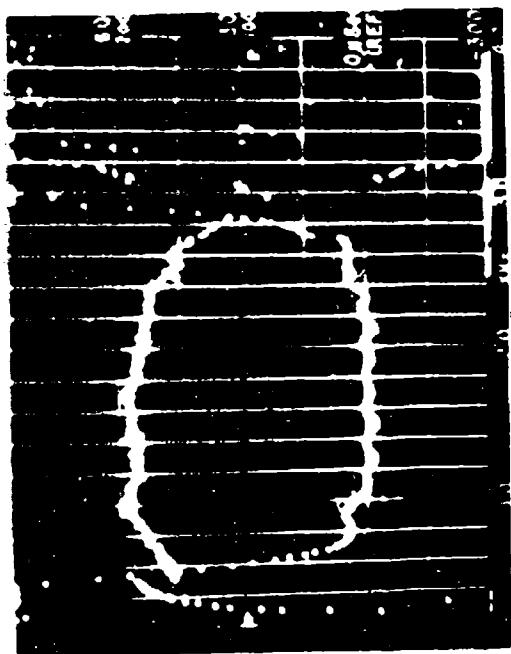
CALL #288



CALL #285



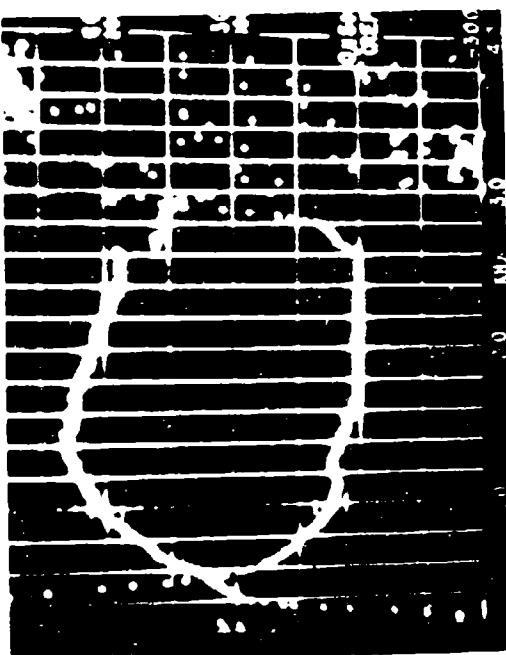
CALL #287



CALL #292



CALL #289



CALL #291



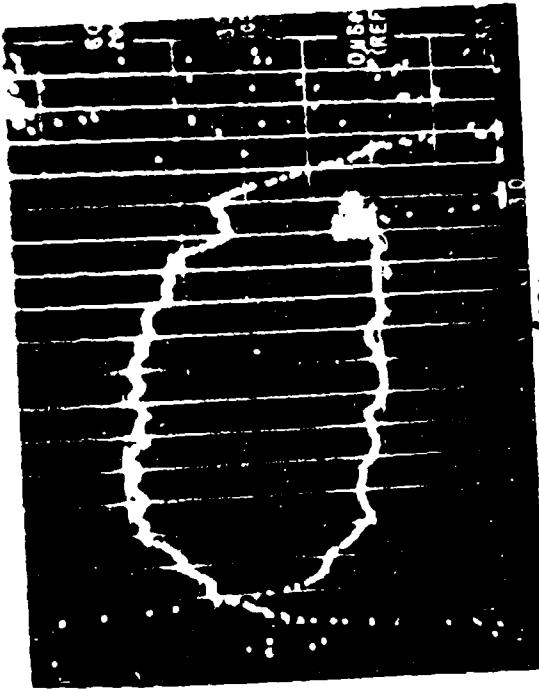
CALL #295



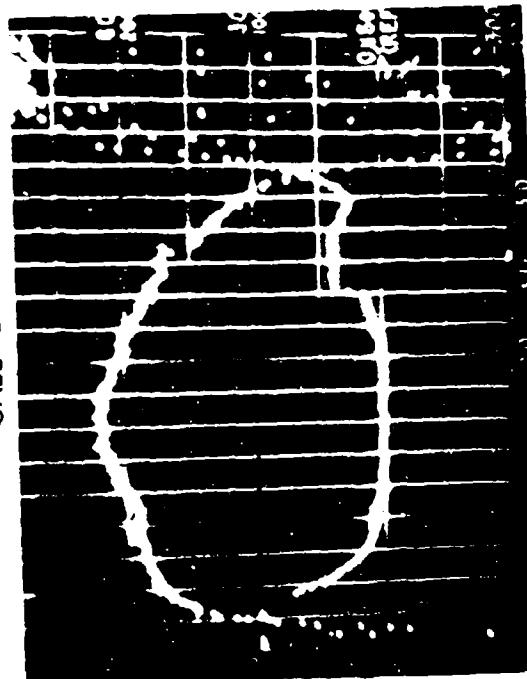
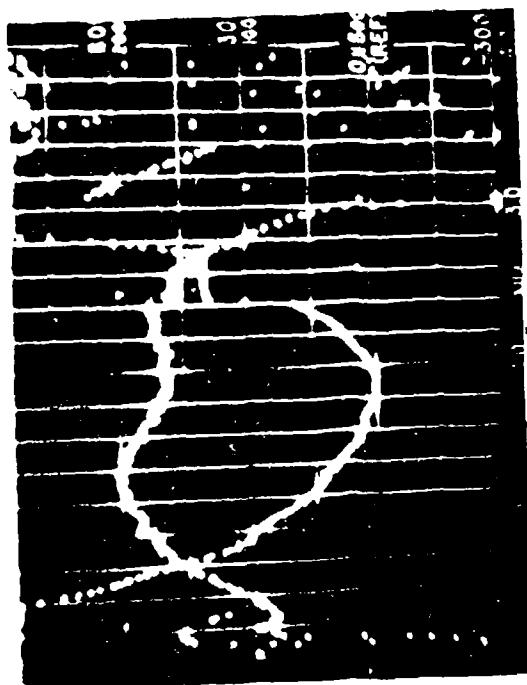
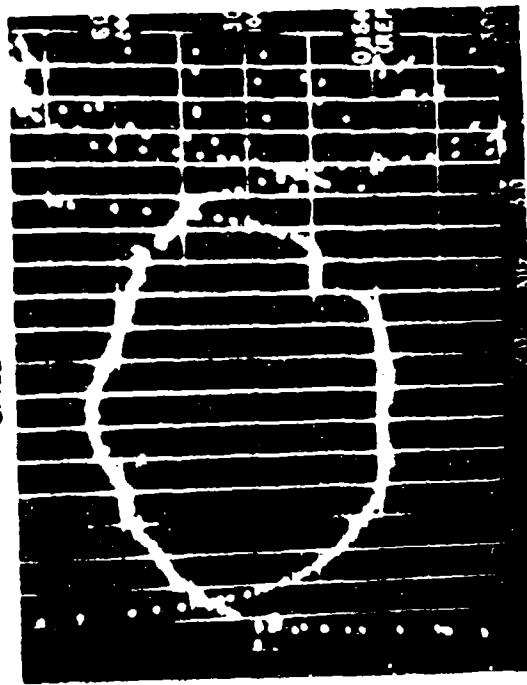
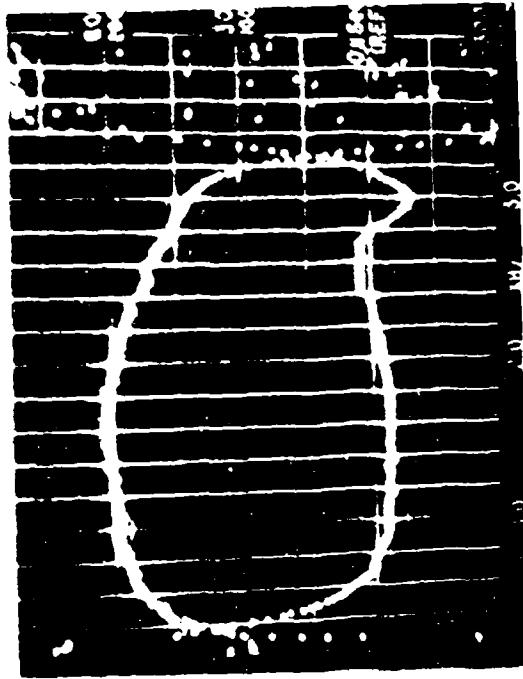
CALL #298

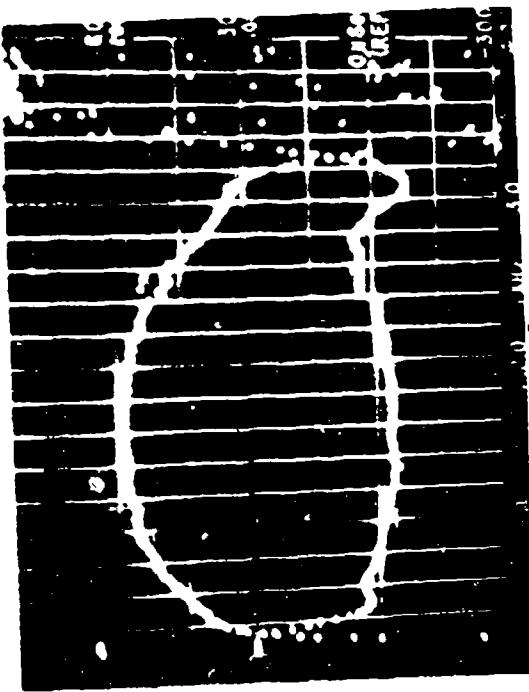


CALL #294

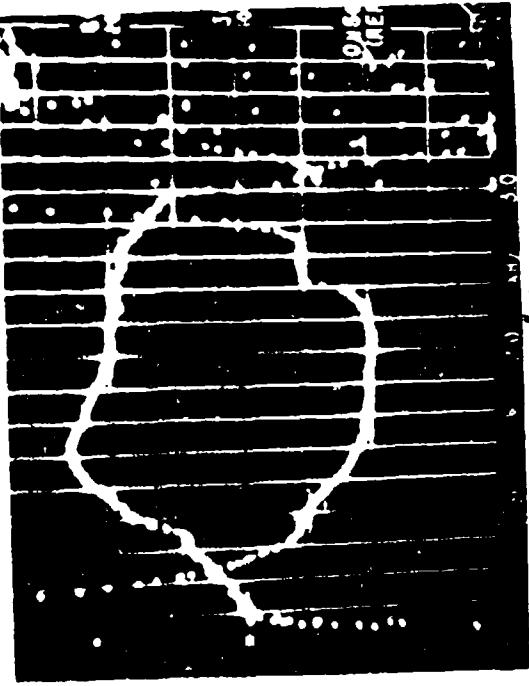


CALL #296

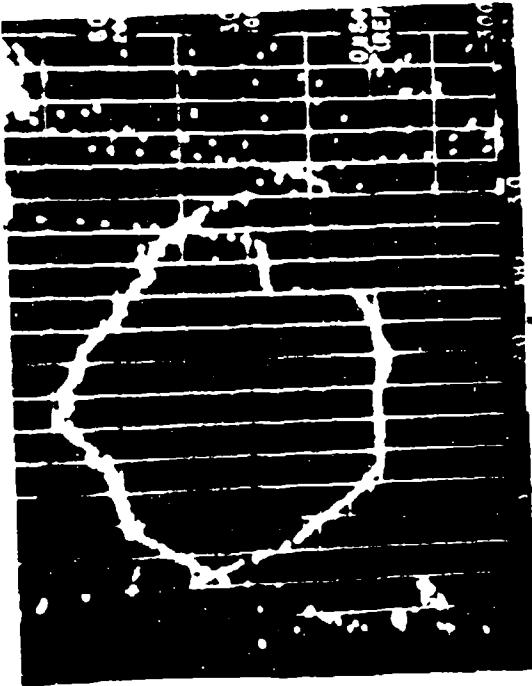




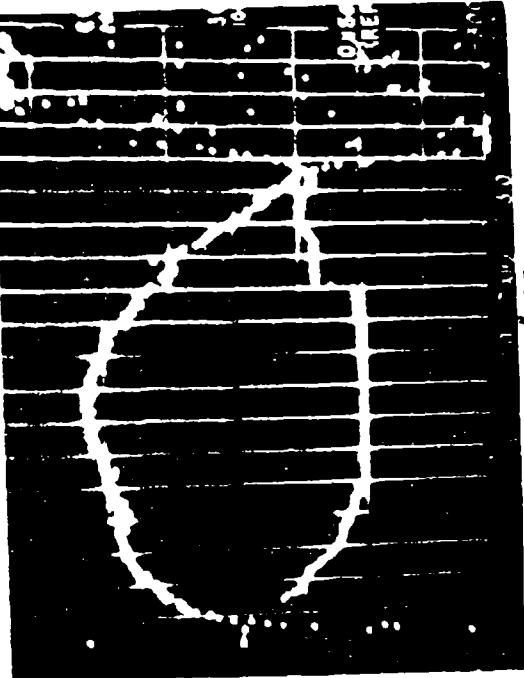
CALL #304



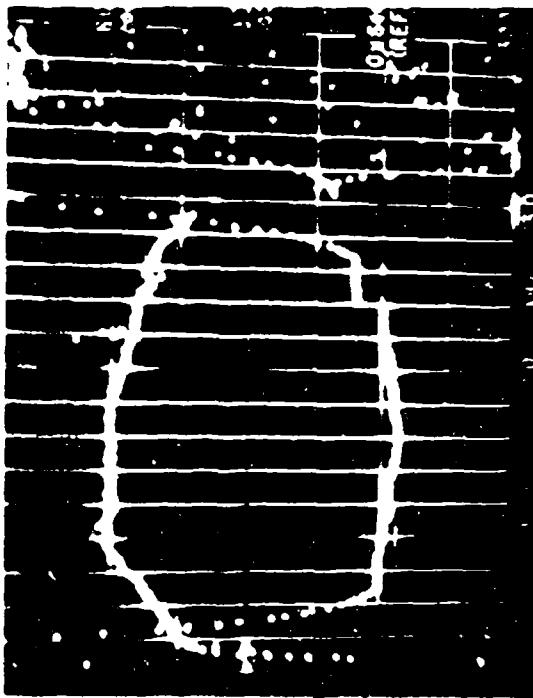
CALL #306



CALL #303



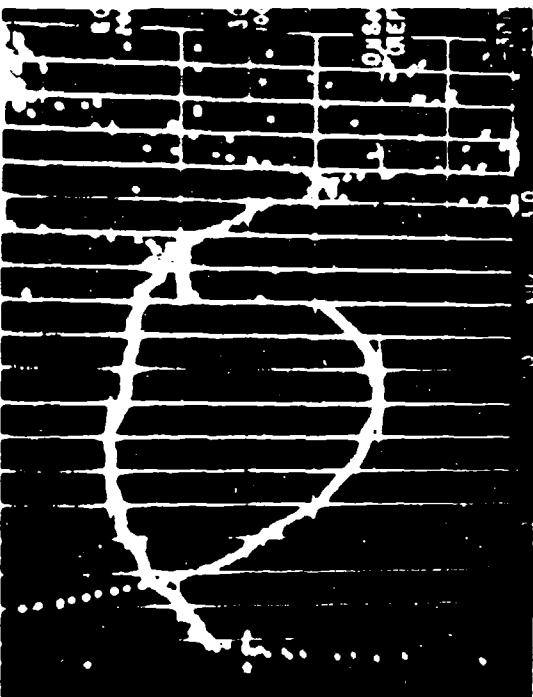
CALL #305



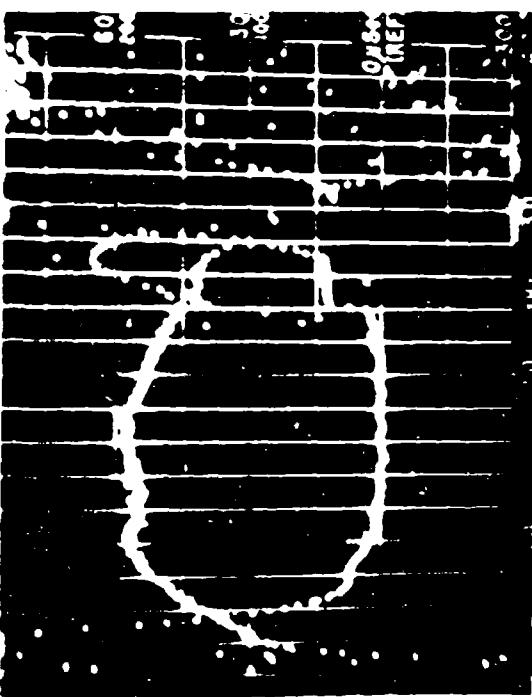
CALL #309



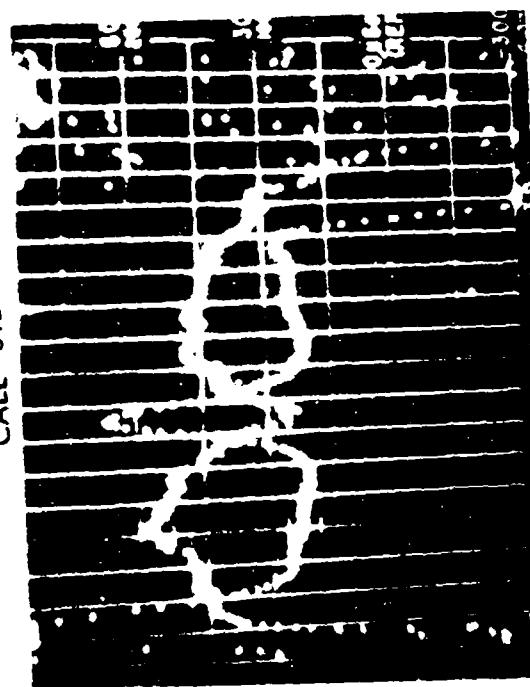
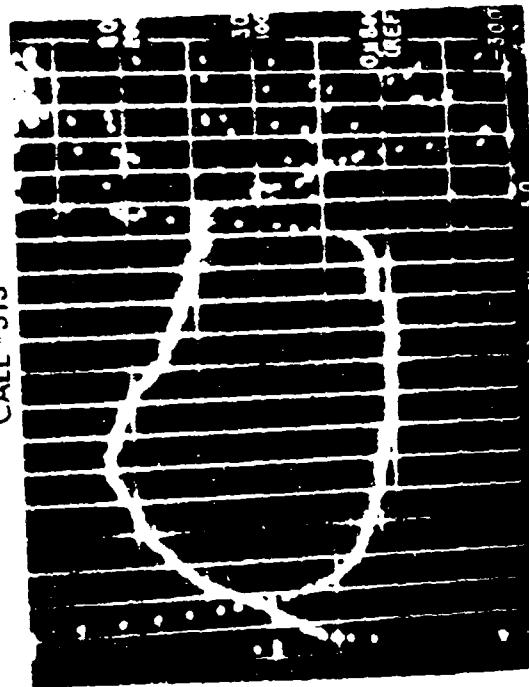
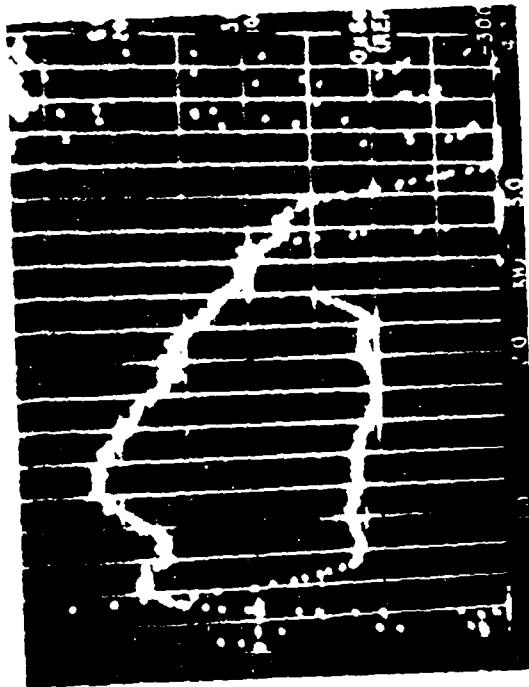
CALL #311

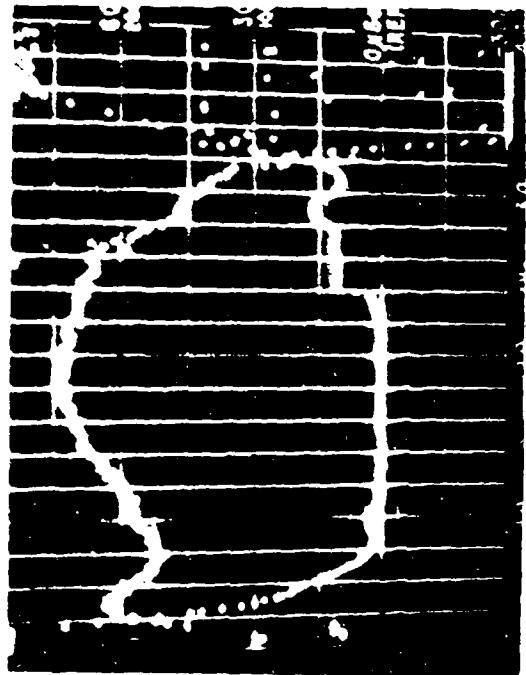


CALL #307

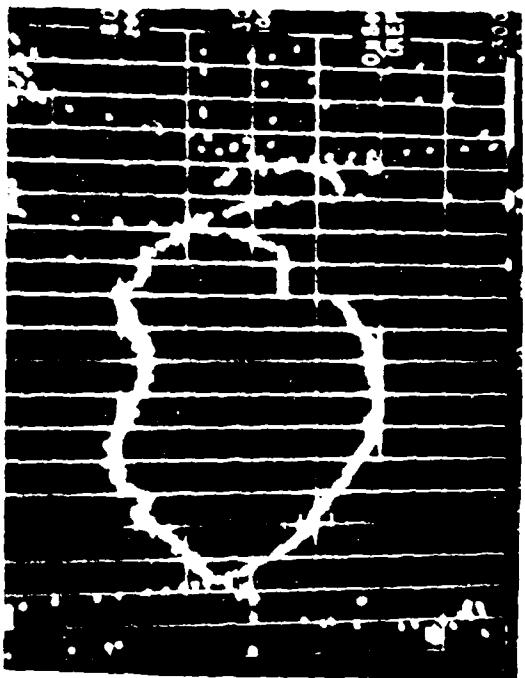


CALL #310

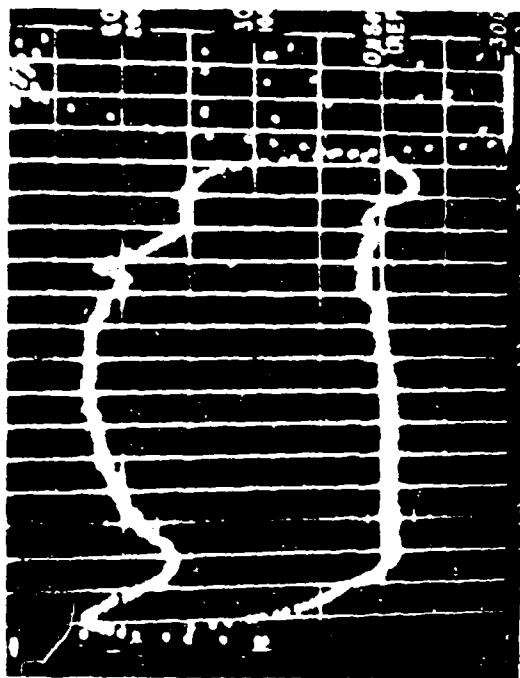




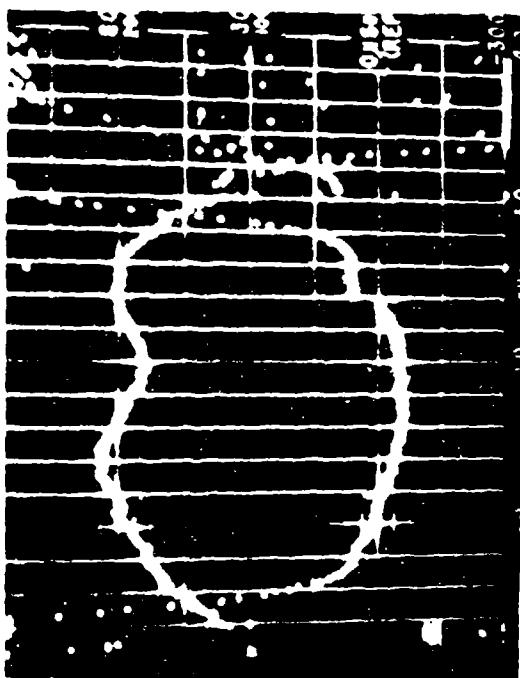
CALL #318



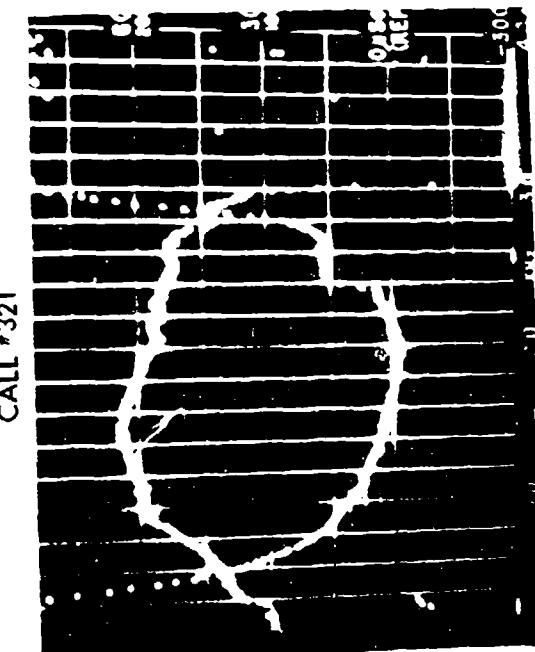
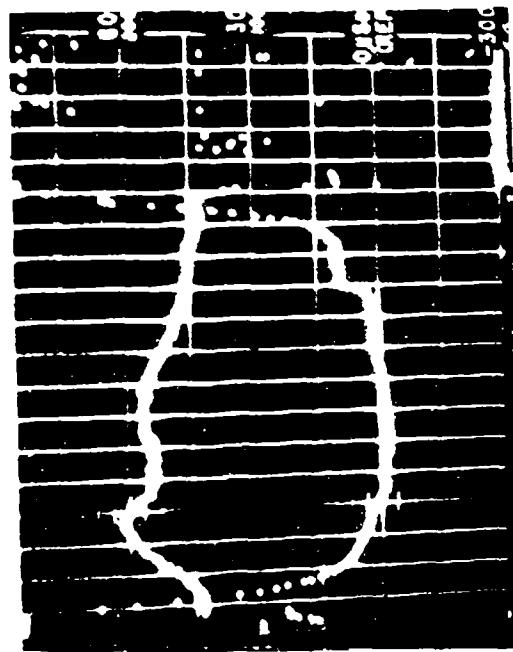
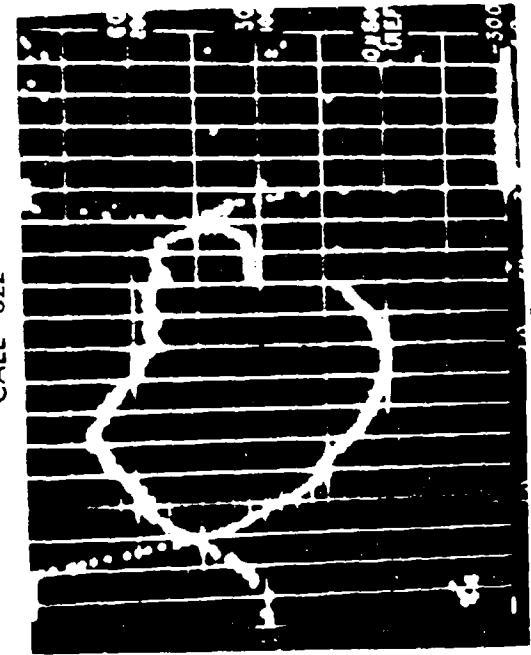
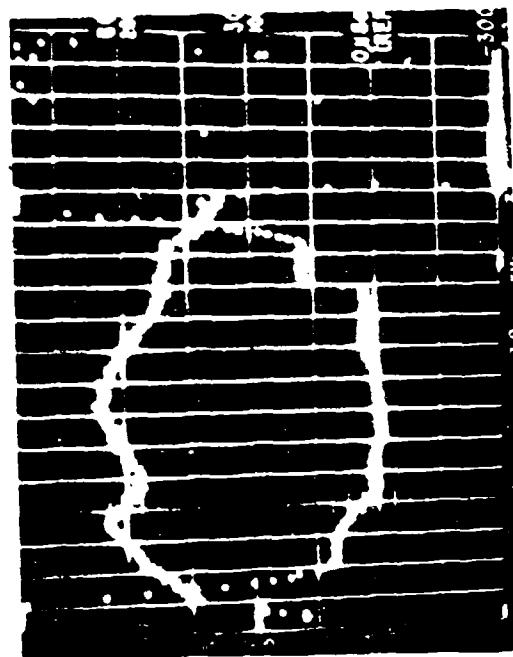
CALL #320

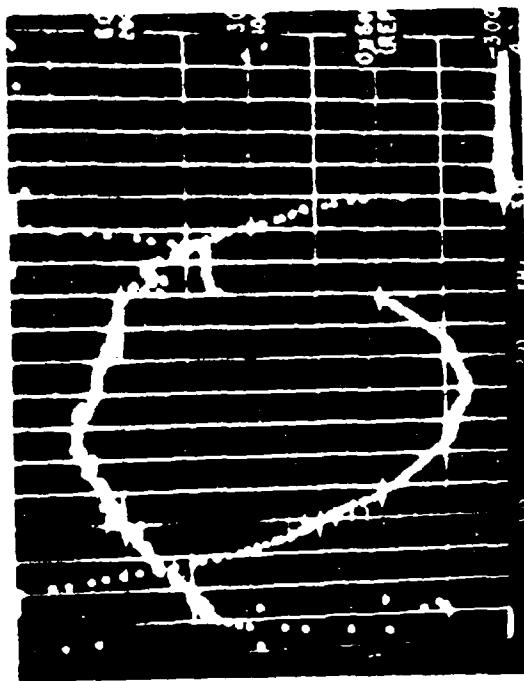


CALL #317

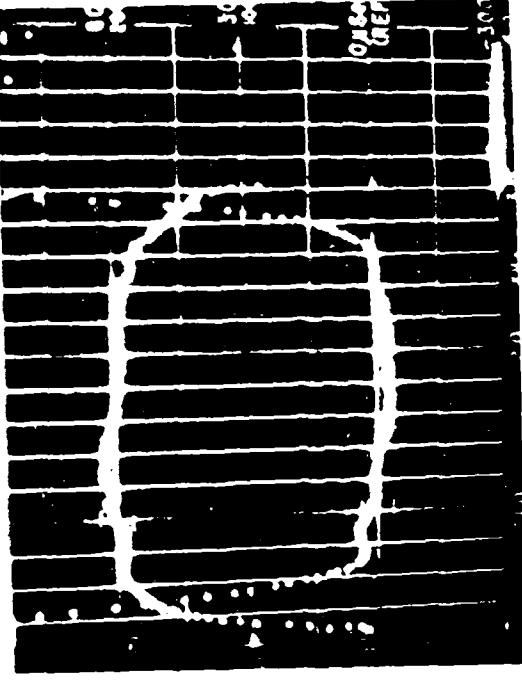


CALL #319

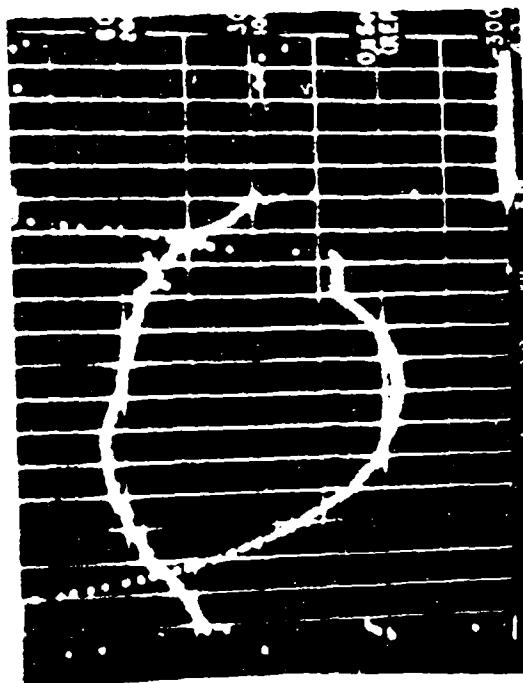




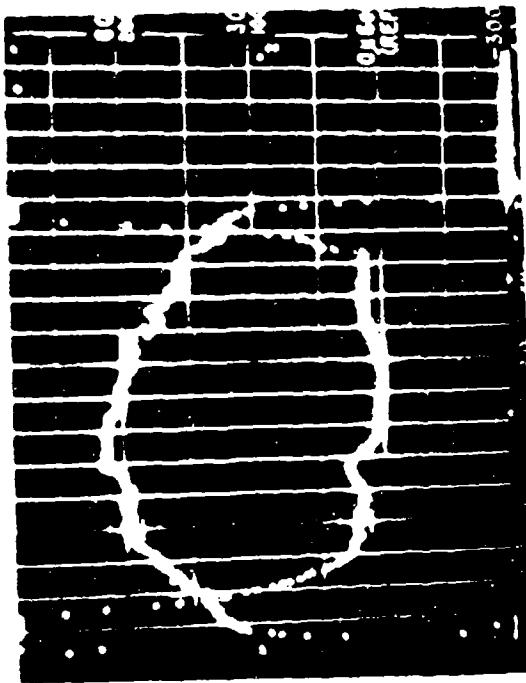
CALL #327



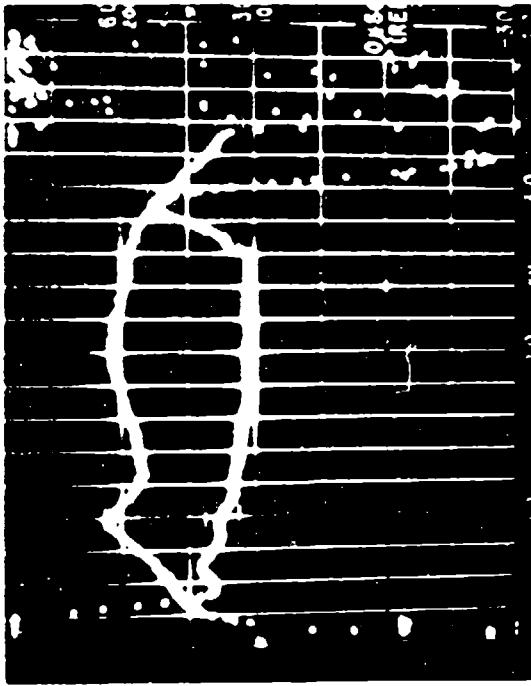
CALL #329



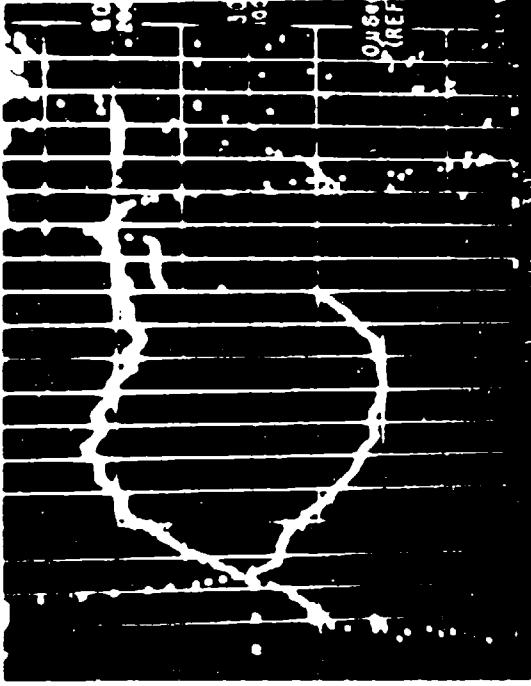
CALL #326



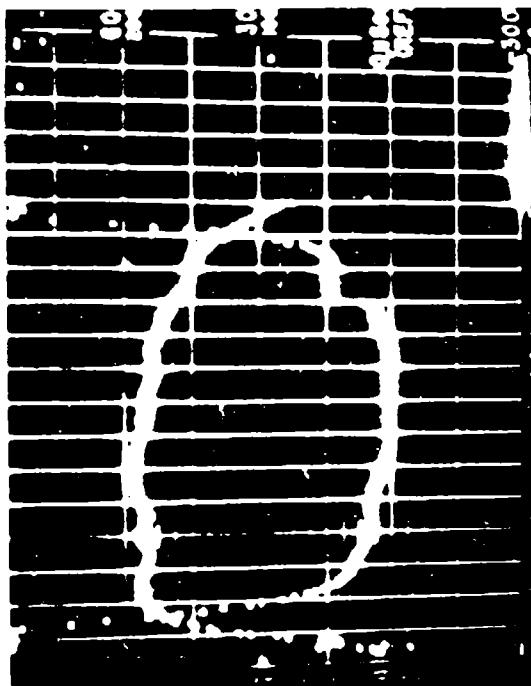
CALL #328



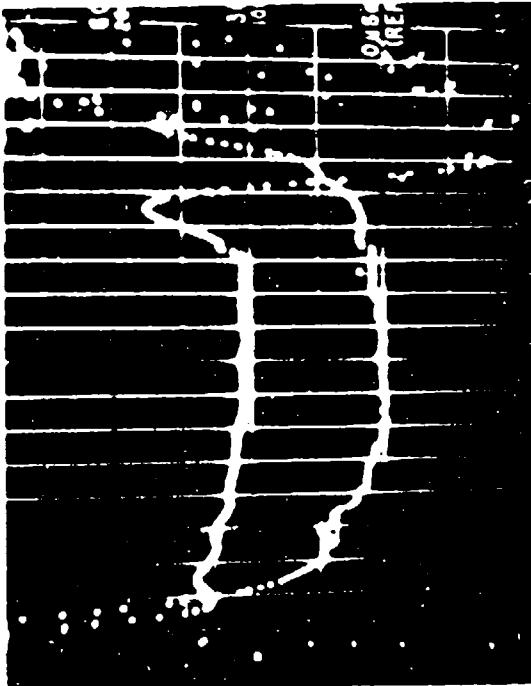
CALL #332



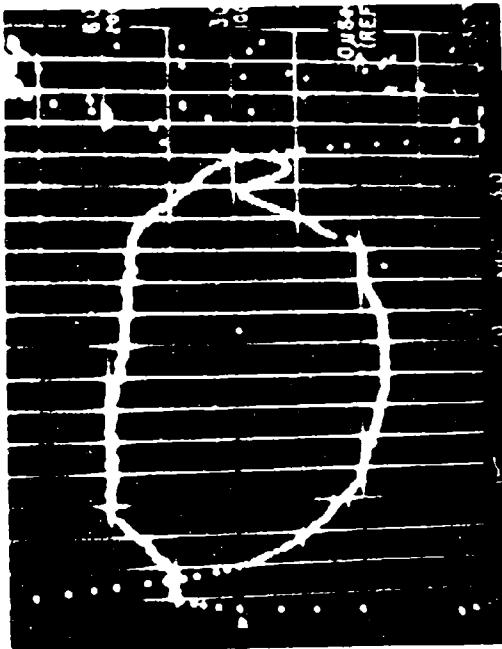
CALL #334



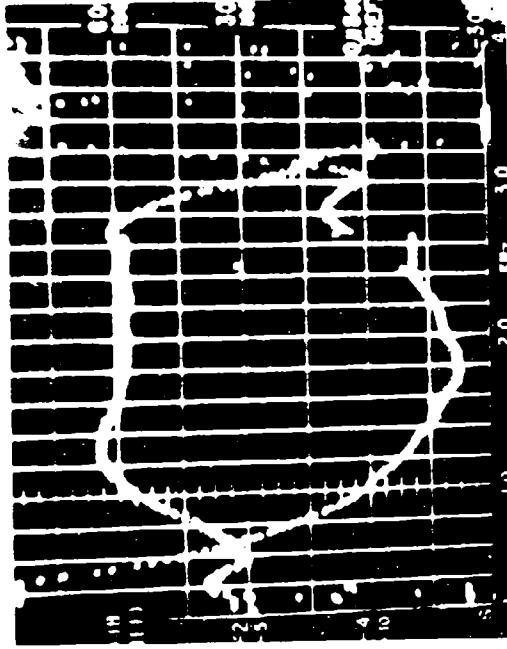
CALL #331



CALL #333



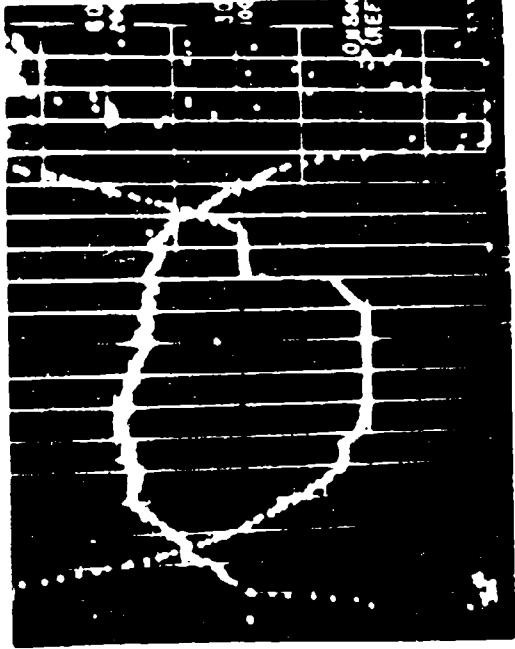
CALL #337



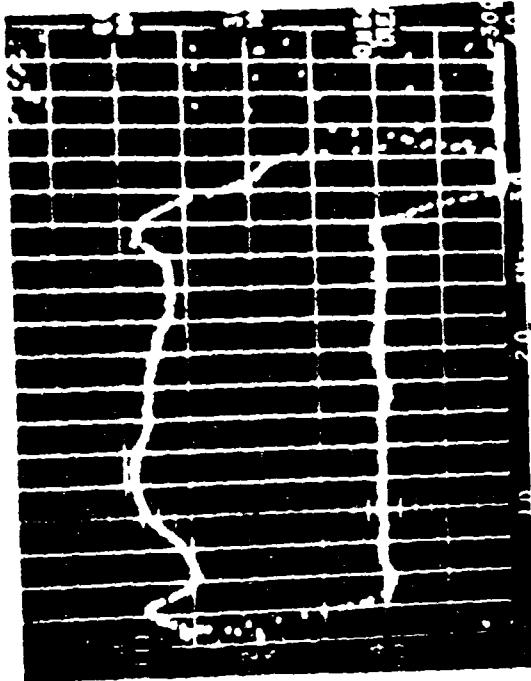
CALL #339



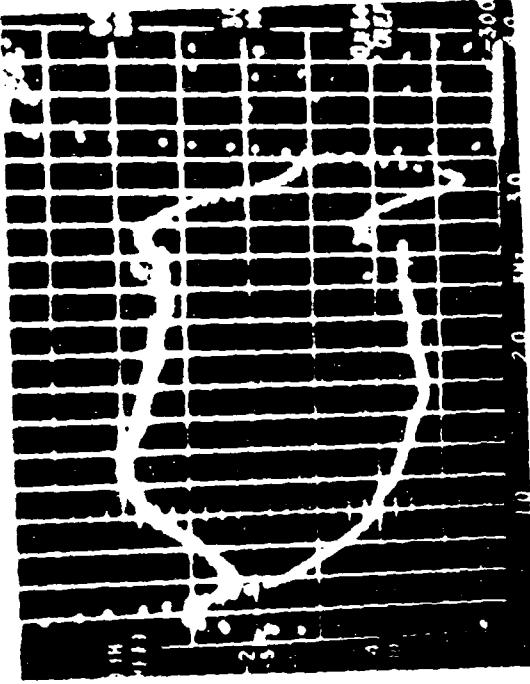
CALL #335



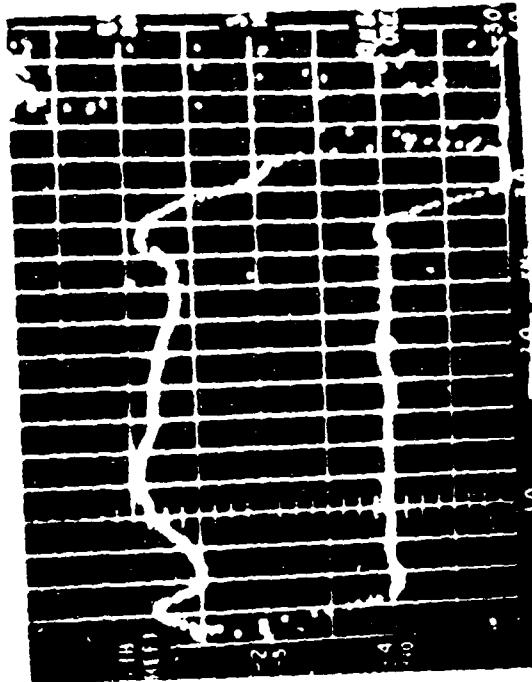
CALL #338



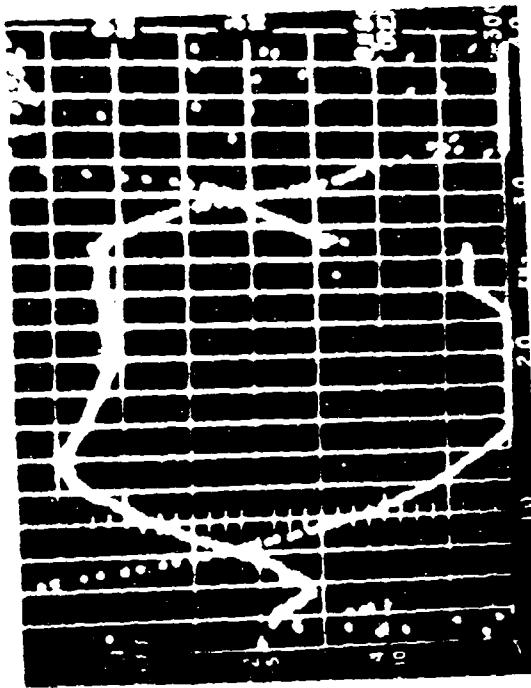
CALL #341



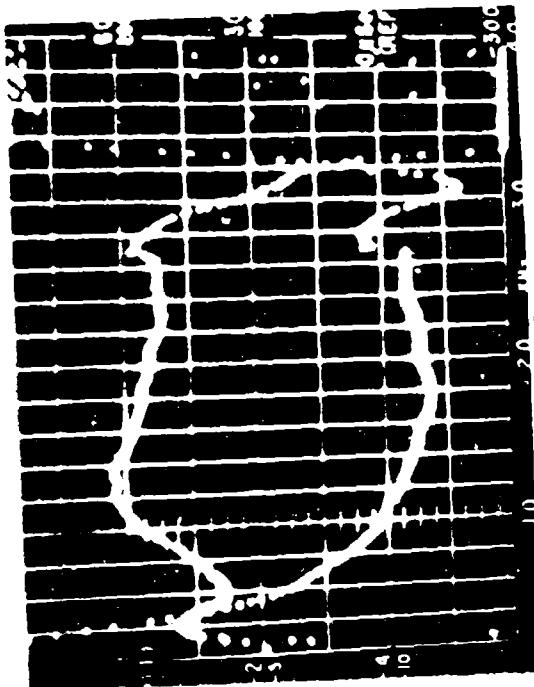
CALL #343



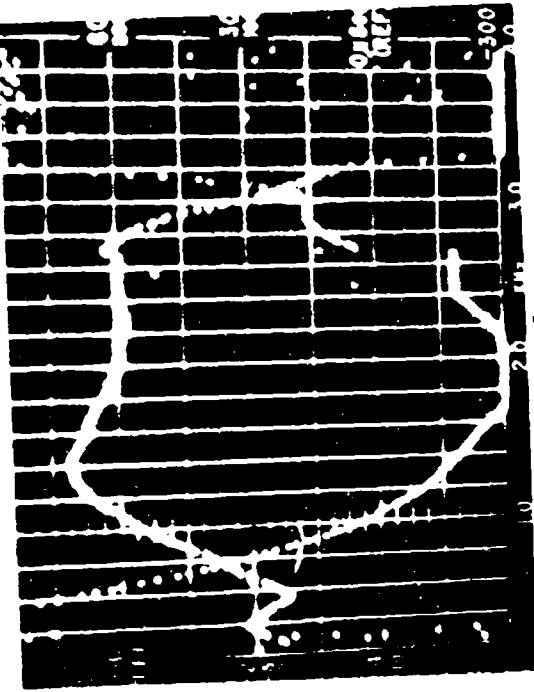
CALL #340



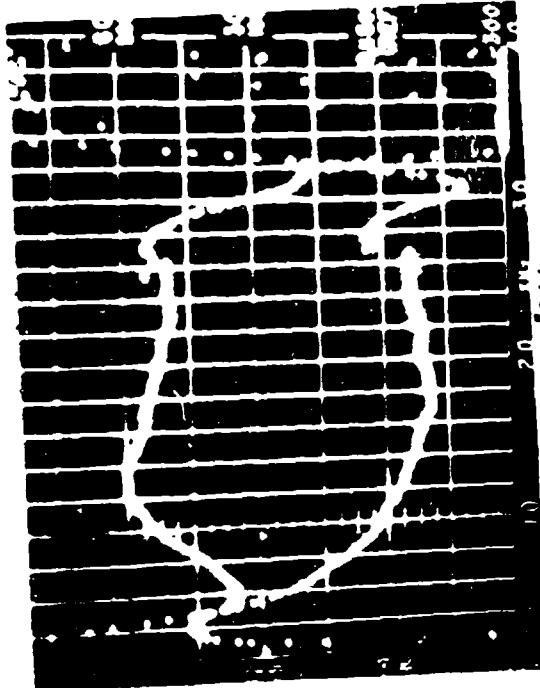
CALL #342



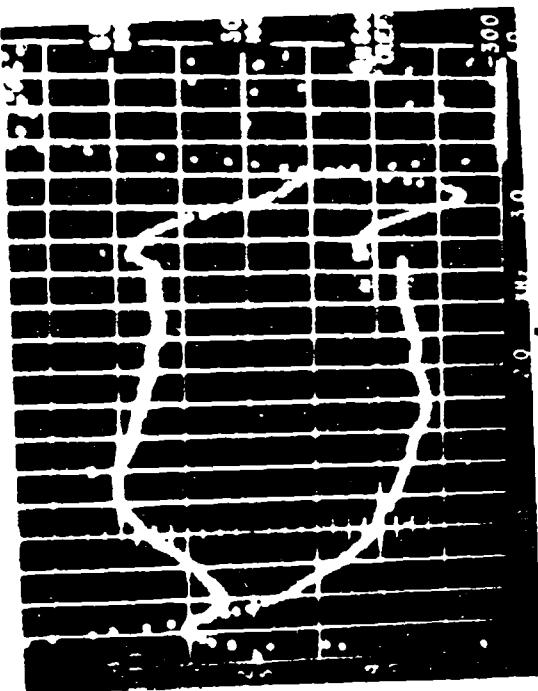
CALL #345



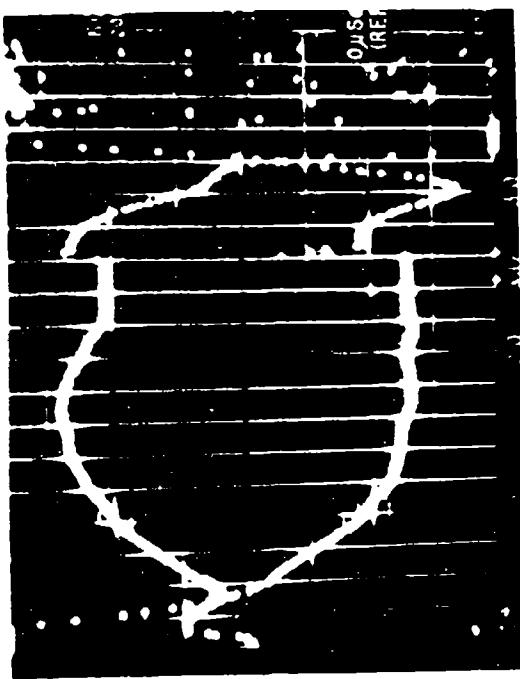
CALL #347



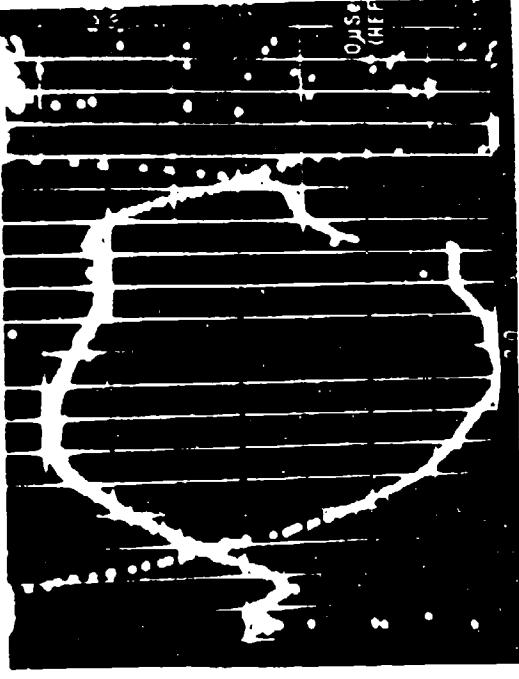
CALL #344



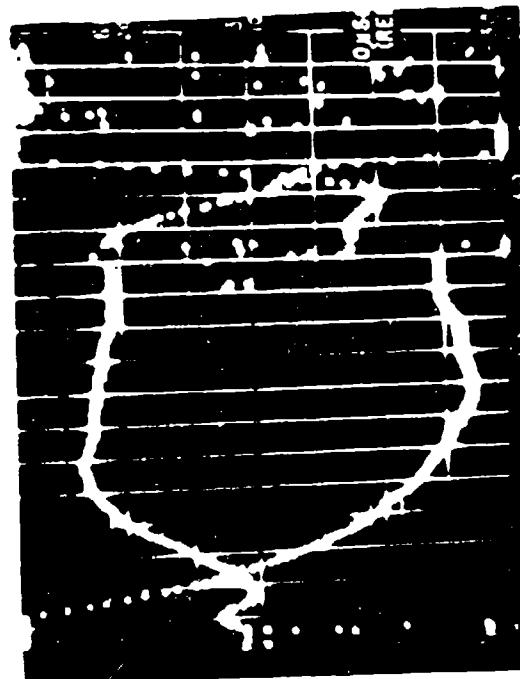
CALL #346



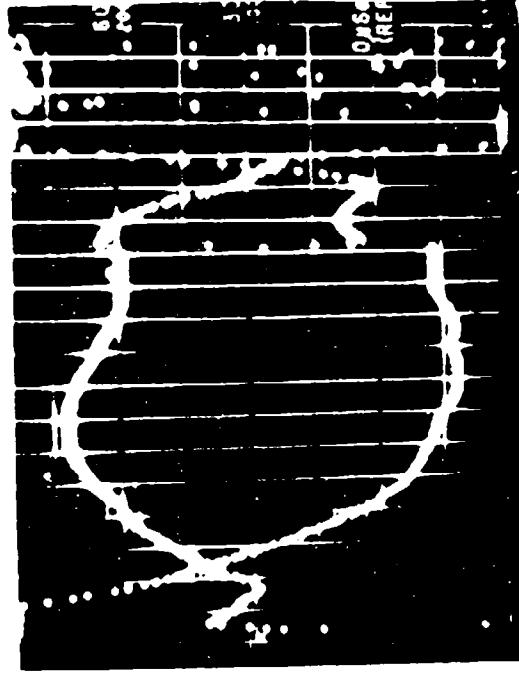
CALL #349



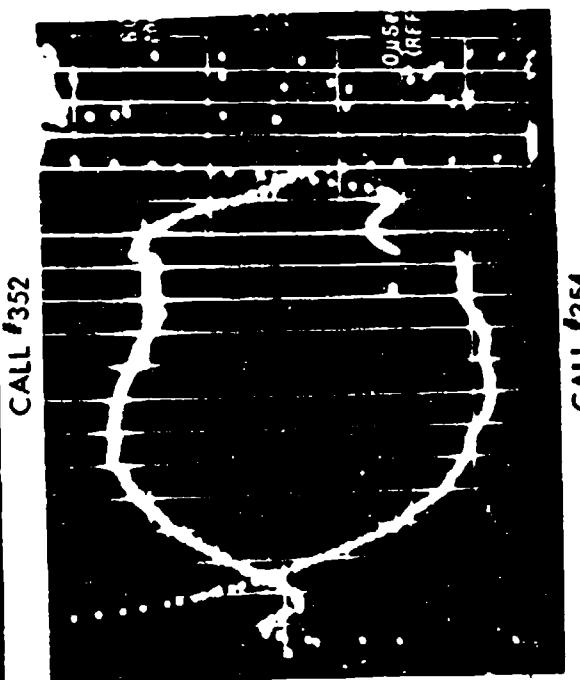
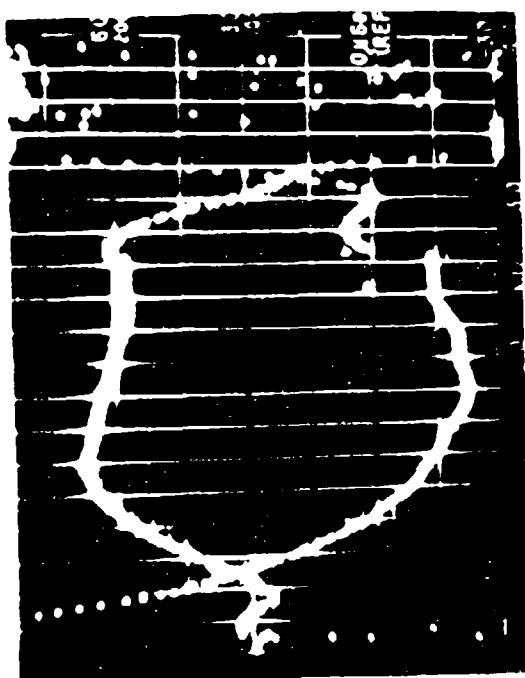
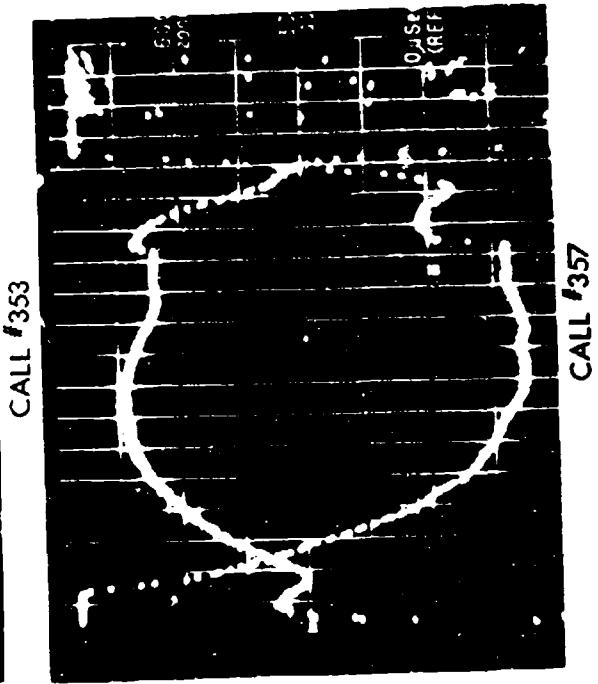
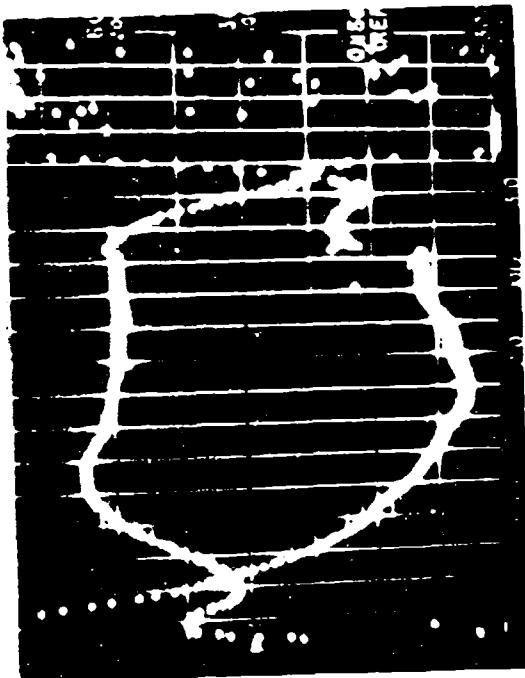
CALL #351

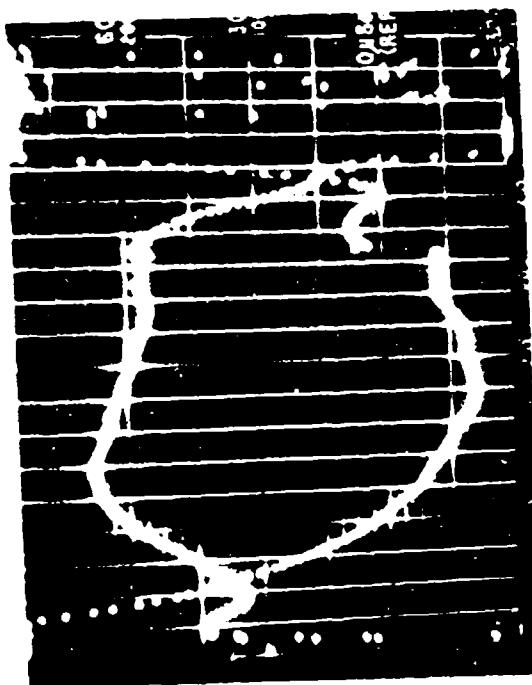


CALL #348

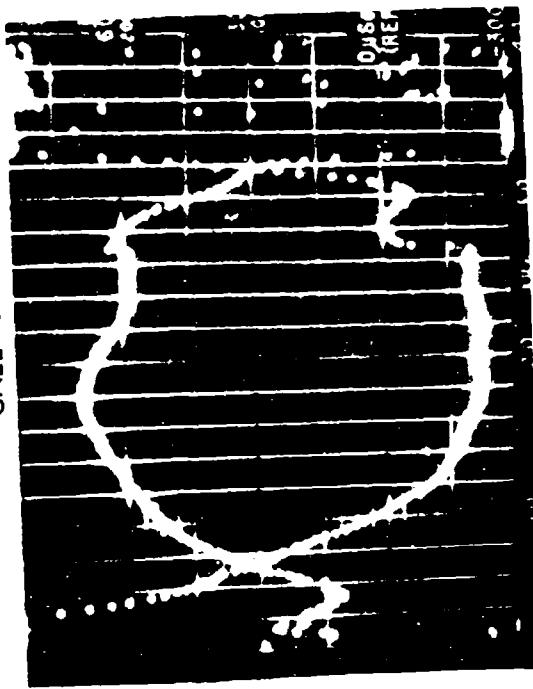


CALL #350

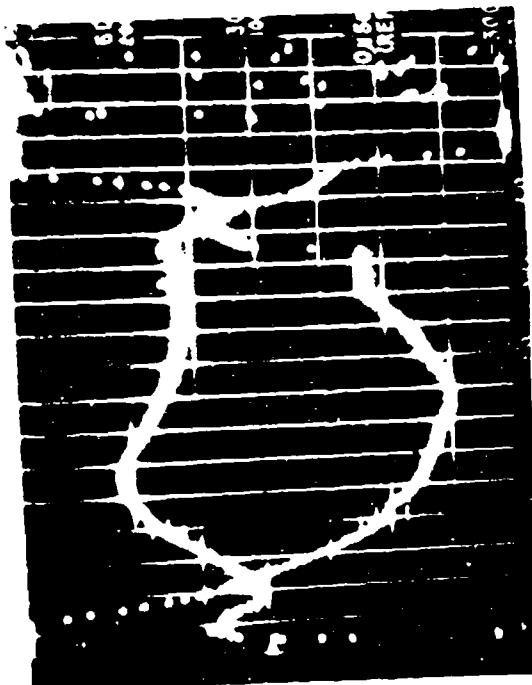




CALL #359



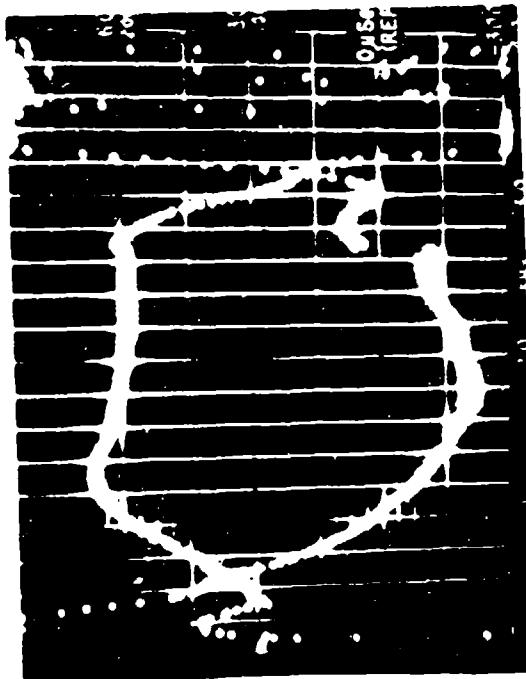
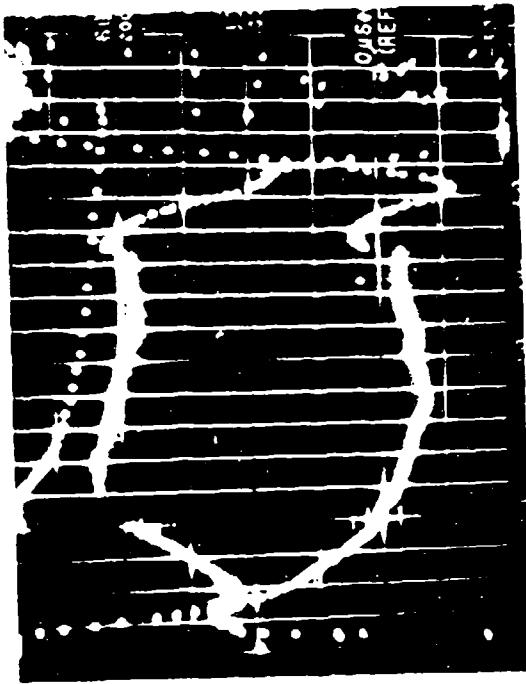
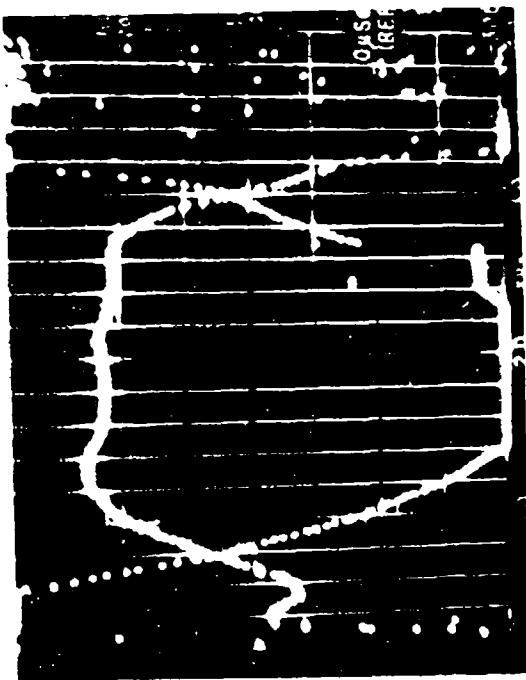
CALL #361

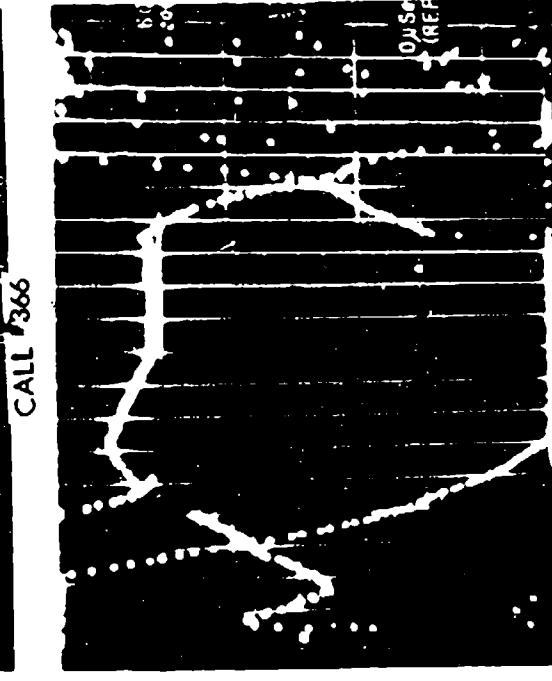
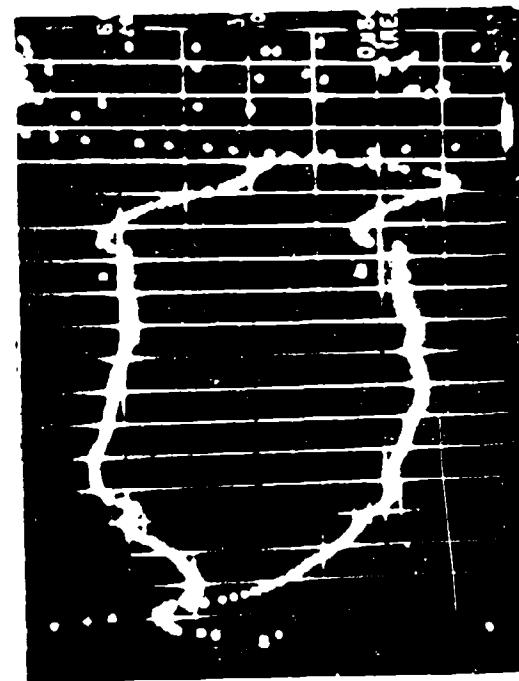
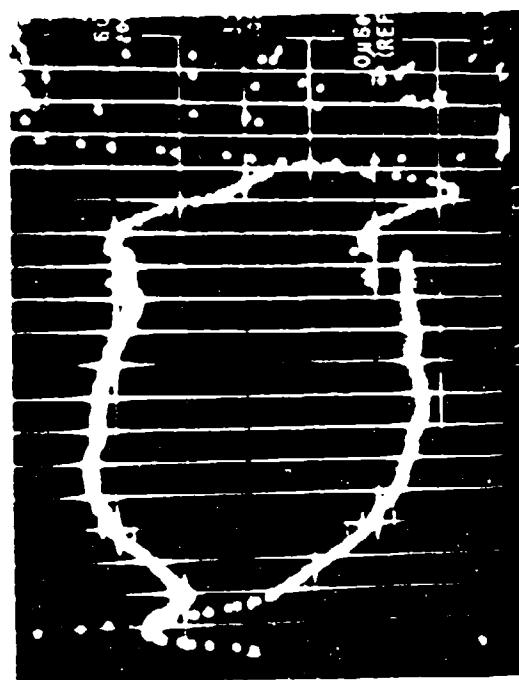


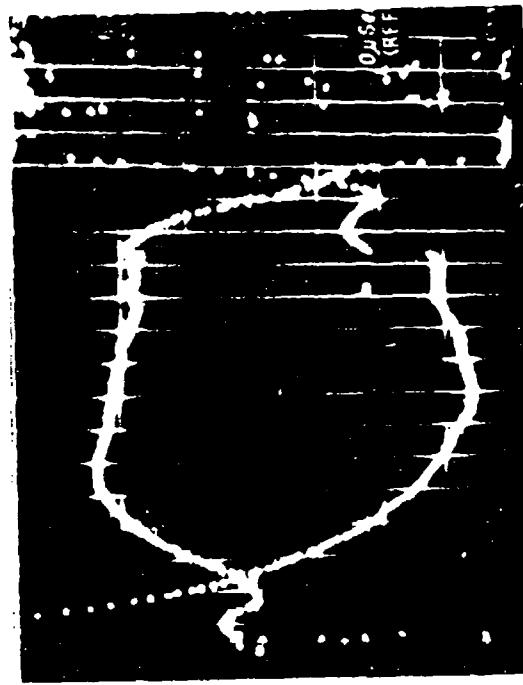
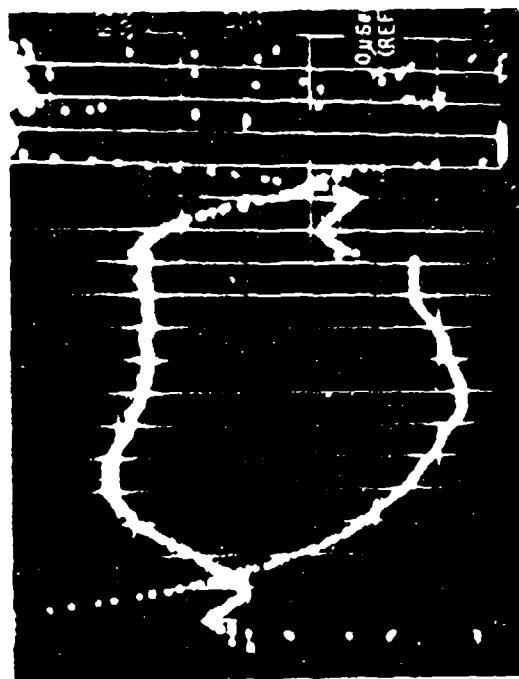
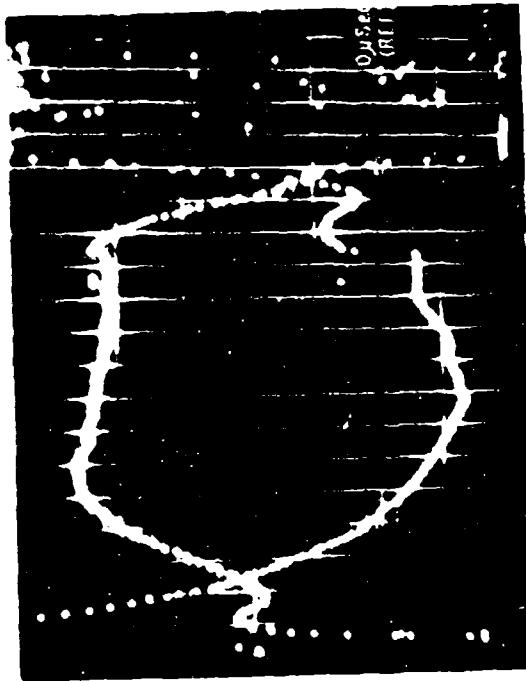
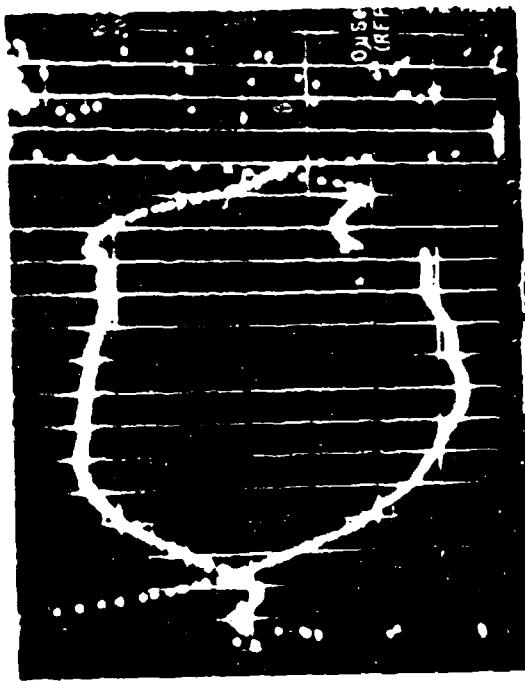
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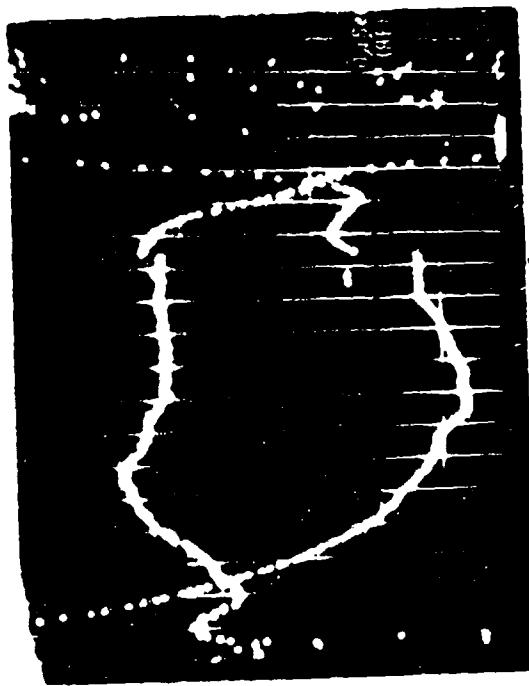


CALL #360

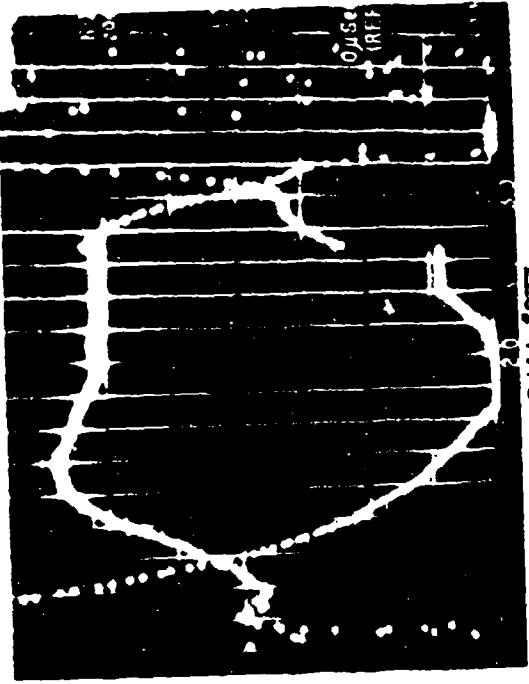




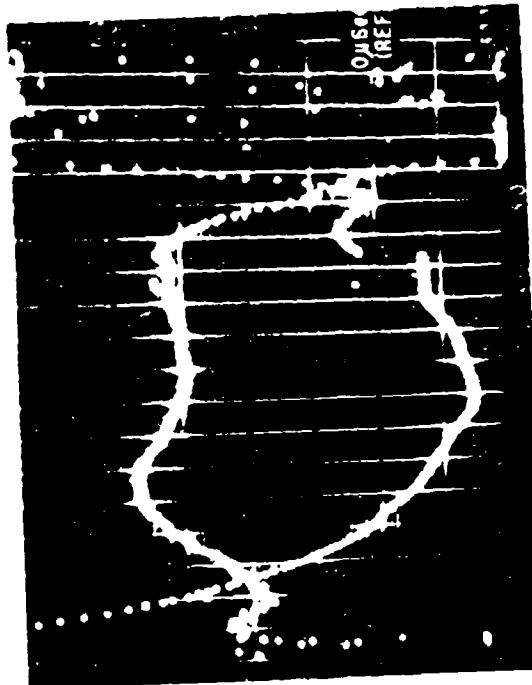




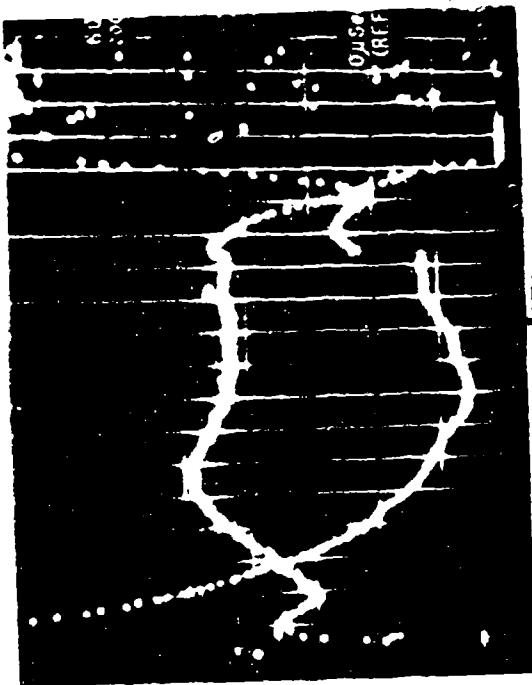
CALL #375



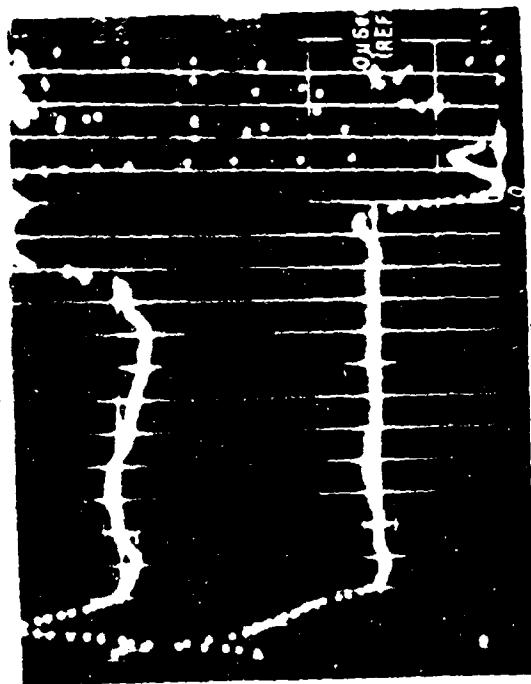
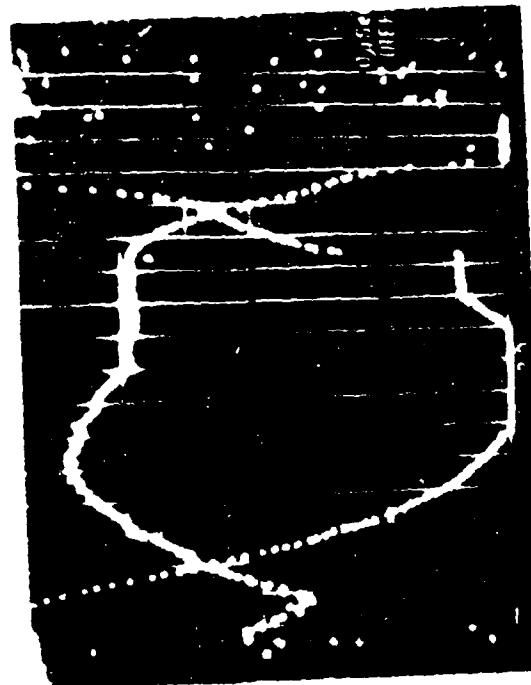
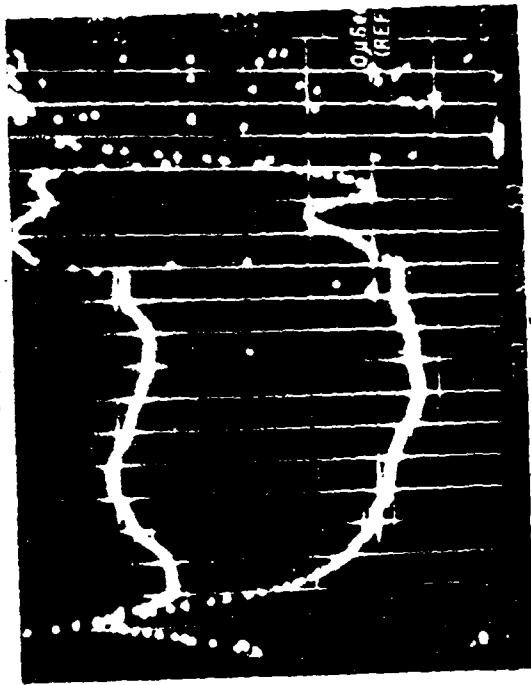
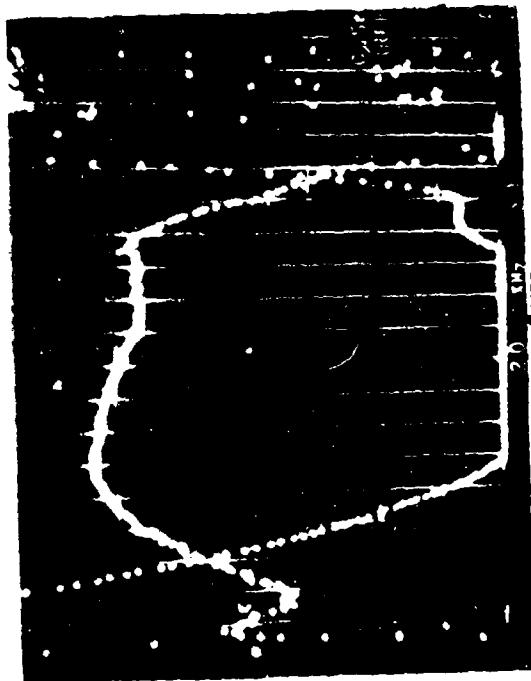
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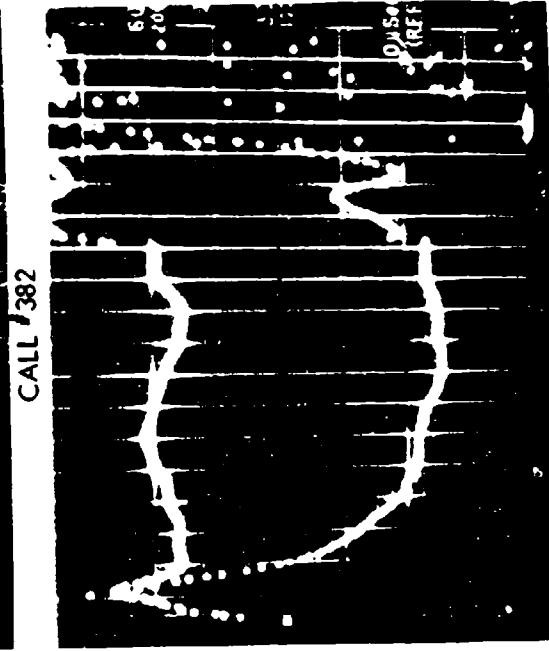
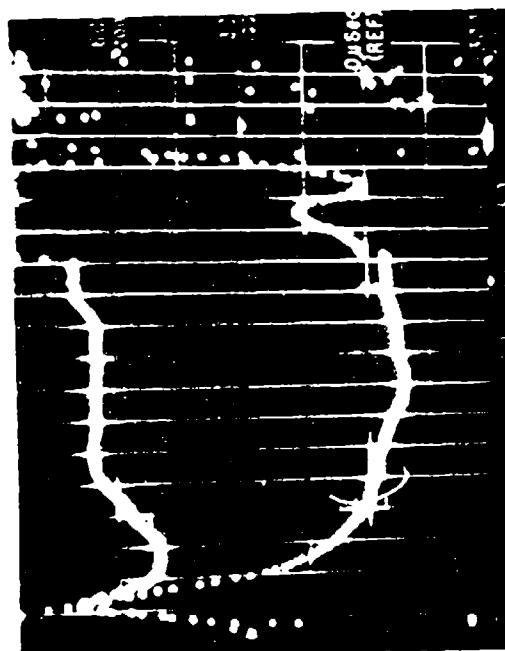
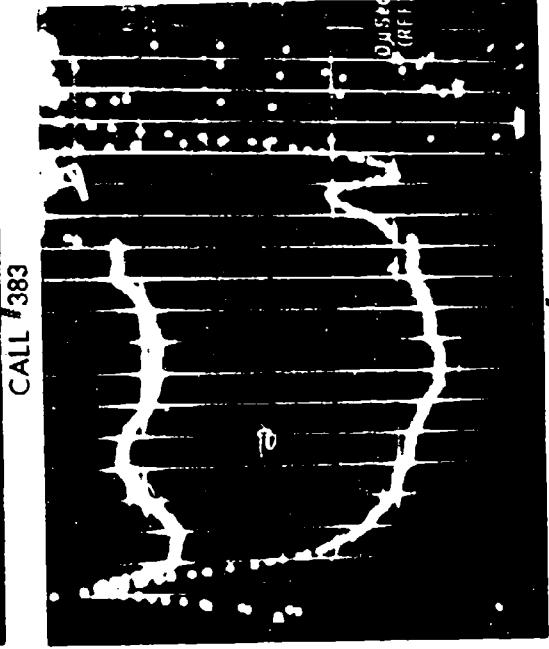


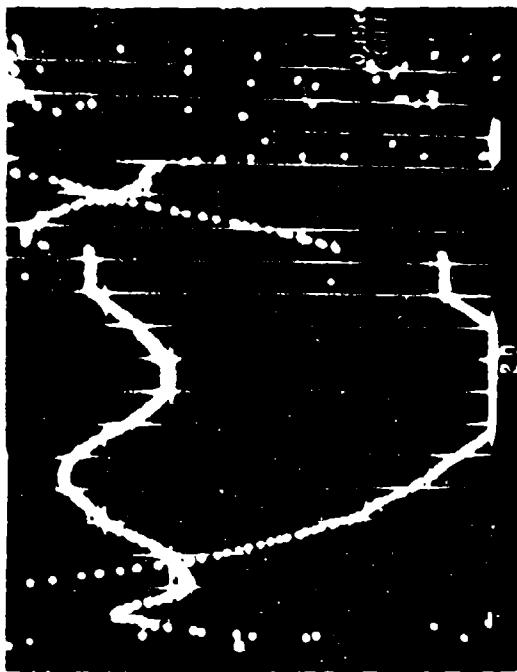
CALL #374



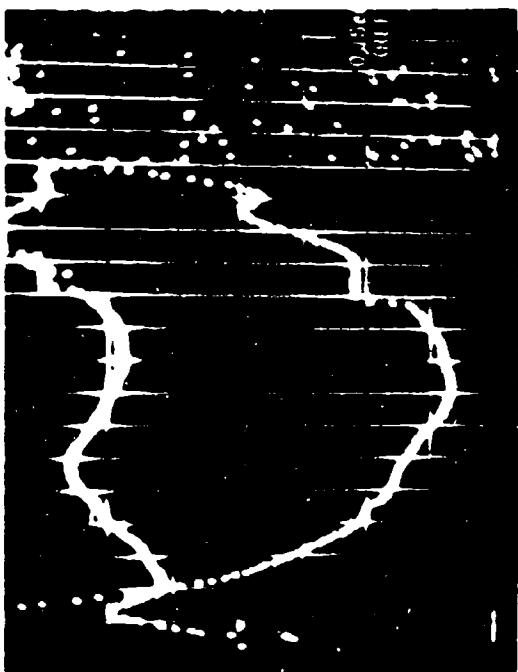
CALL #376







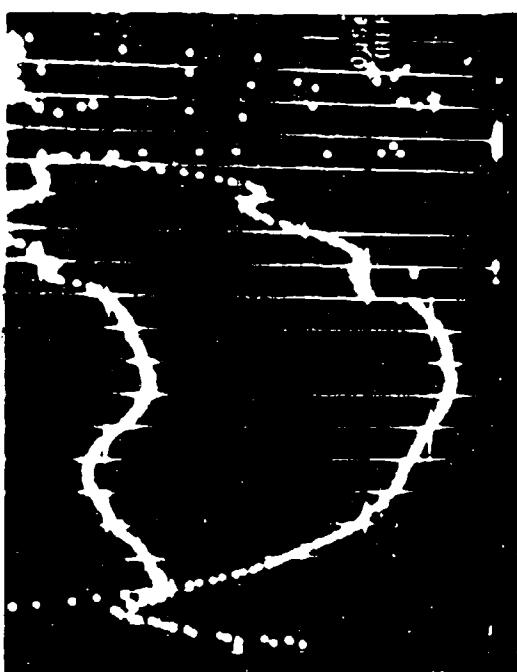
CALL #387



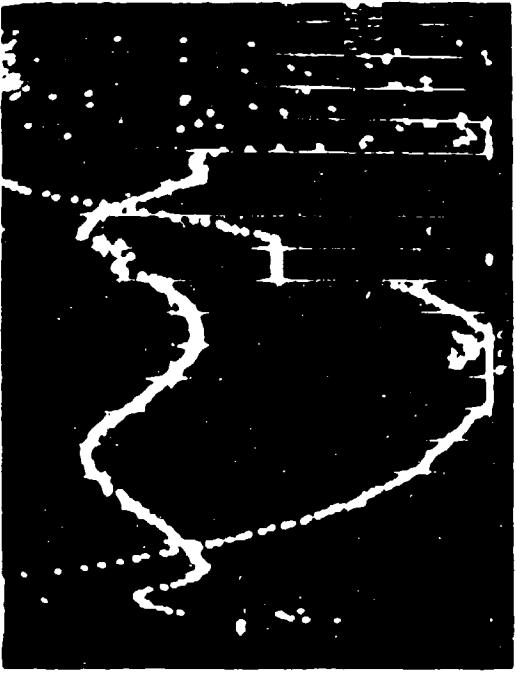
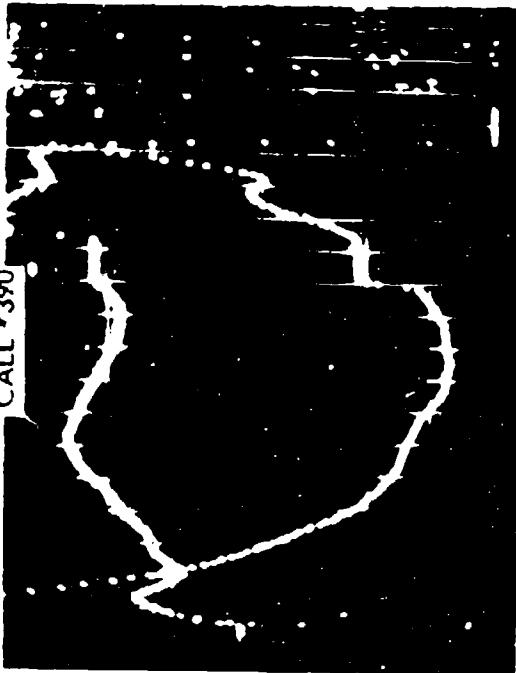
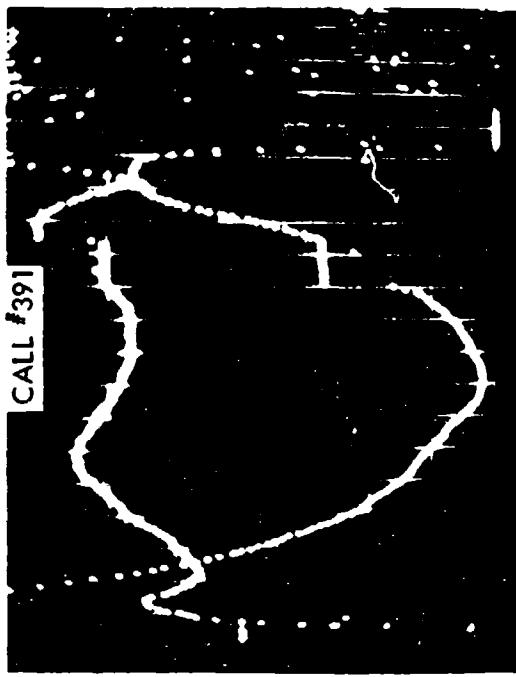
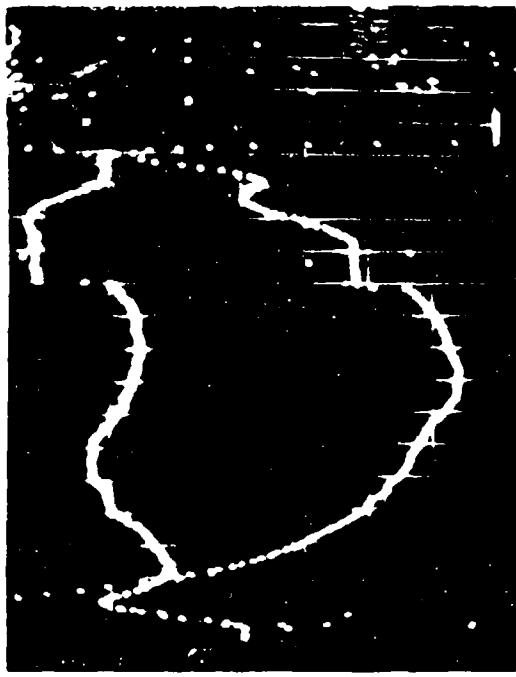
CALL #389



CALL #386



CALL #388

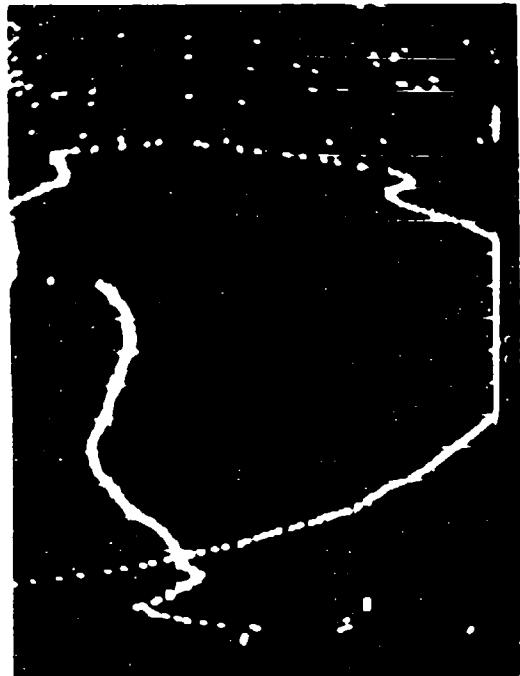


CALL #391

CALL #390

CALL #393

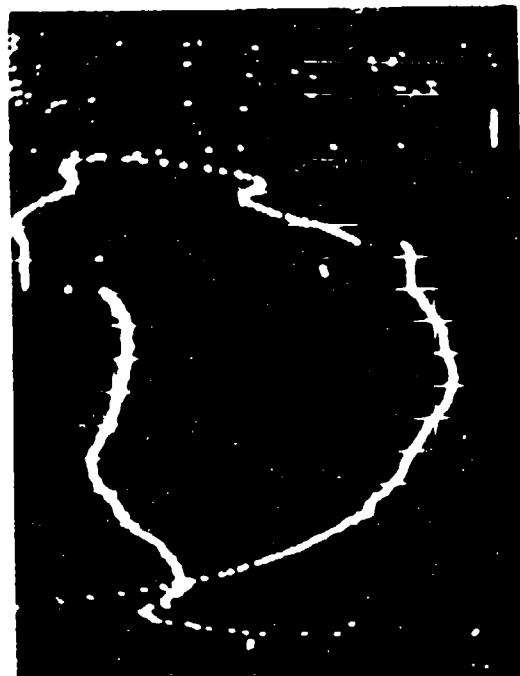
CALL #392



CALL #395



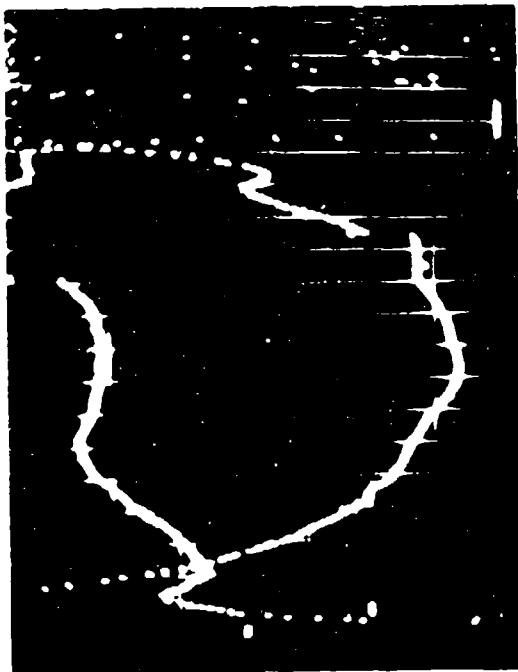
CALL #397



CALL #394



CALL #396



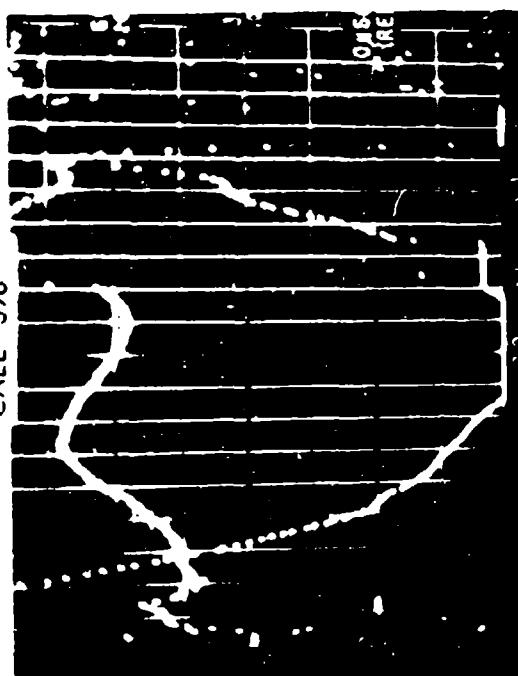
CALL #399



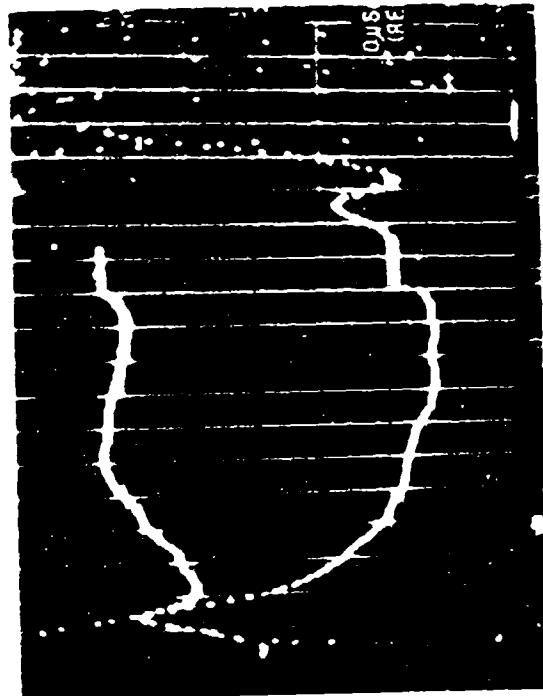
CALL #401



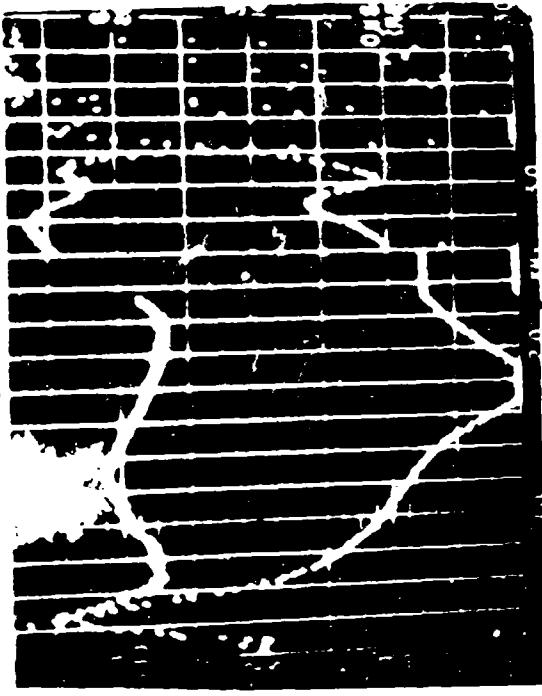
CALL #398



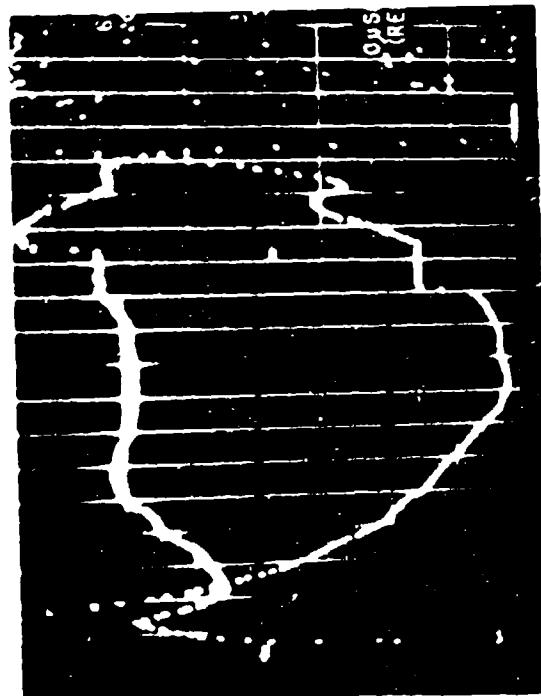
CALL #400



CALL #403



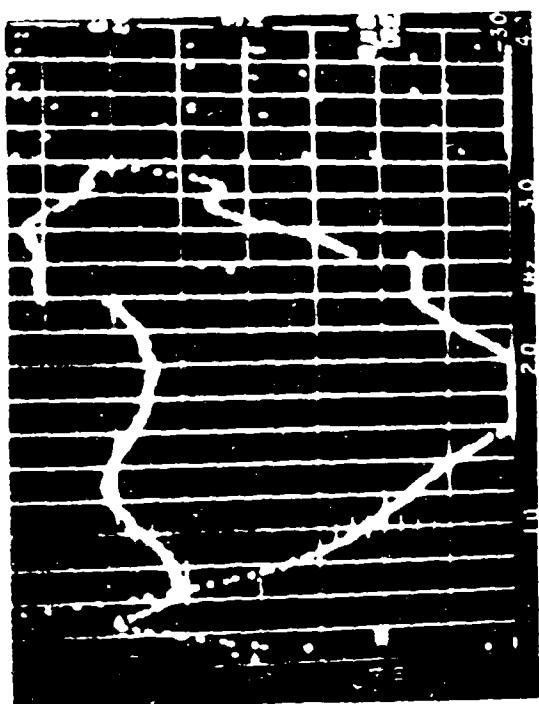
CALL #405



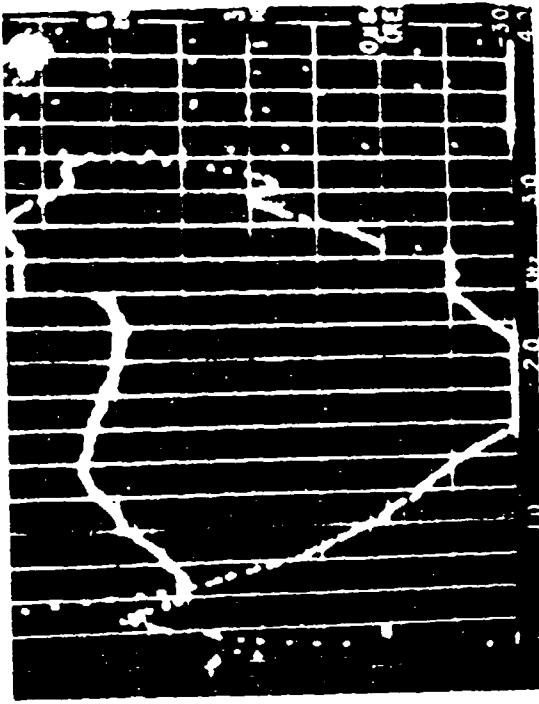
CALL #402



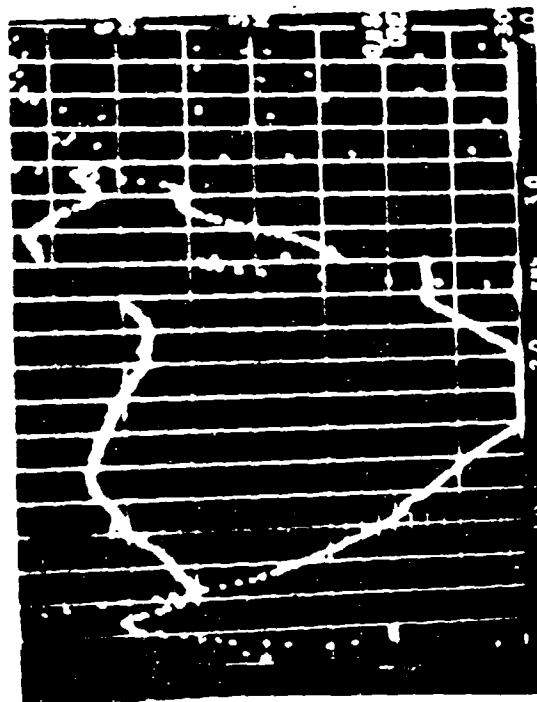
CALL #404



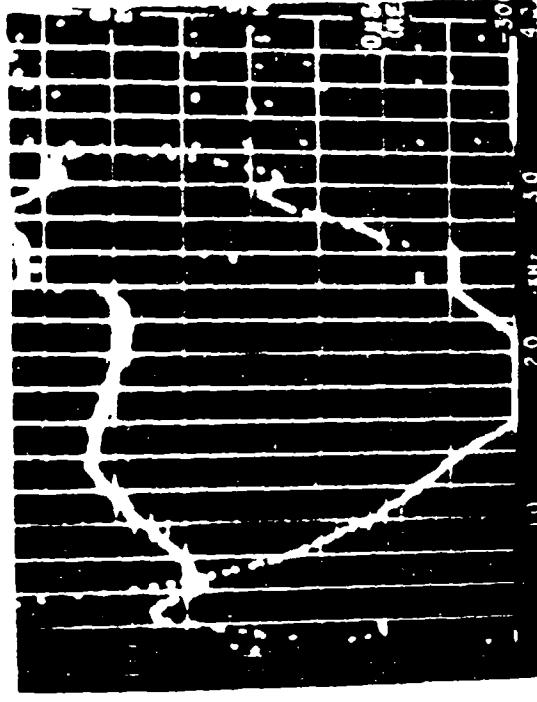
CALL #407



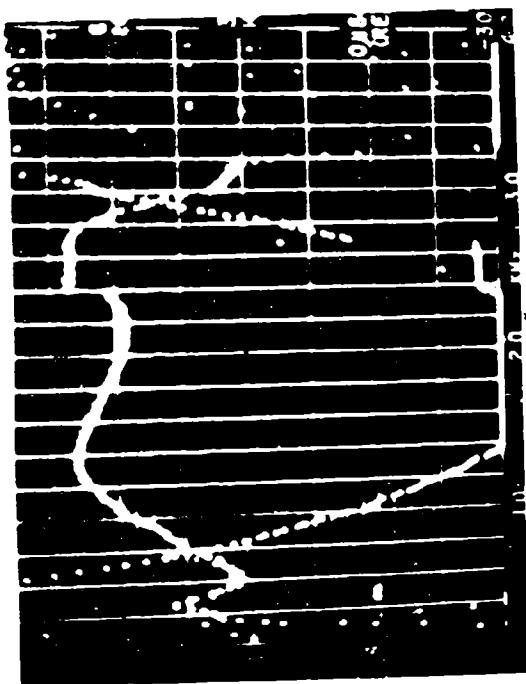
CALL #409



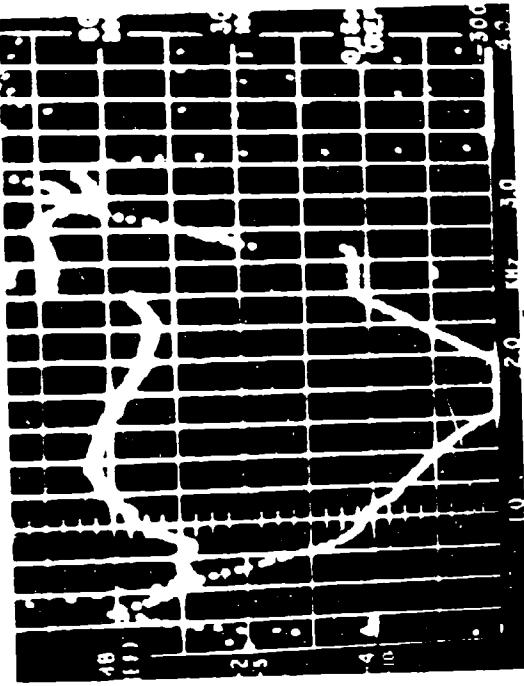
CALL #406



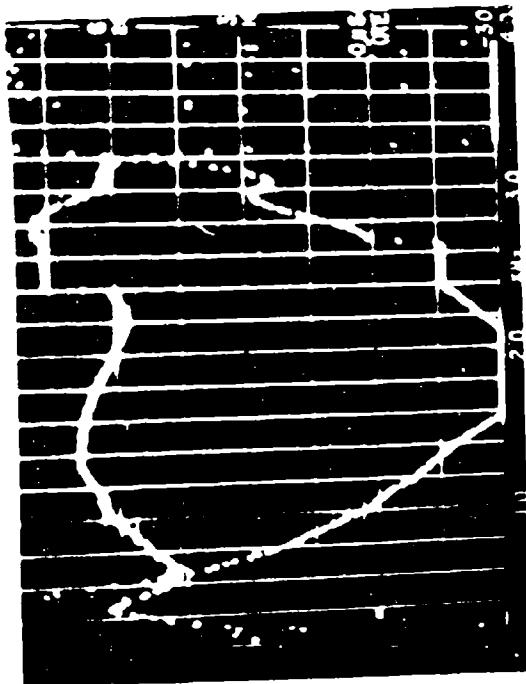
CALL #408



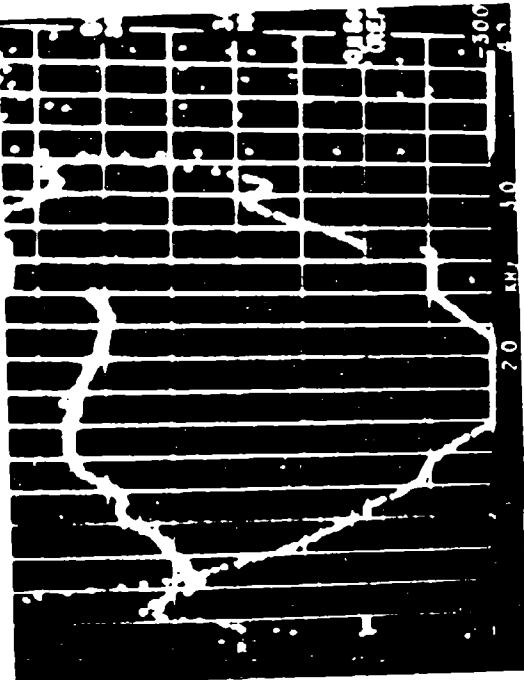
CALL #411



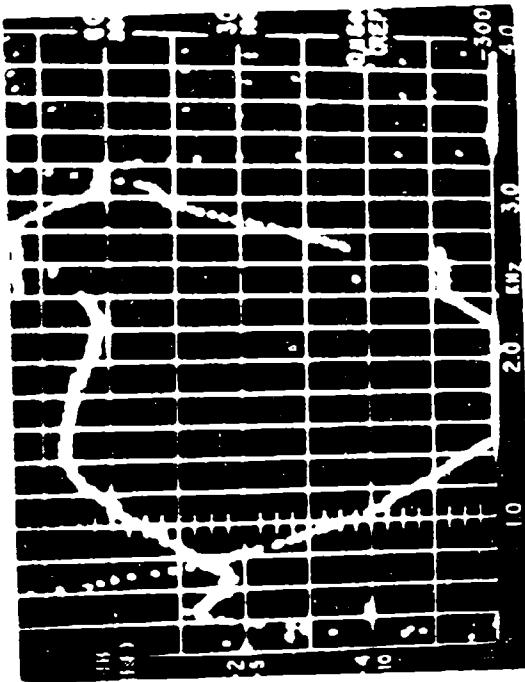
CALL #413



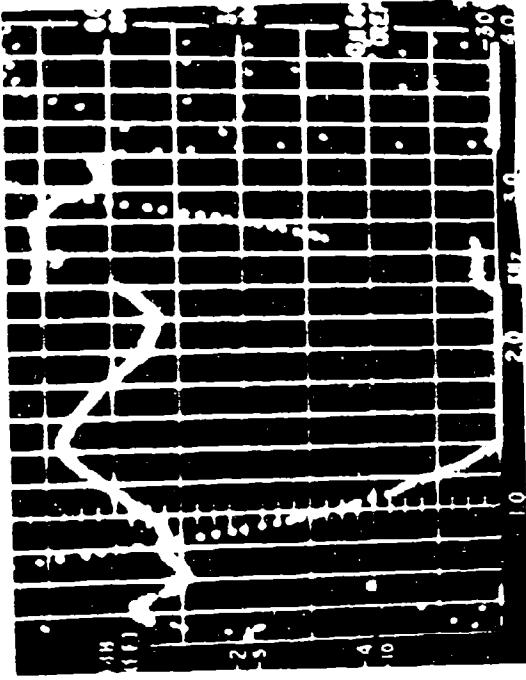
CALL #410



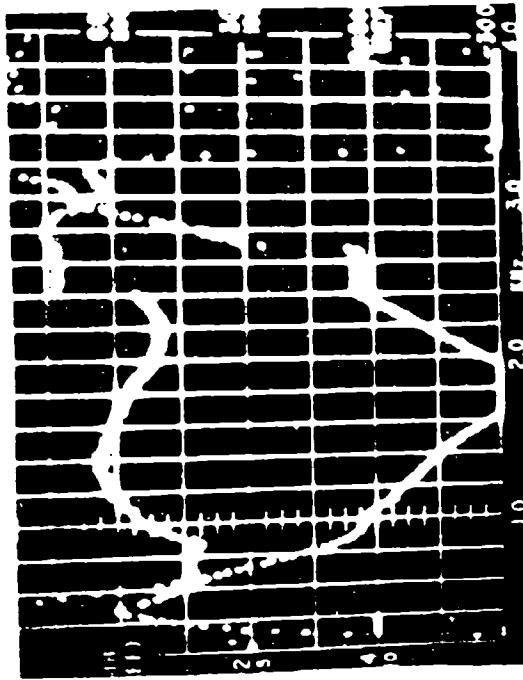
CALL #412



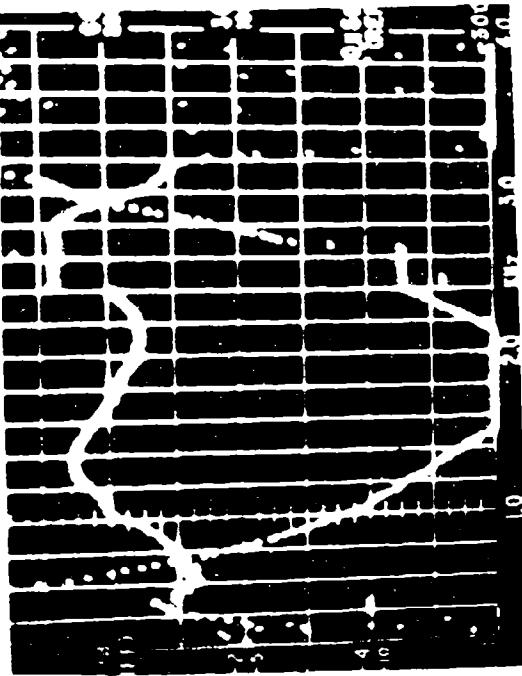
CALL #415



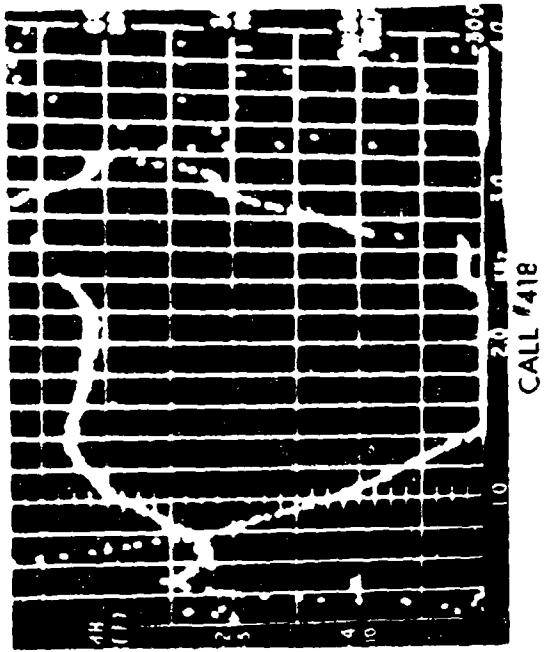
CALL #417



CALL #414

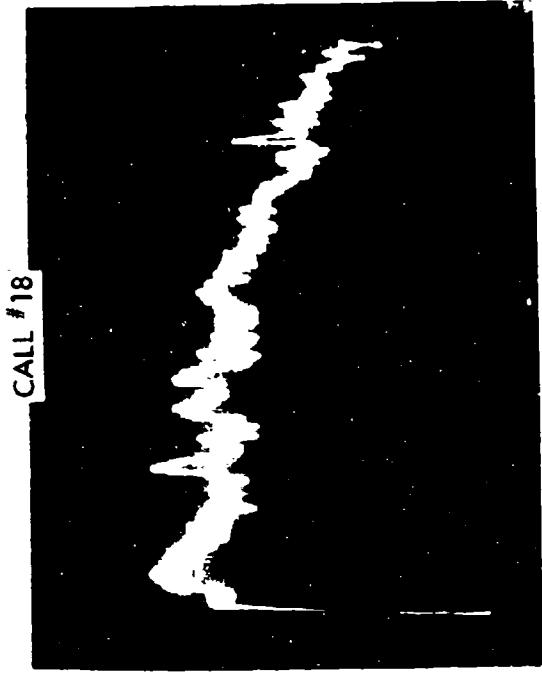
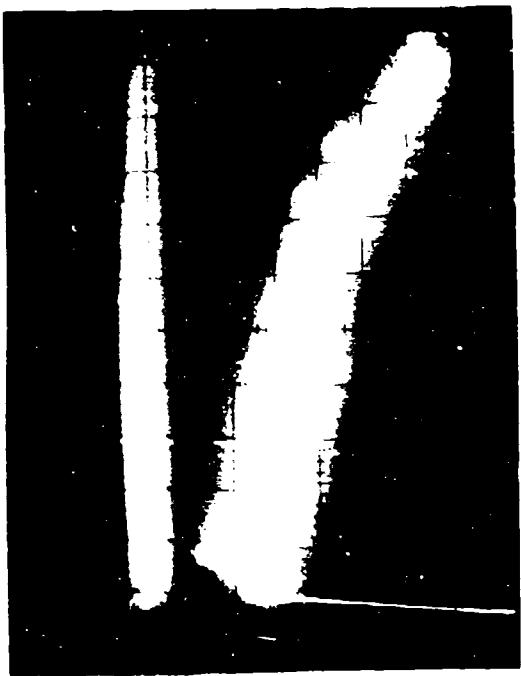


CALL #416

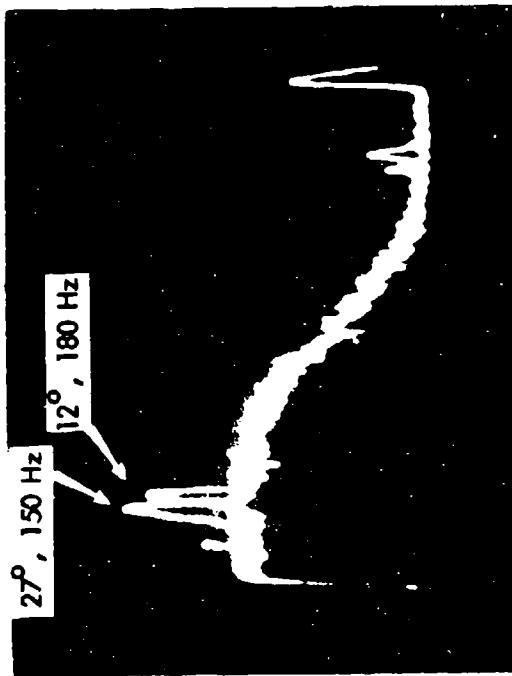


CALL #418

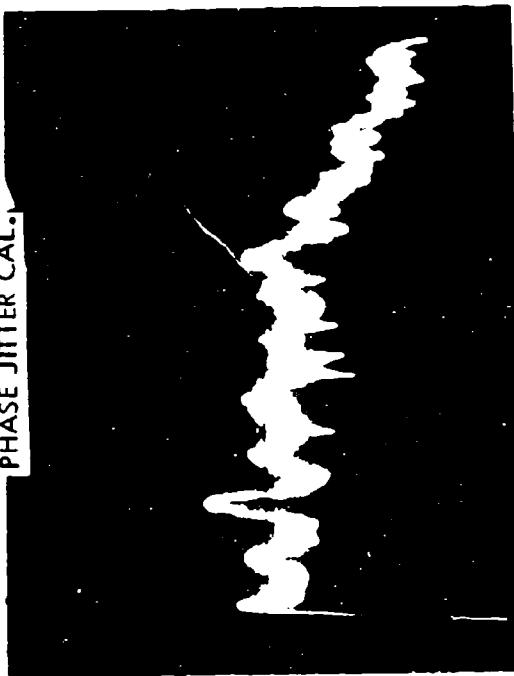
**PHASE JITTER PHOTOGRAPHS**



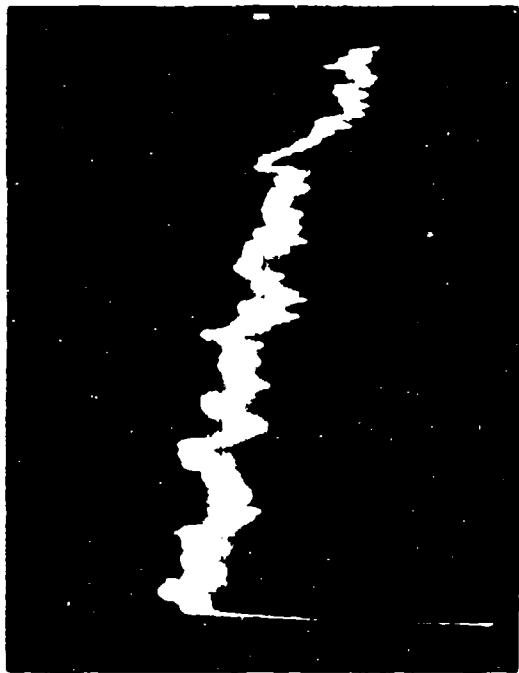
CALL #18



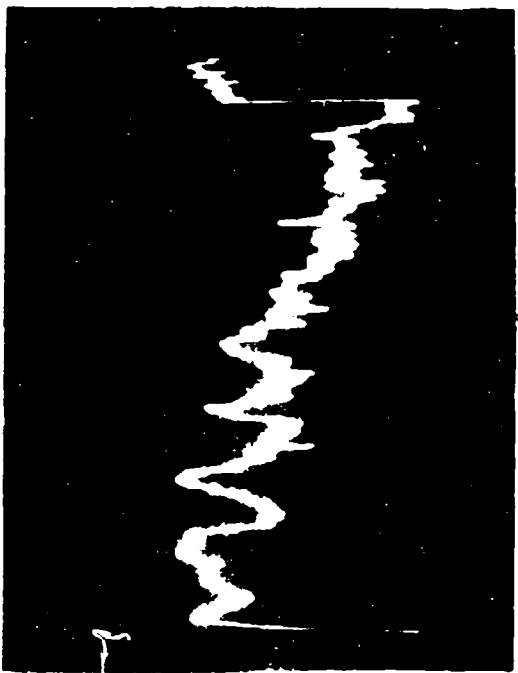
PHASE JITTER CAL.



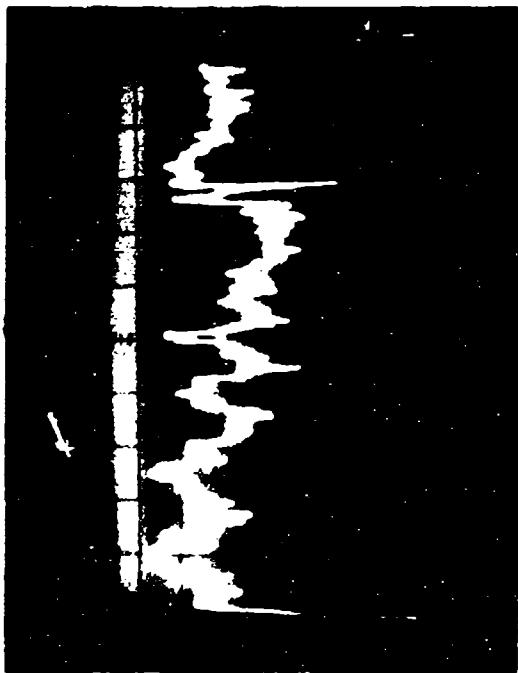
CALL #20



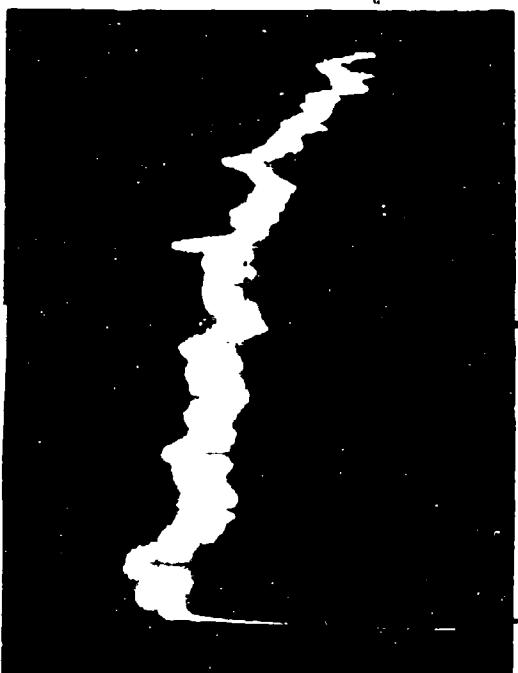
CALL #23



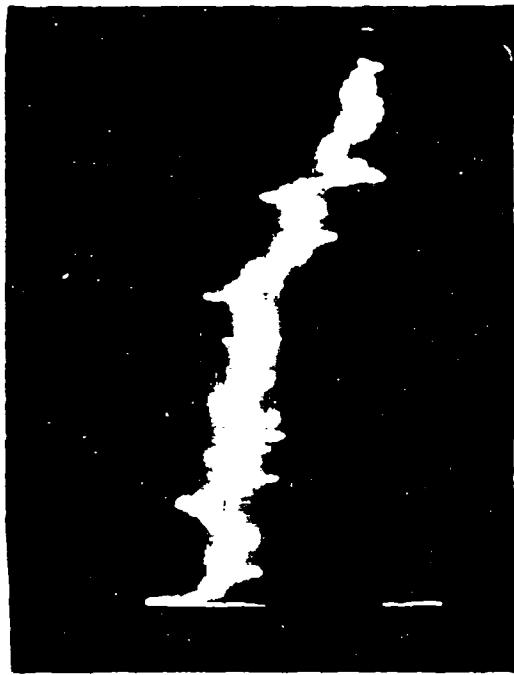
CALL #27



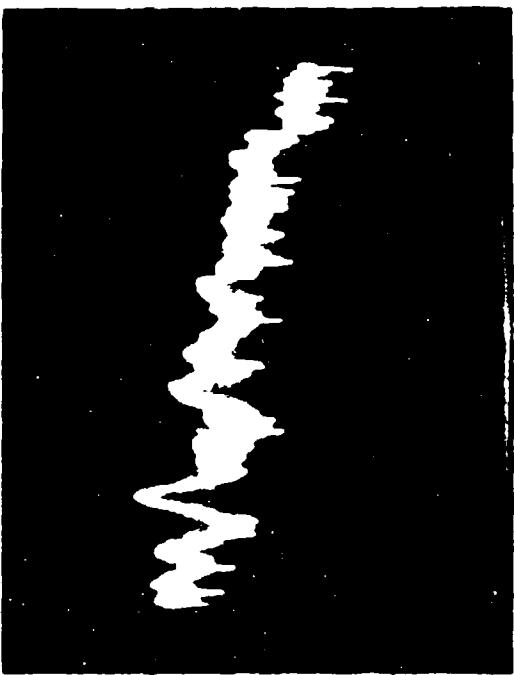
CALL #22



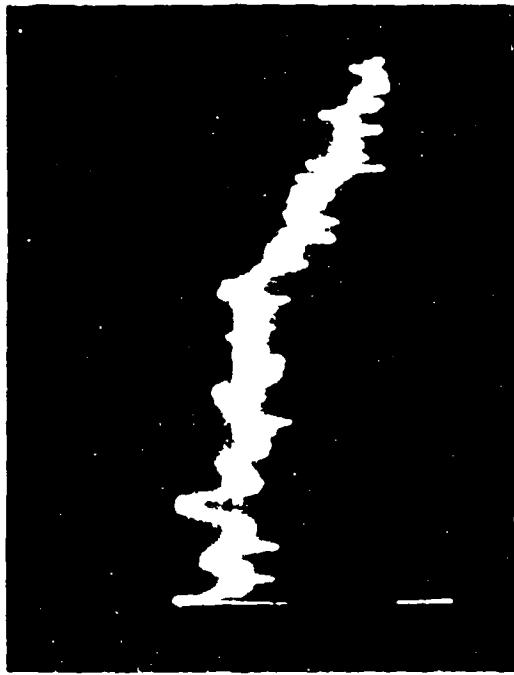
CALL #24



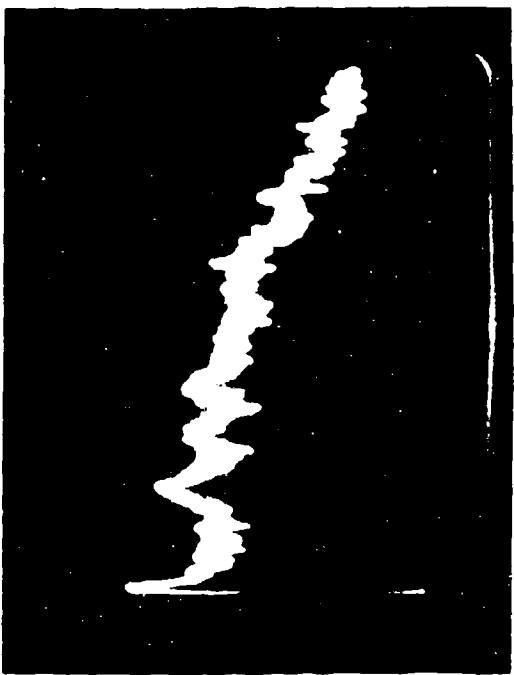
CALL #31



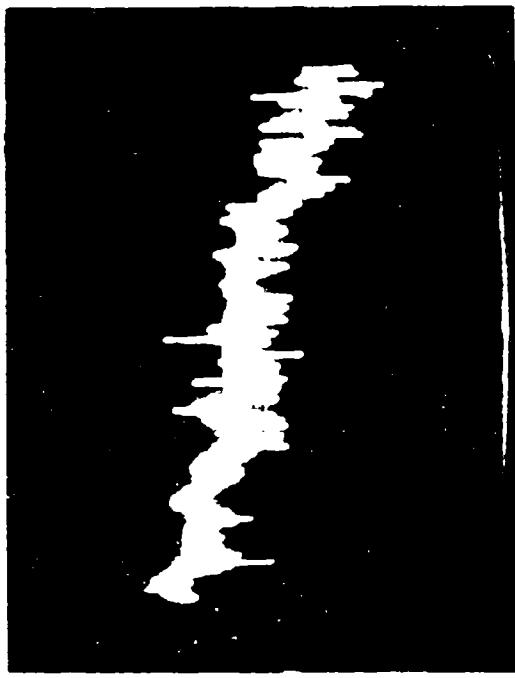
CALL #38



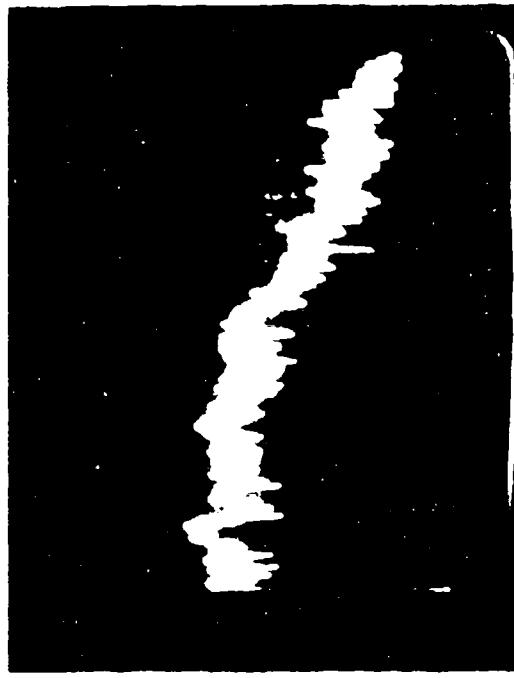
CALL #30



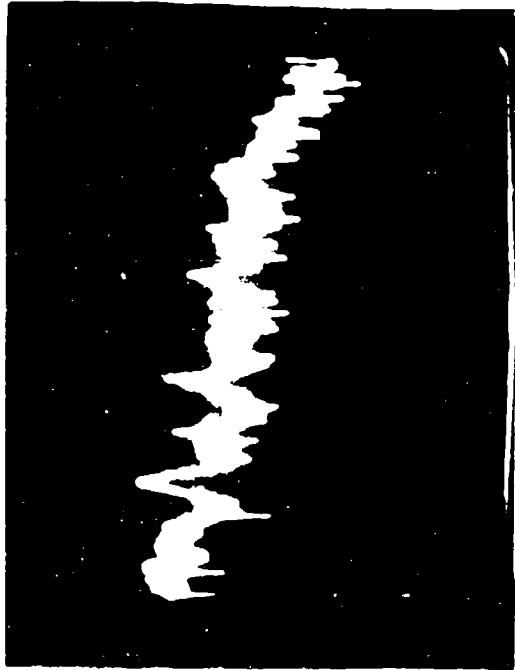
CALL #37



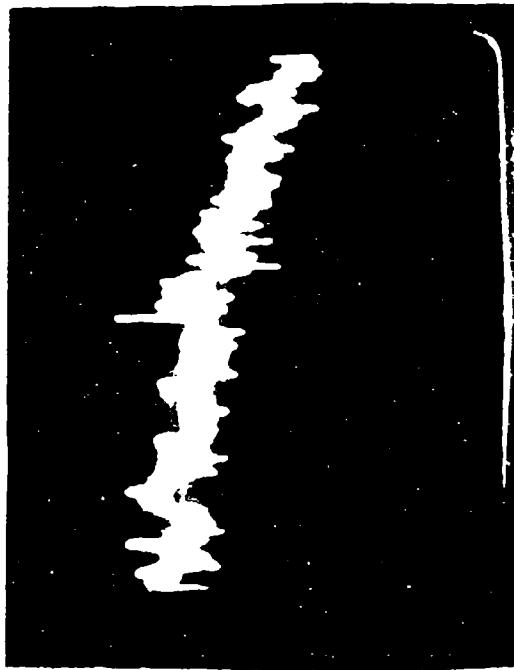
CALL #46



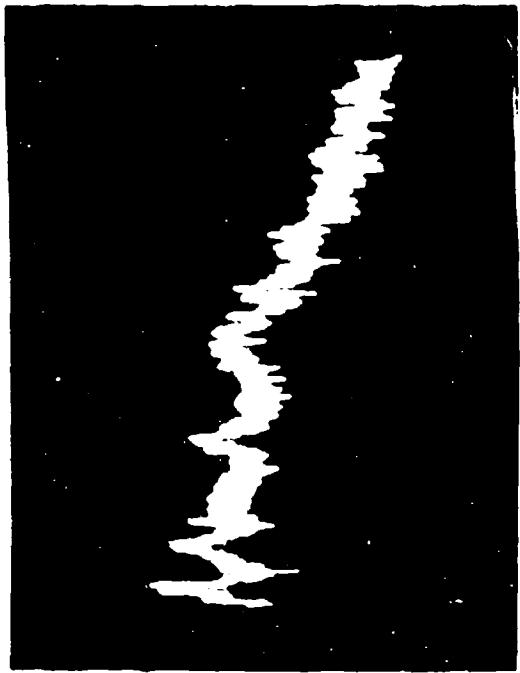
CALL #51



CALL #39



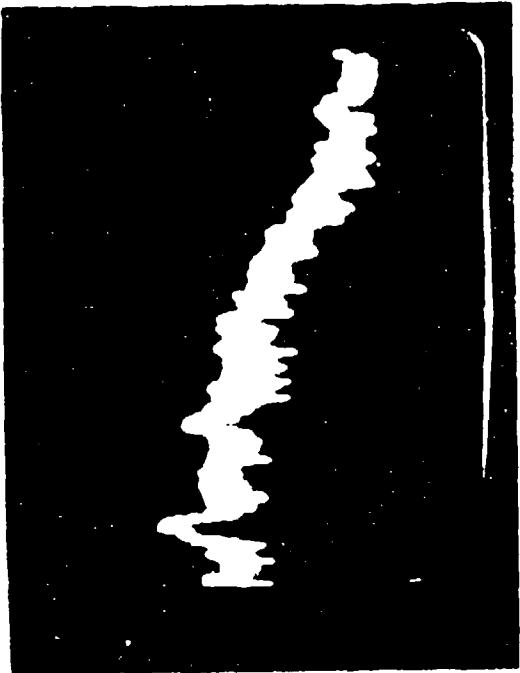
CALL #47



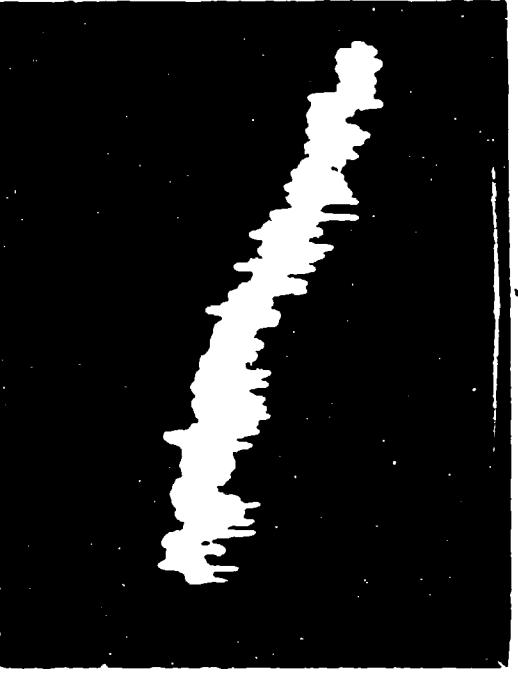
CALL #53



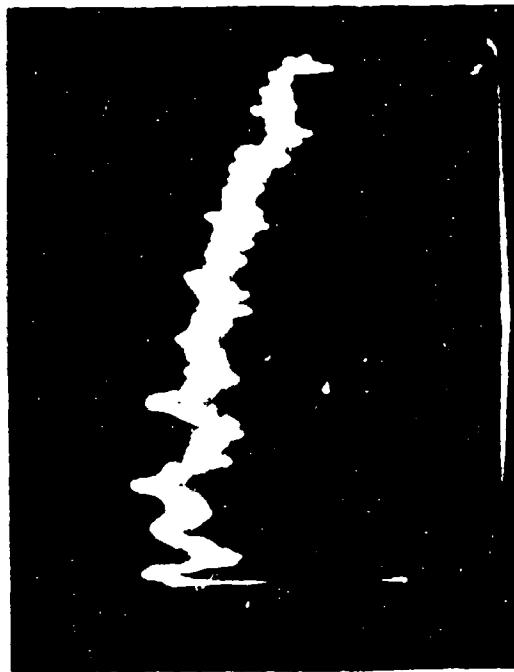
CALL #58



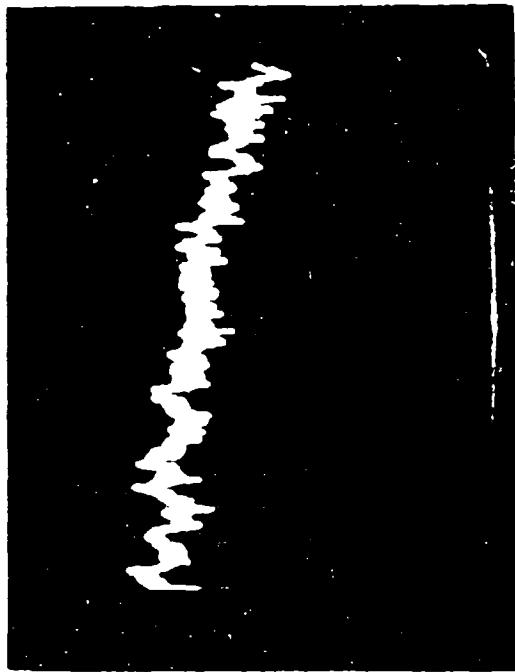
CALL #52



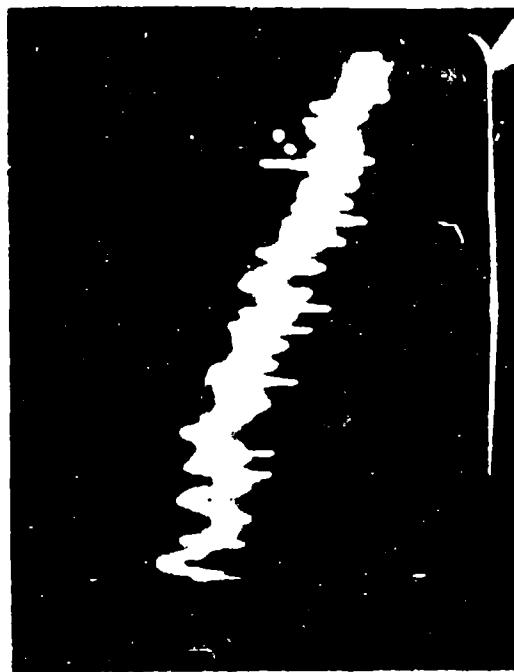
CALL #55



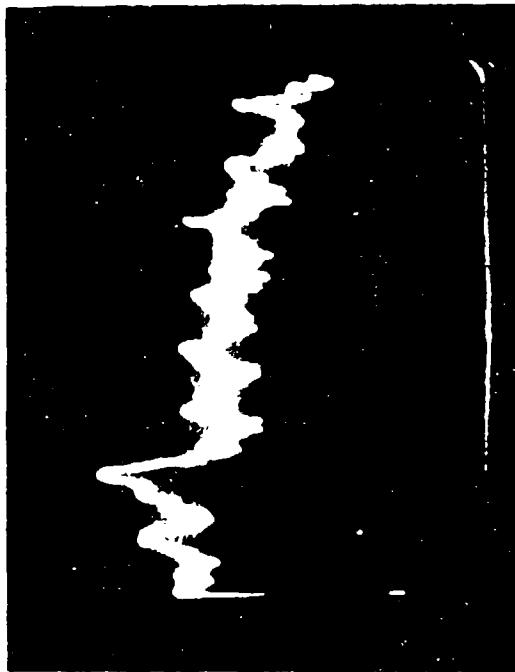
CALL #61



CALL #66



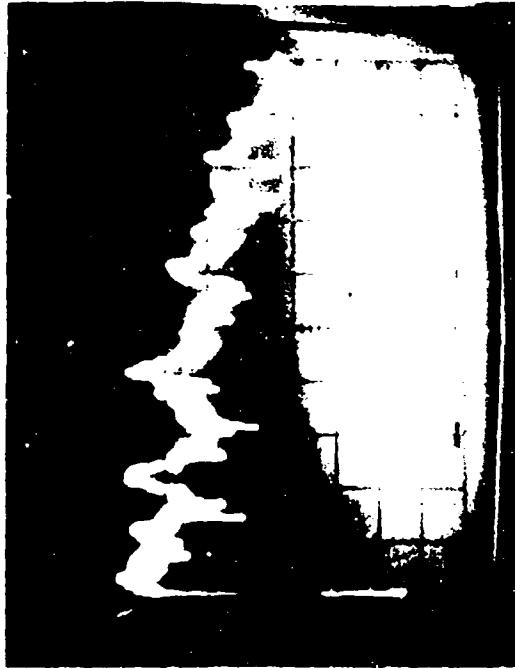
CALL #60



CALL #62



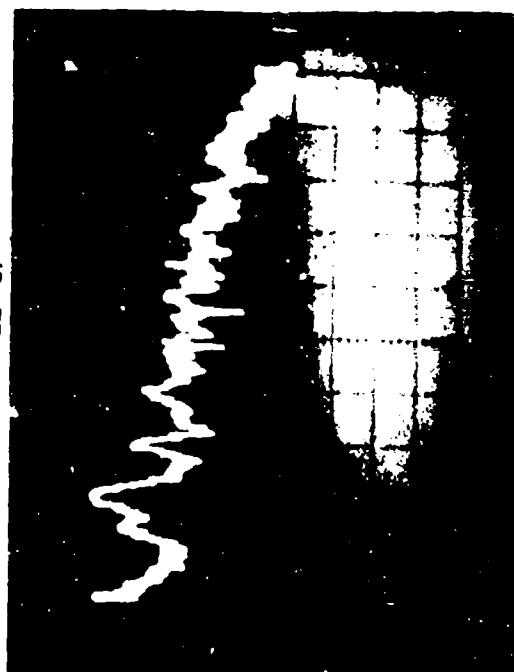
CALL #82



CALL #95



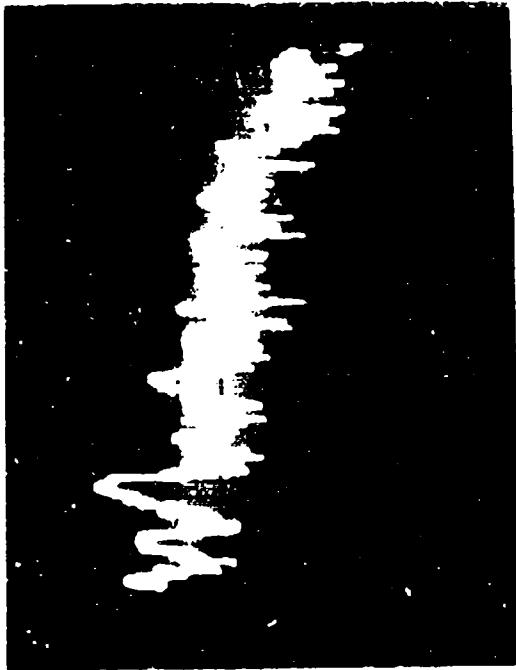
CALL #67



CALL #68



CALL #102



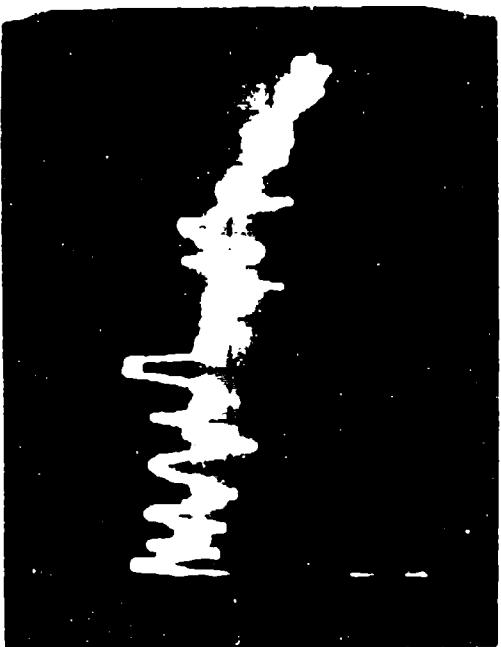
CALL #156



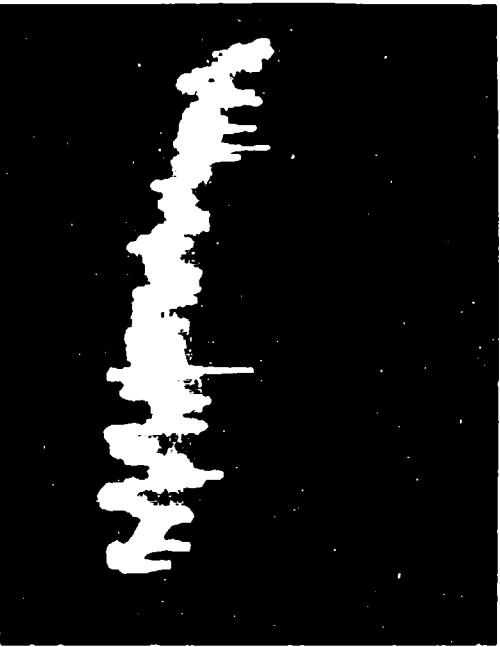
CALL #99



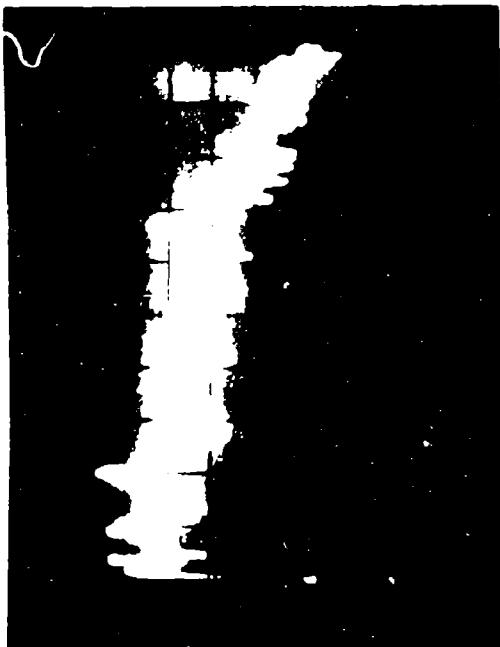
CALL #126



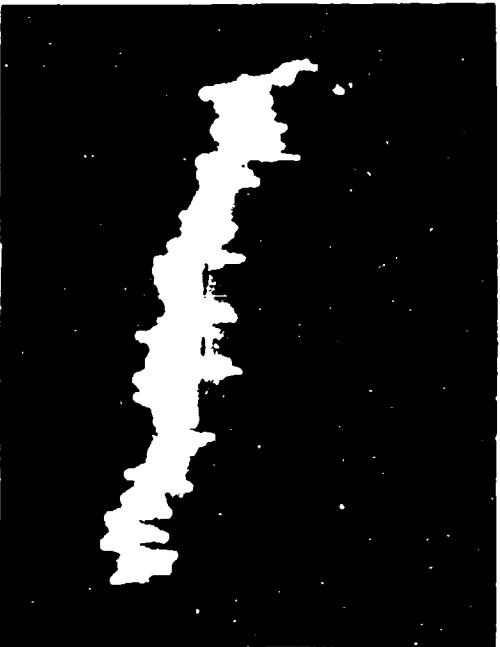
CALL #169



CALL #182



CALL #162



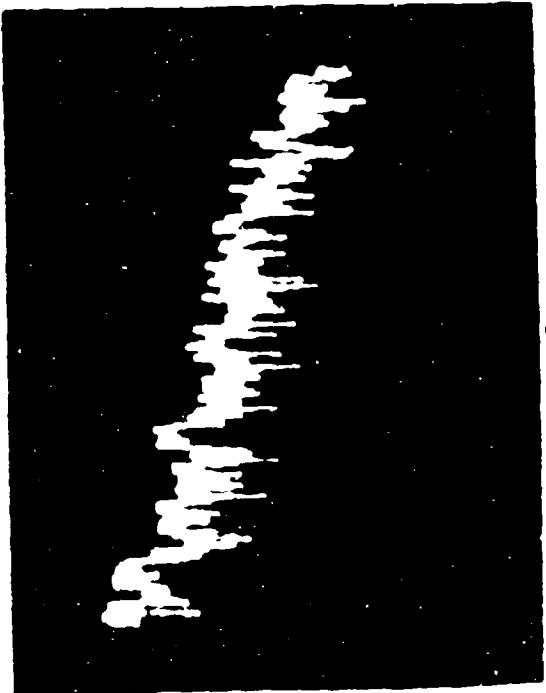
CALL #172



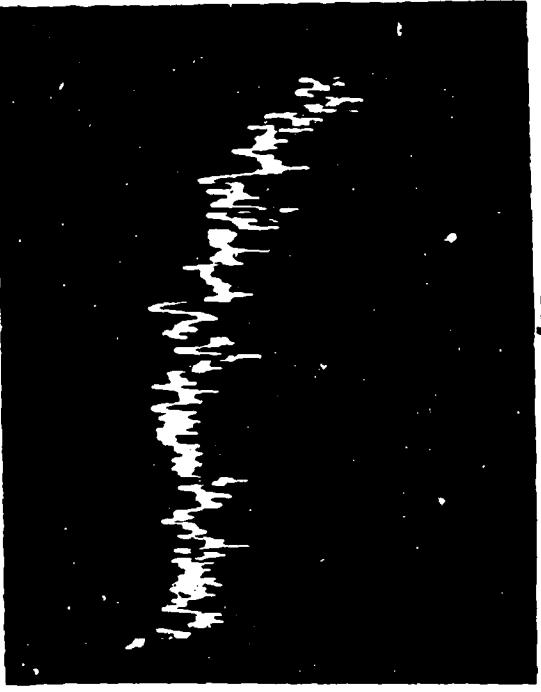
CALL #207



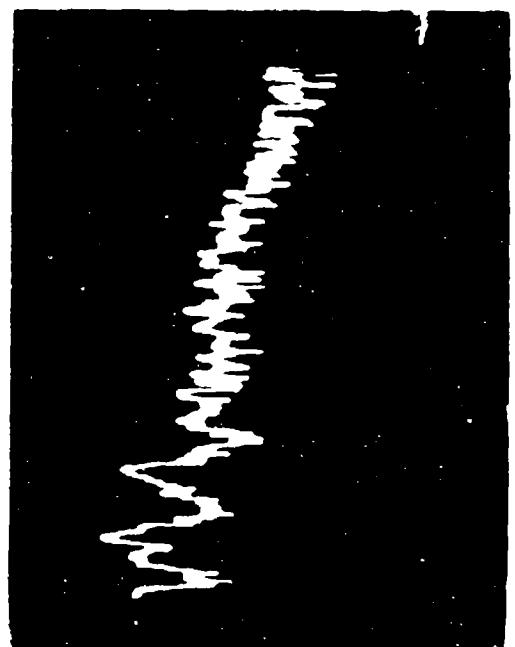
CALL #226



CALL #206



CALL #276



CALL #313

**AMPLITUDE VARIATION PHOTOGRAPHS**



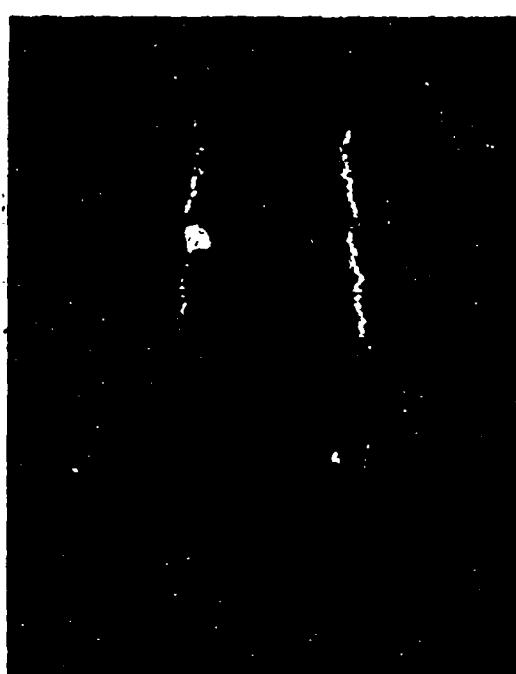
CALL #31 20 MS/DIV



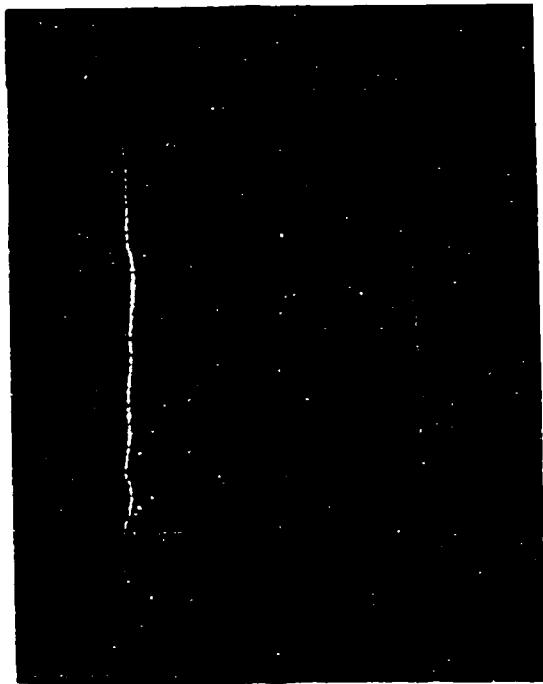
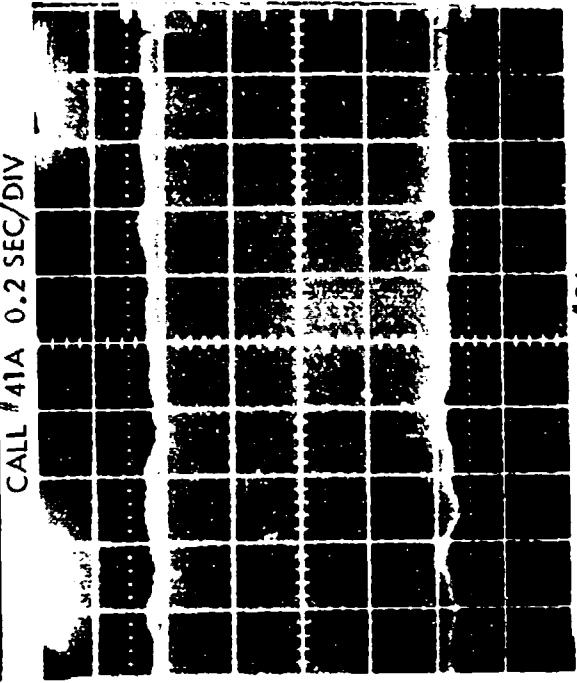
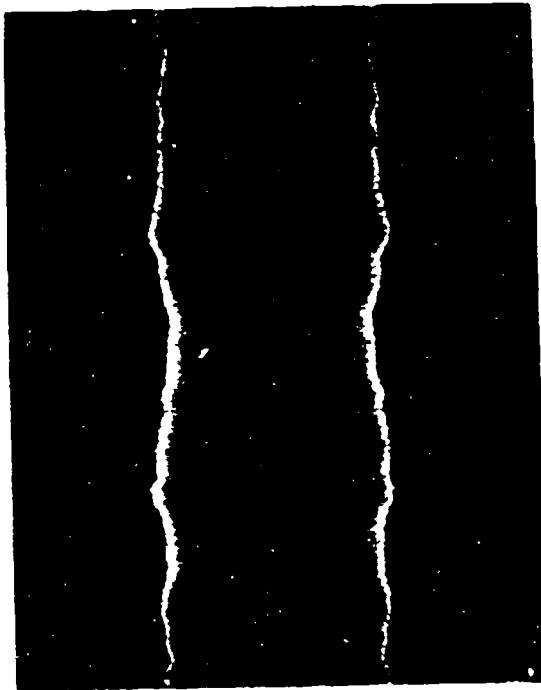
CALL #37 0.2 SEC/DIV

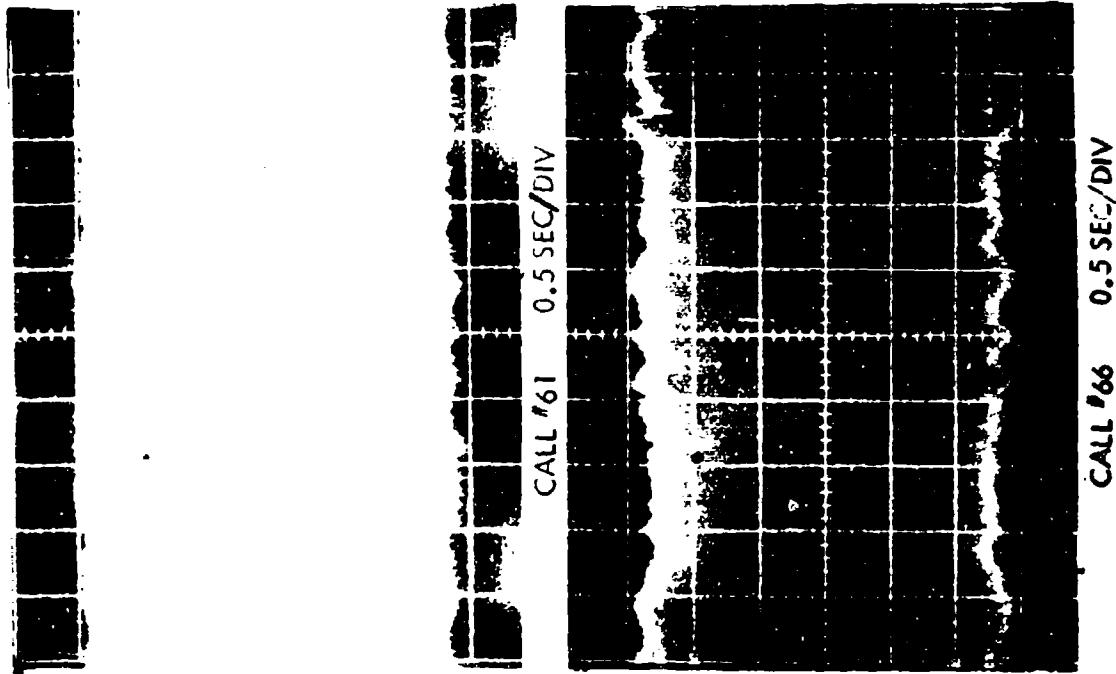
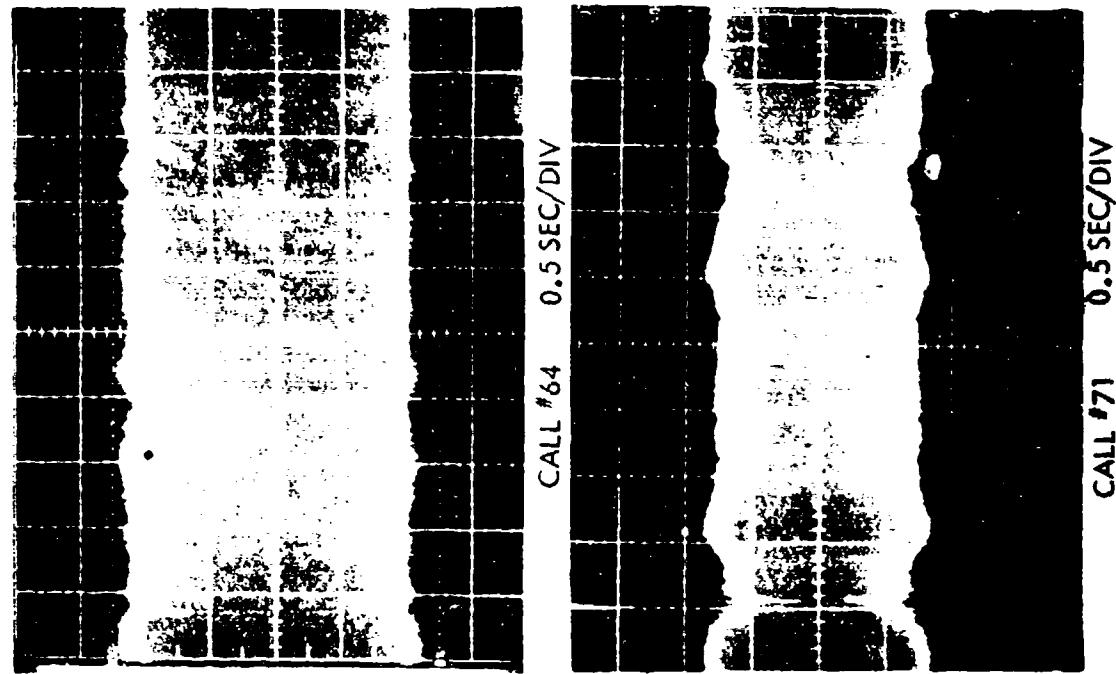


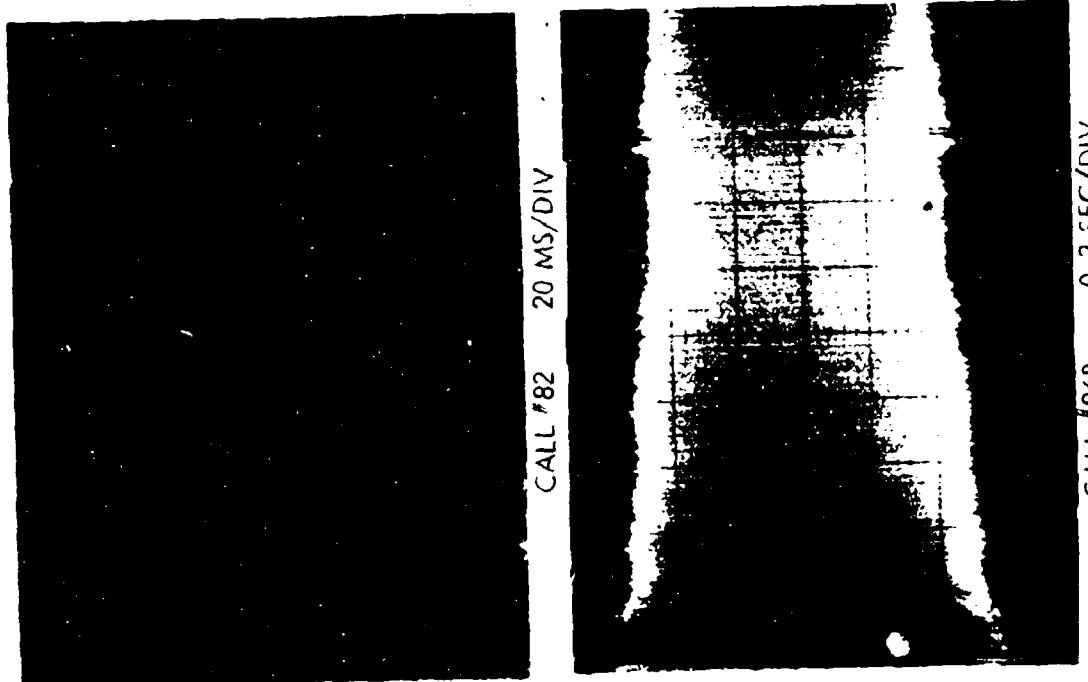
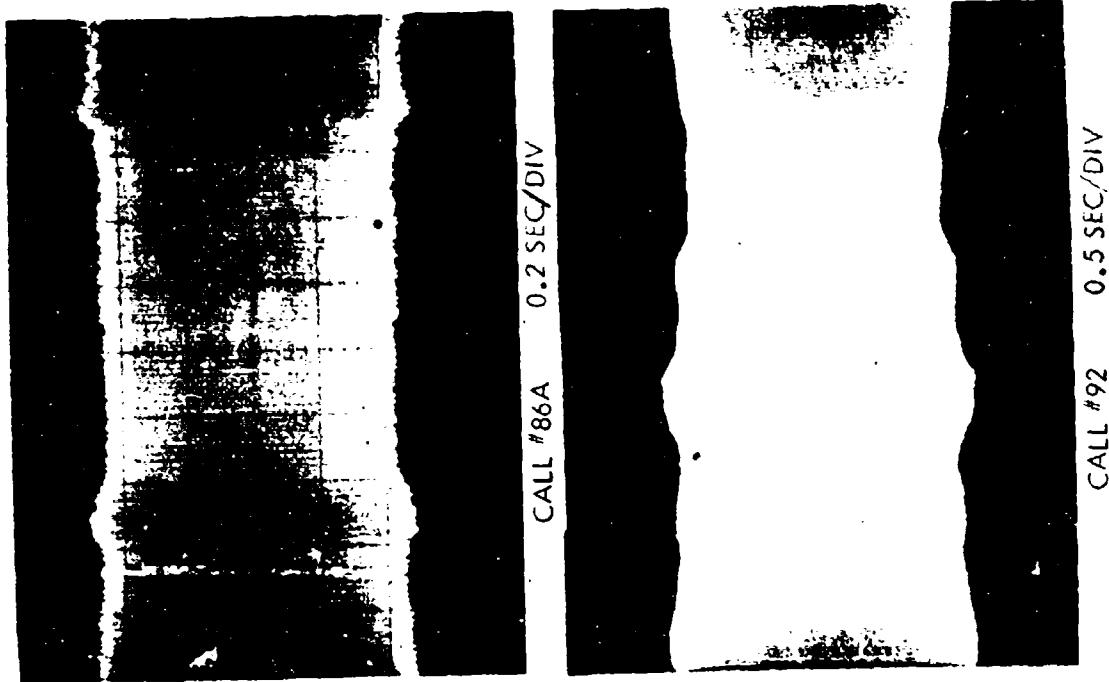
CALL #30 0.2 SEC/DIV

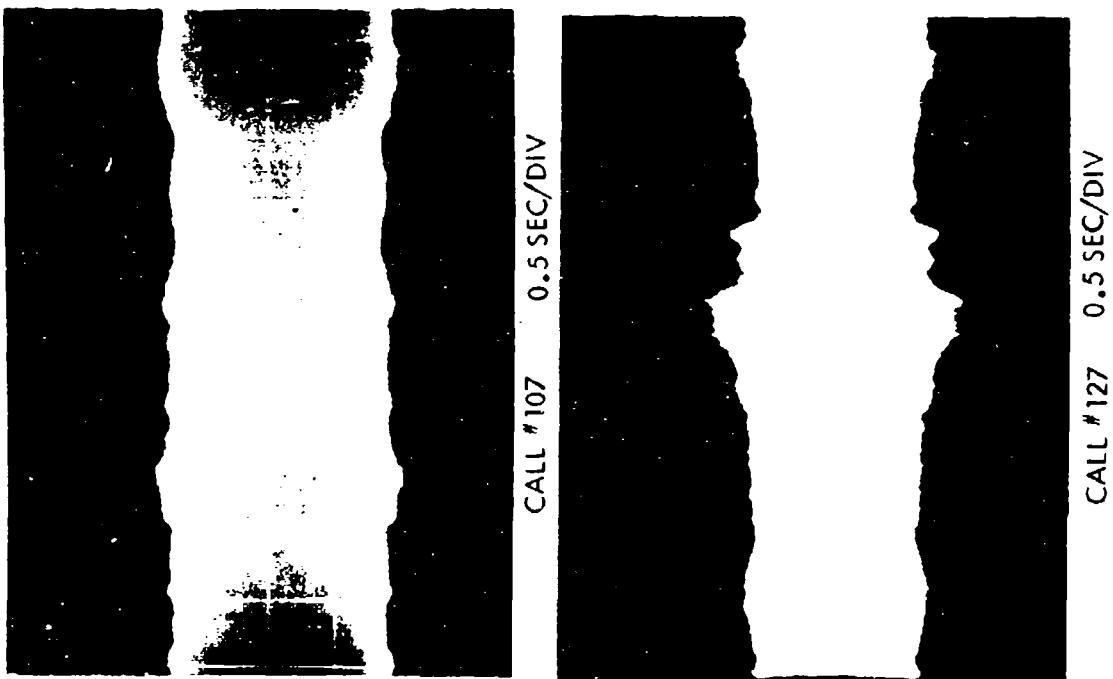
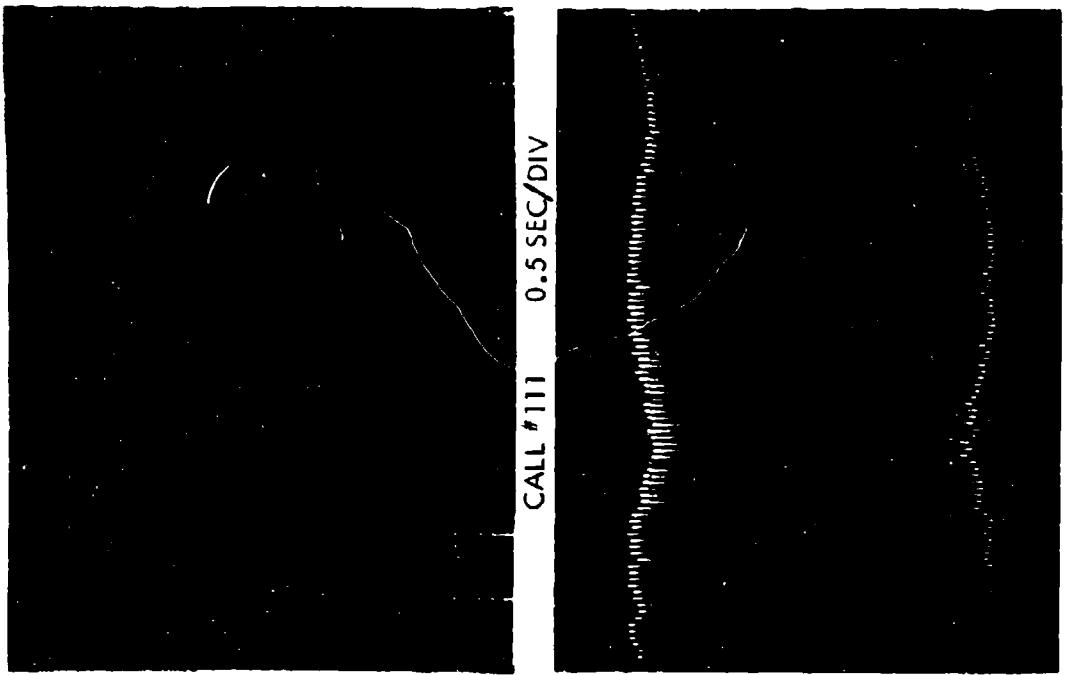


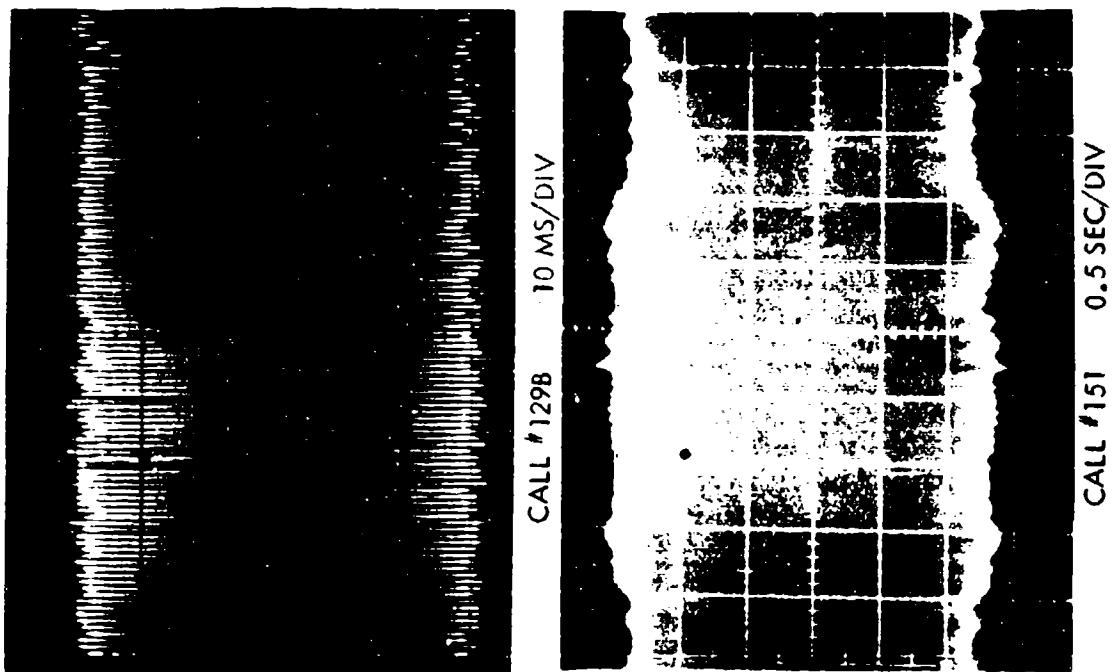
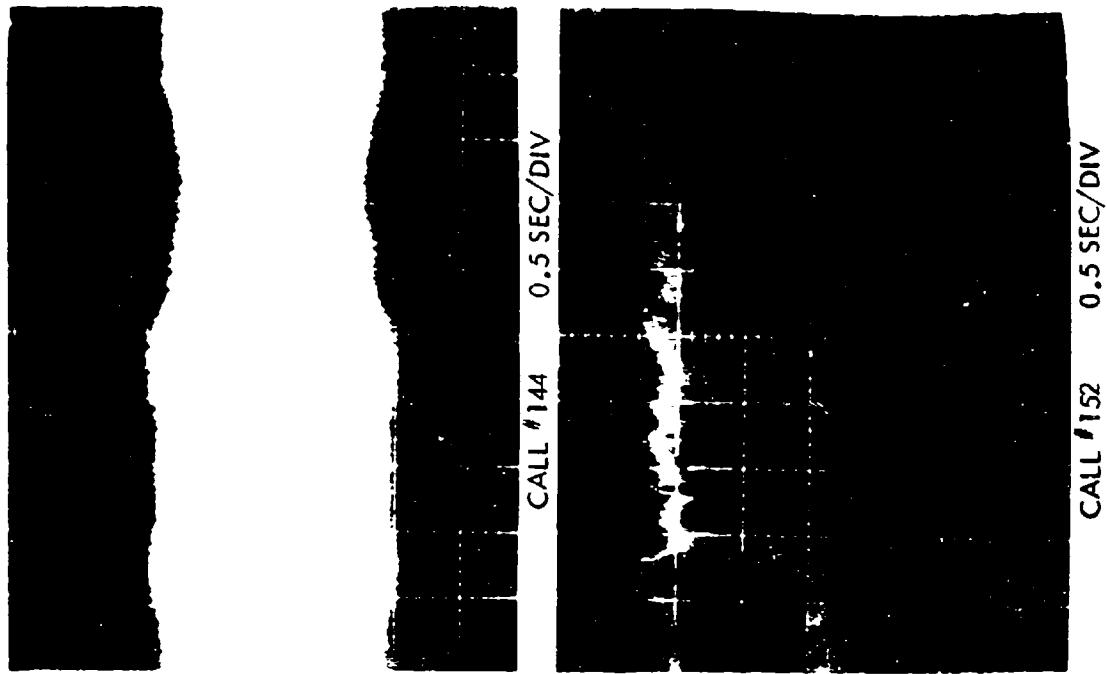
CALL #35 0.2 SEC/DIV

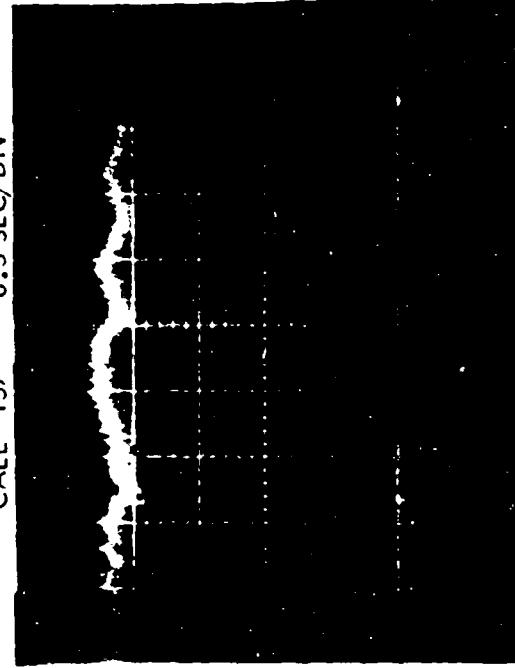
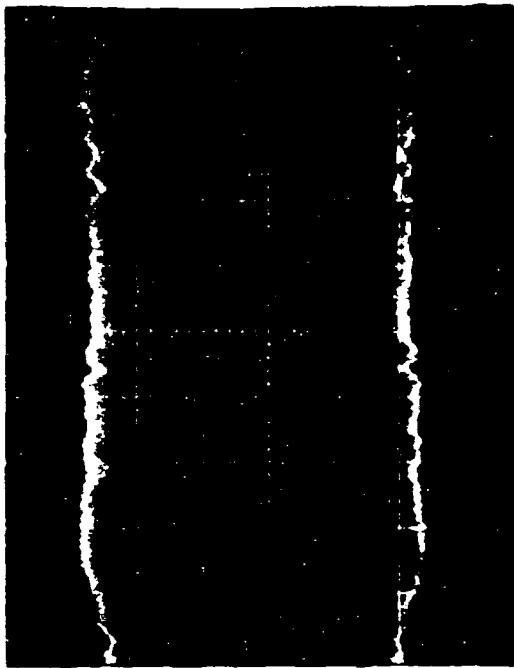




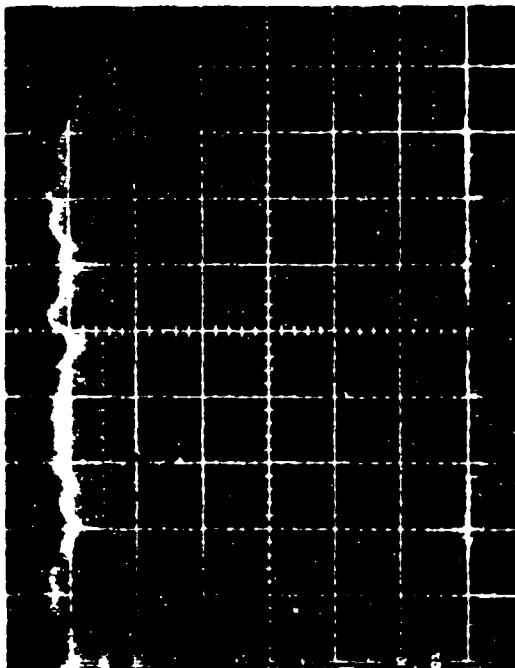




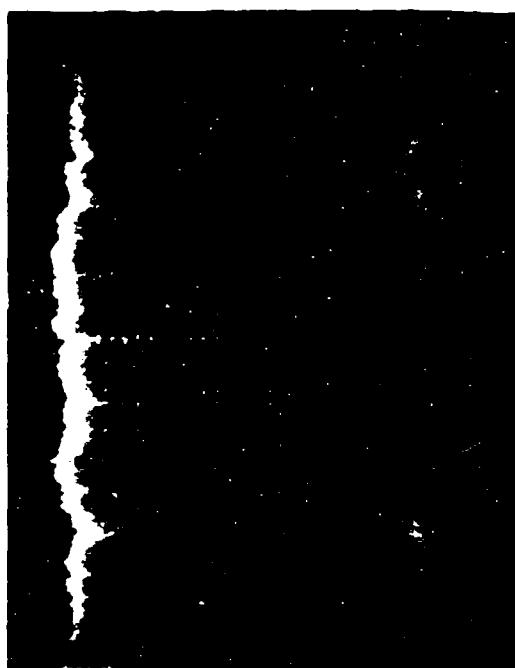




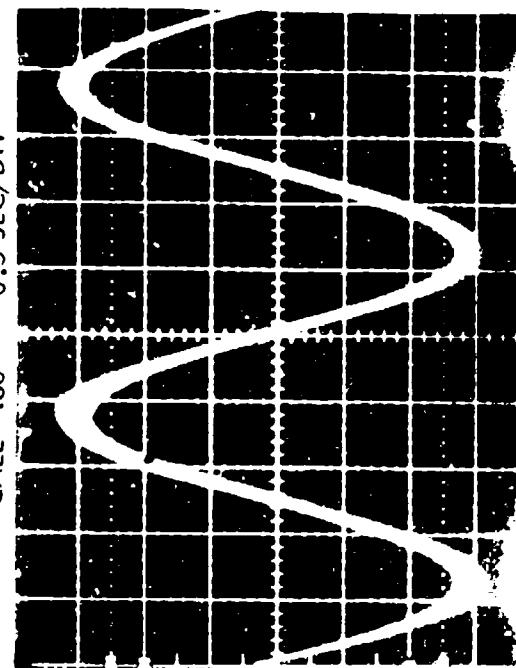
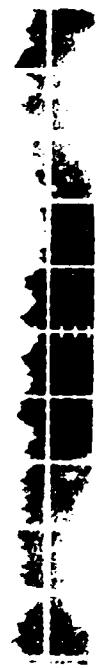
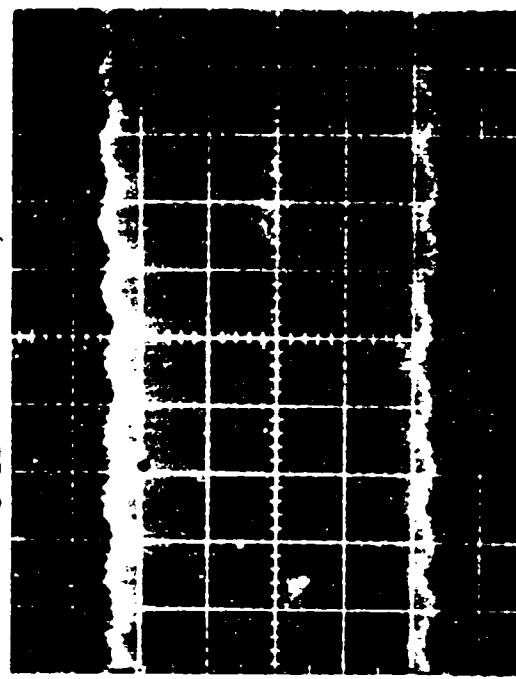
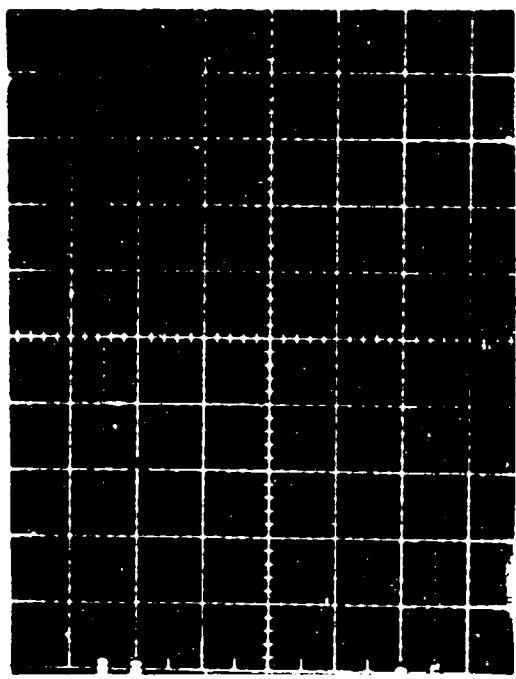
CALL #162 0.5 SEC/DIV



CALL #154 0.5 SEC/DIV



CALL #158 0.5 SEC/DIV

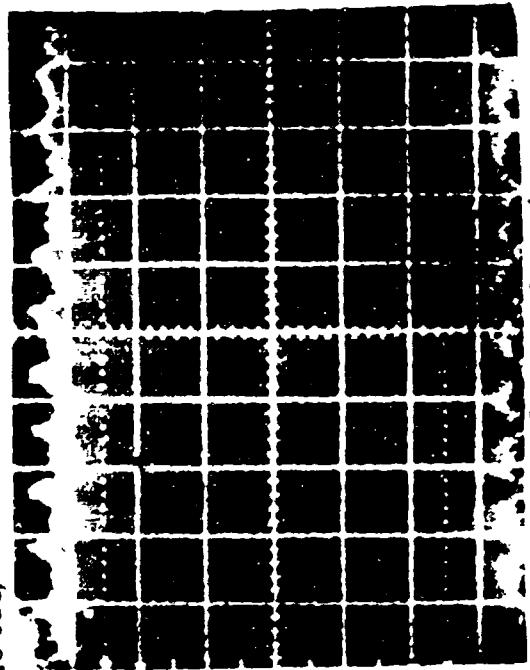


CALL #240



CALL #297

CALL #292 0.5 SEC/DIV



CALL #313 20 MS/DIV

Several unusual cases were also photographed:

- a. Call number 181 exhibited a high frequency variation which is difficult to distinguish as additive or multiplicative.
- b. Two cases of severe distortion were photographed (calls 240 and 297). These illustrate the time-variant waveforms on these calls, presumably caused by combinations of distortion and frequency offset.

#### D-5

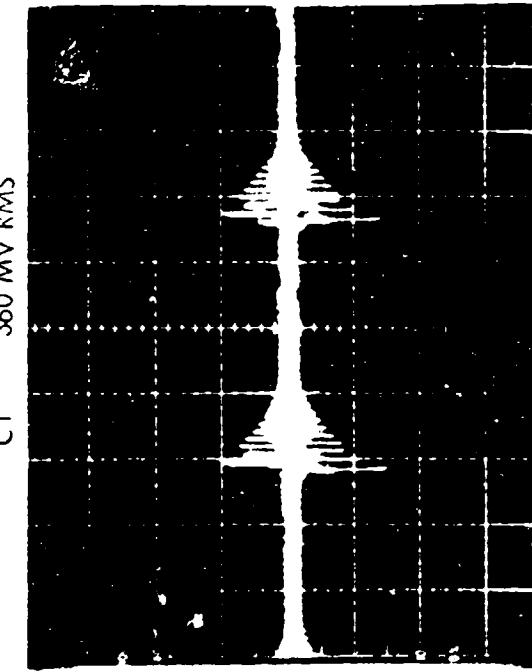
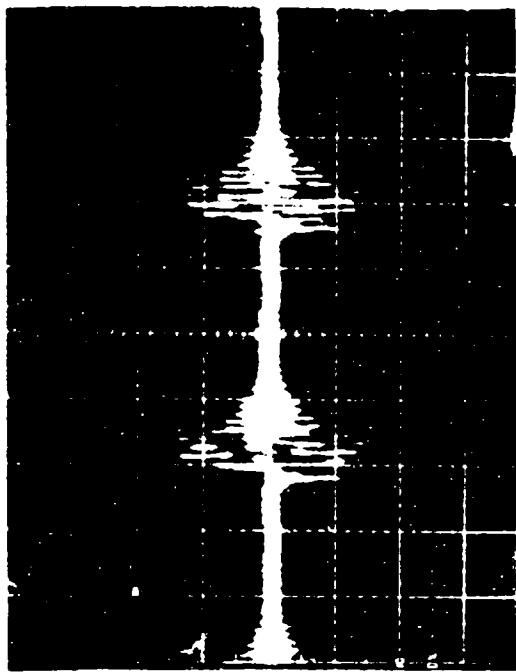
#### EQUALIZER WEIGHTS

On some calls, photographs were taken of the analog version of the equalizer weights. The calls were usually selected as having unusual or interesting weight patterns. On these photos, the two weight patterns for sine and cosine demodulator outputs are shown. The 25 ms time span of the equalizer occupies 3.75 horizontal divisions on these photos.

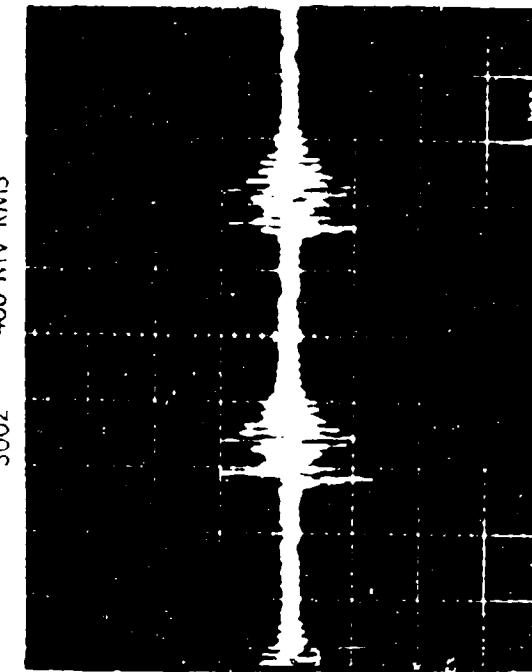
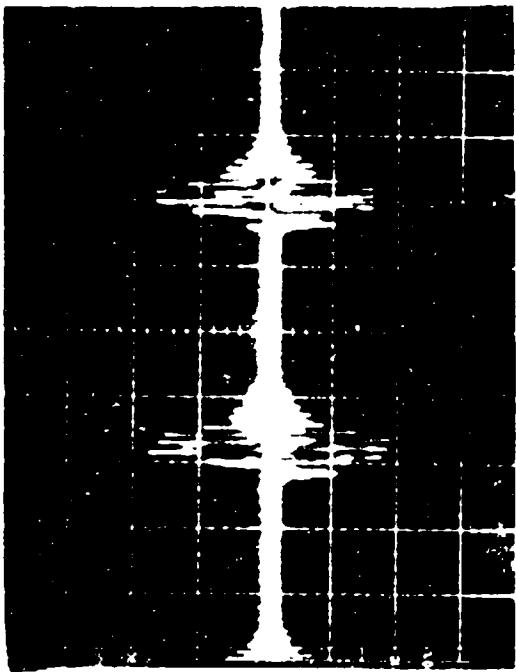
For reference, the weight patterns generated by the four simulated lines (3002, C1, C2, C4) of the Axel line simulator are shown.

It was found difficult to assess the significance of the weight patterns, although calls like No. 225 are clearly harder to equalize than, say, call No. 170. Long weight patterns, such as call No. 188 are attributed to reflections due to poor terminations at some point in the circuit.

**EQUALIZER WEIGHTS**



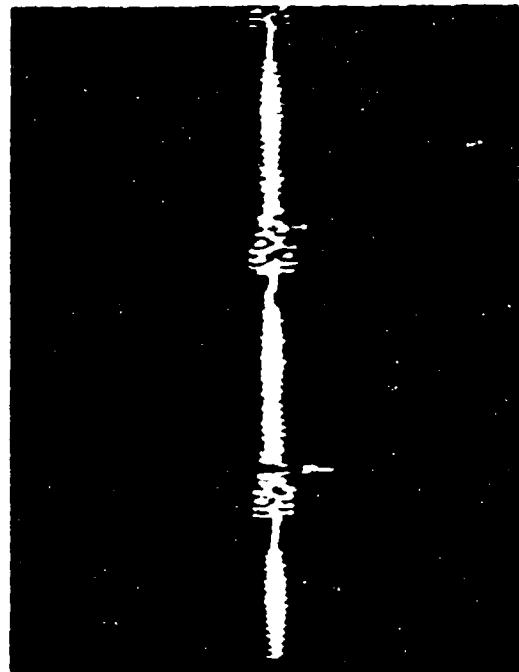
C1  
240 MV RMS



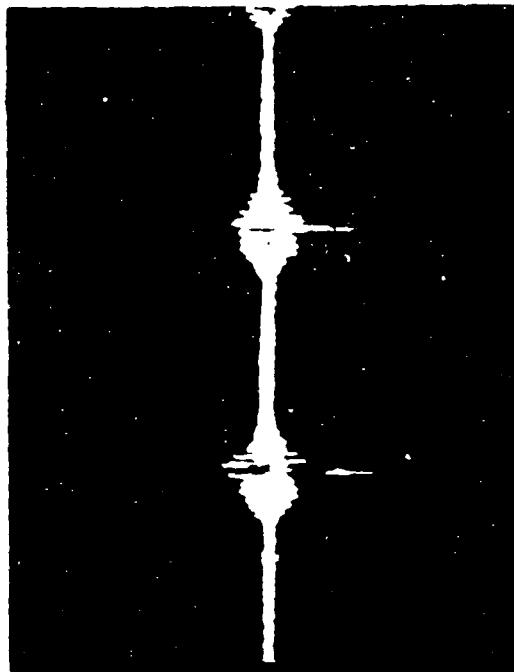
C2  
250 MV RMS



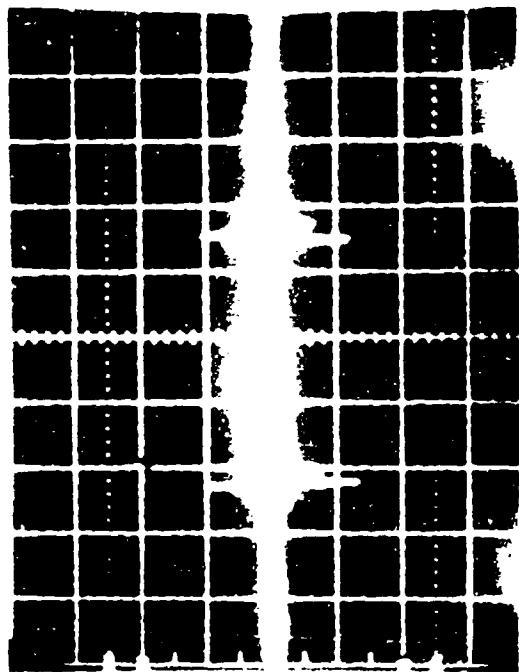
CALL #45



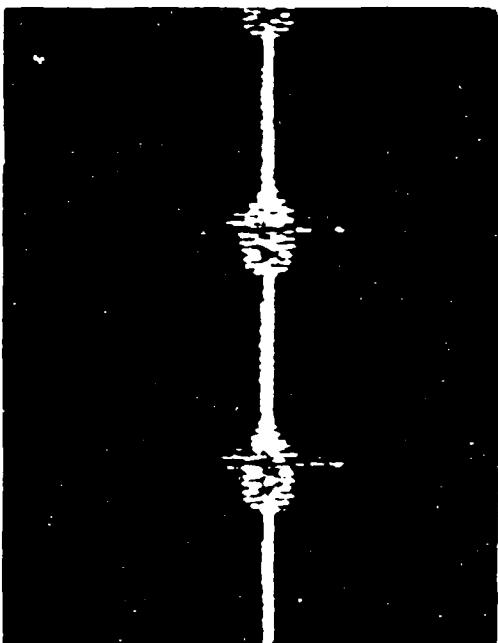
CALL #63



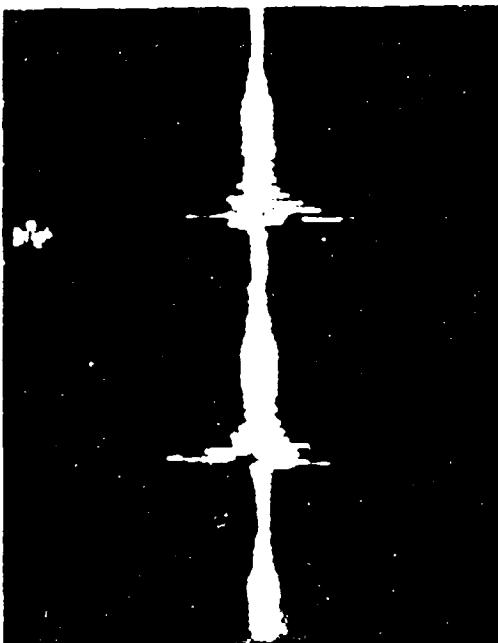
CALL #44



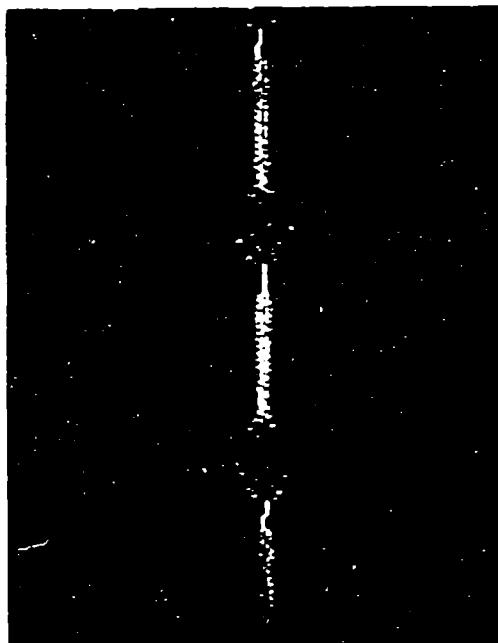
CALL #56



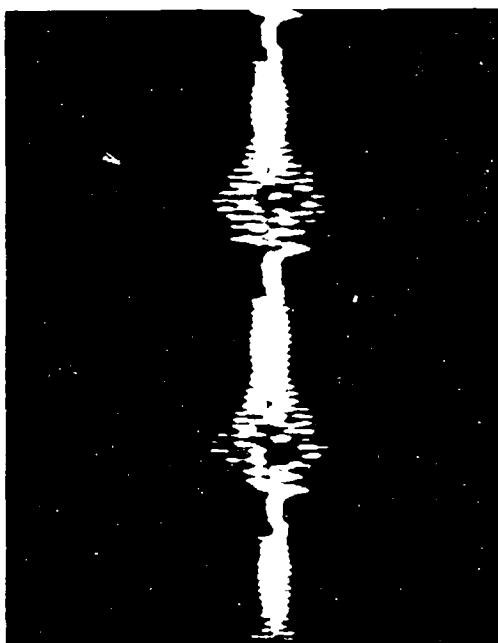
CALL #106



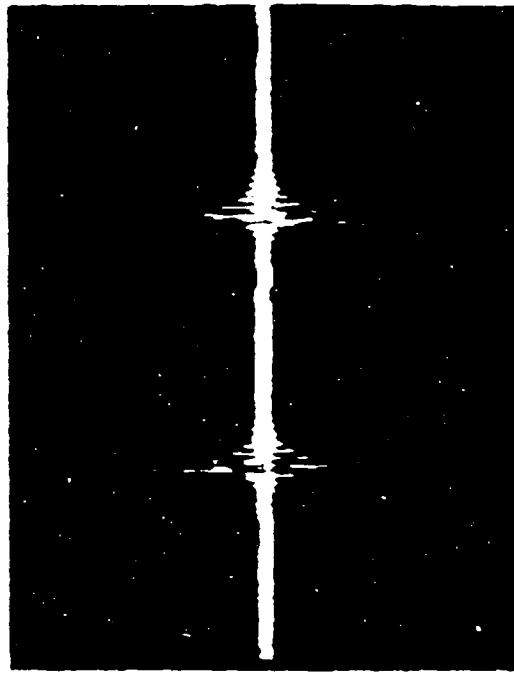
CALL #156



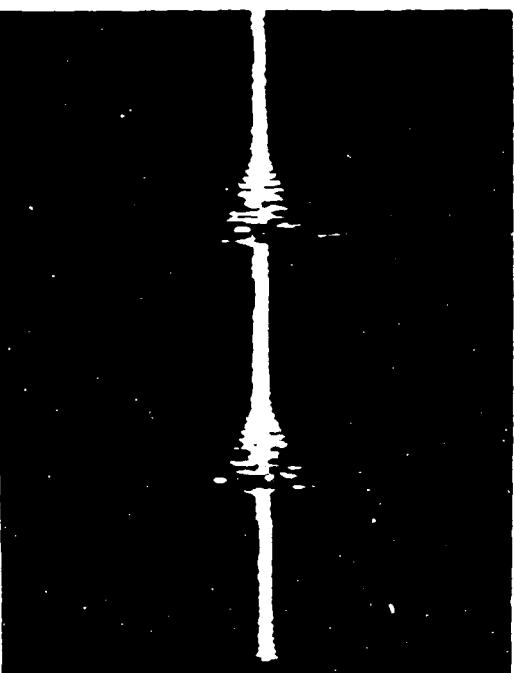
CALL #65



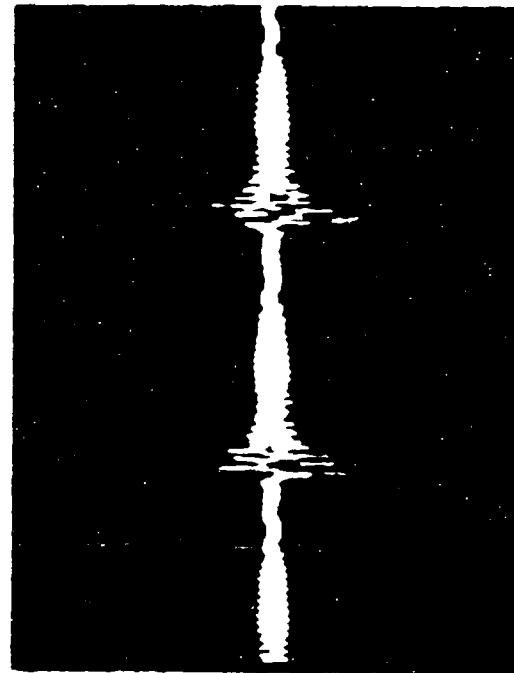
CALL #129B



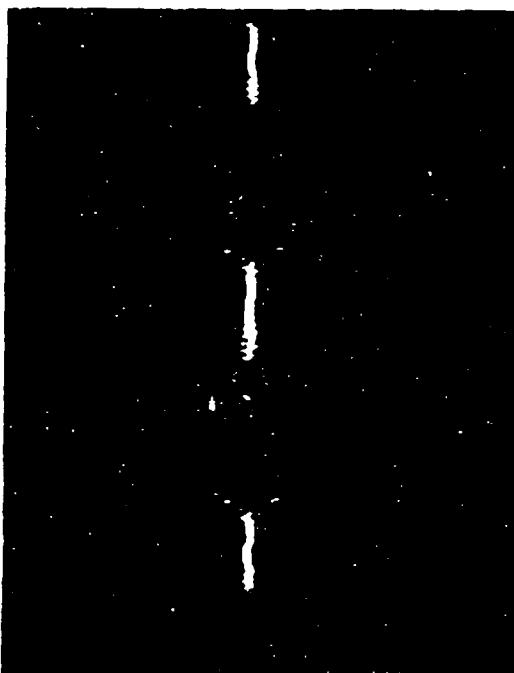
CALL #164



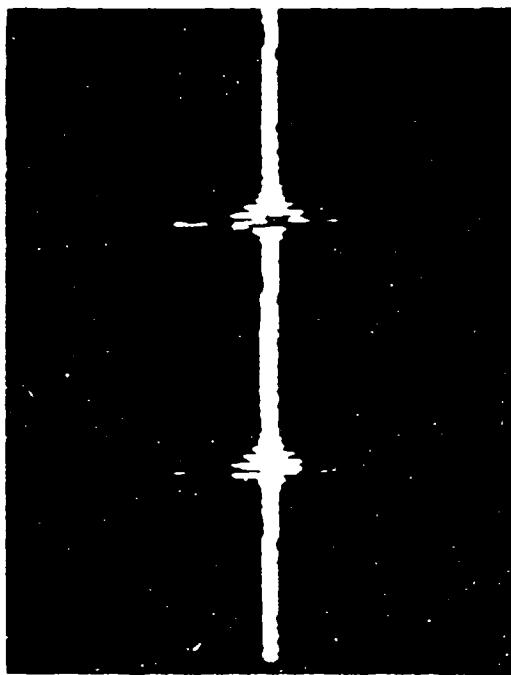
CALL #167



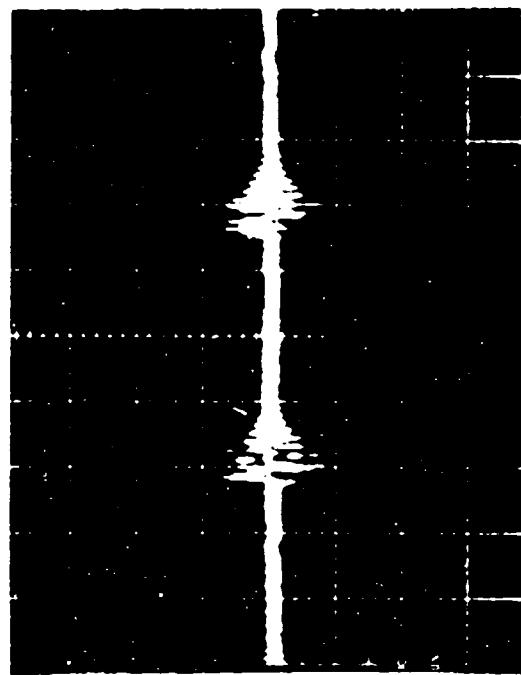
CALL #162



CALL #165



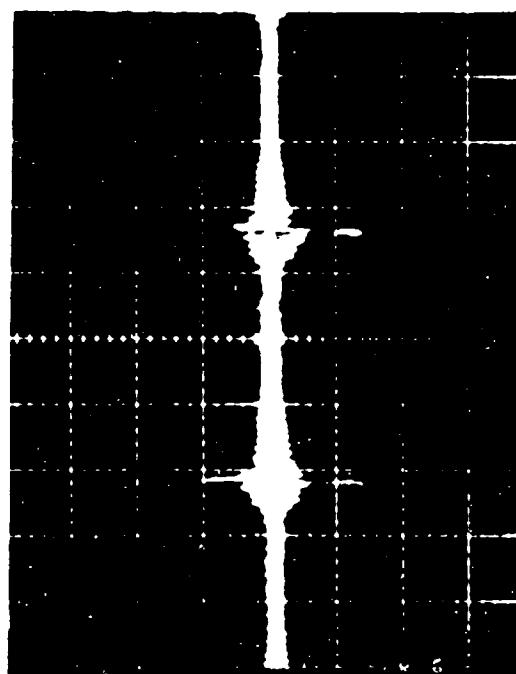
CALL #170



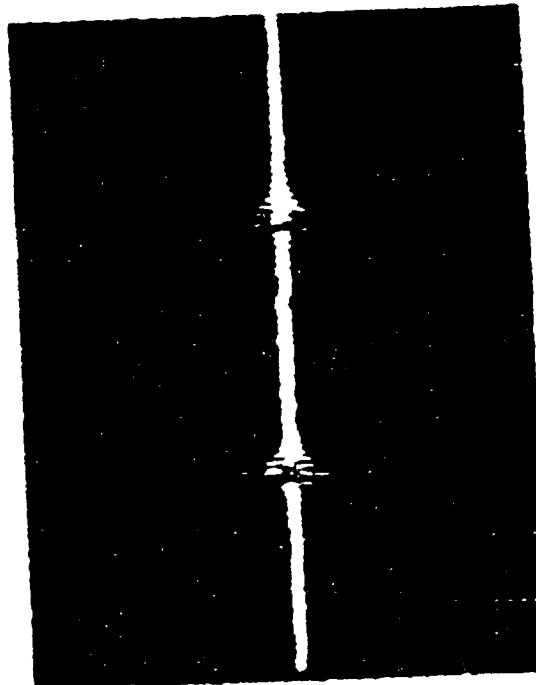
CALL #173



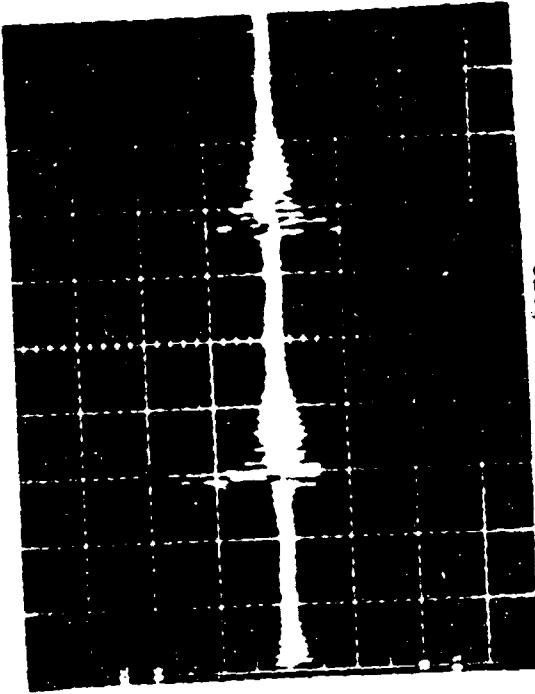
CALL #169



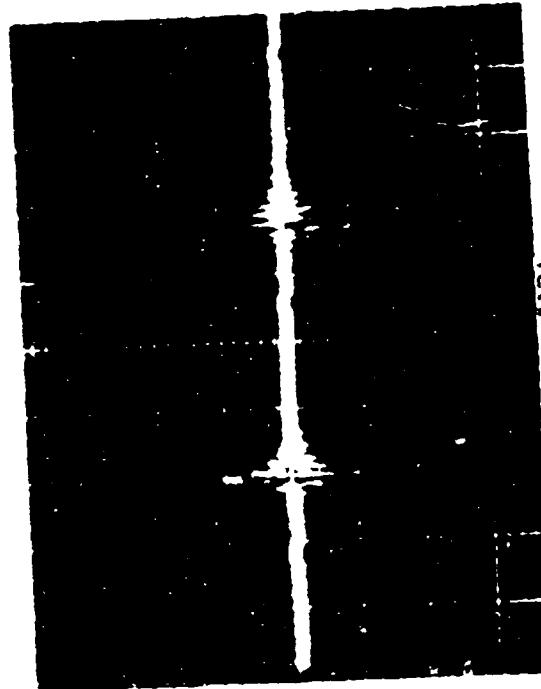
CALL #172



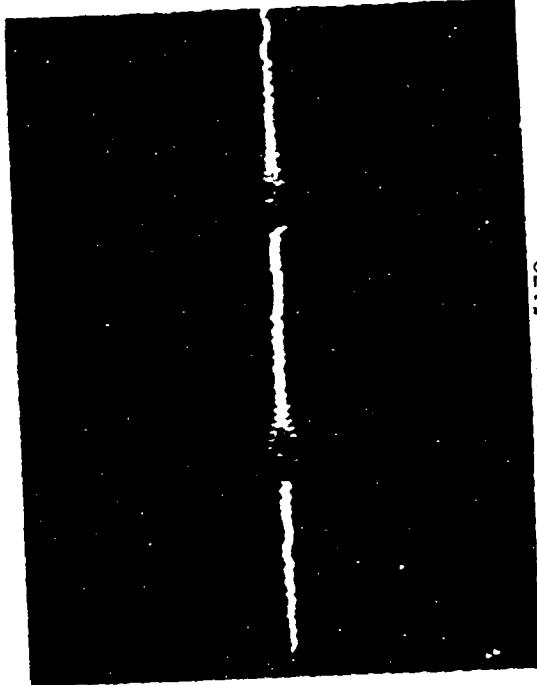
CALL #175



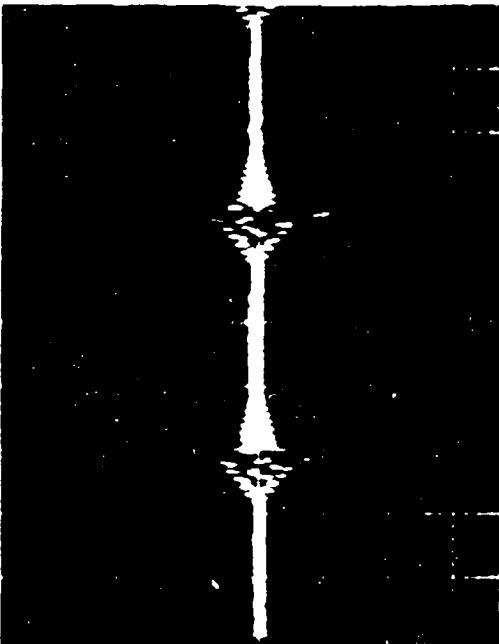
CALL #179



CALL #174



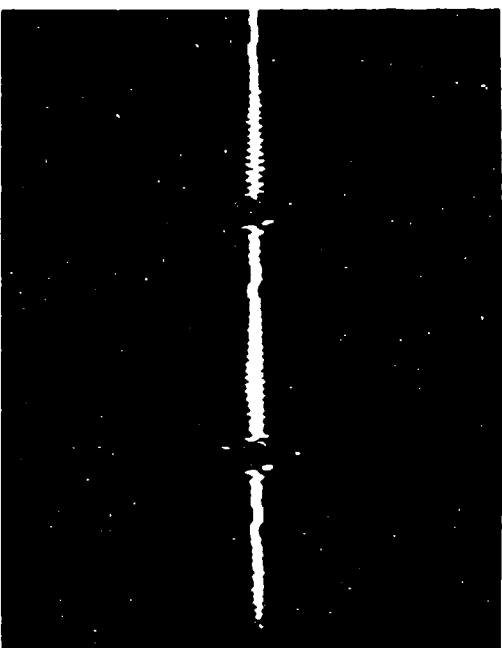
CALL #178



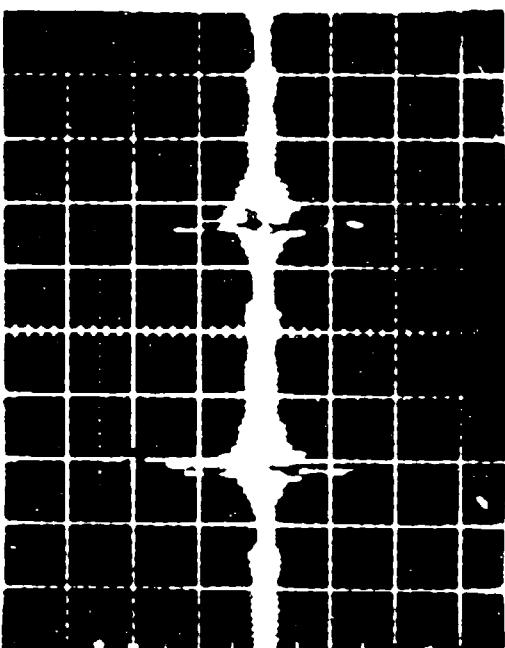
CALL #181



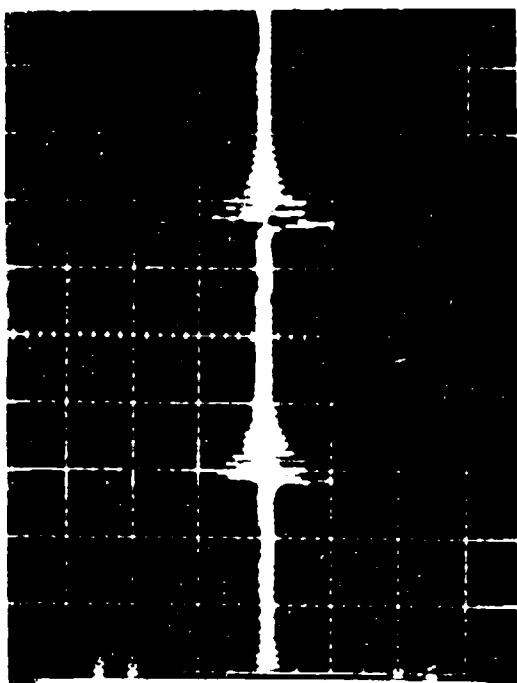
CALL #186



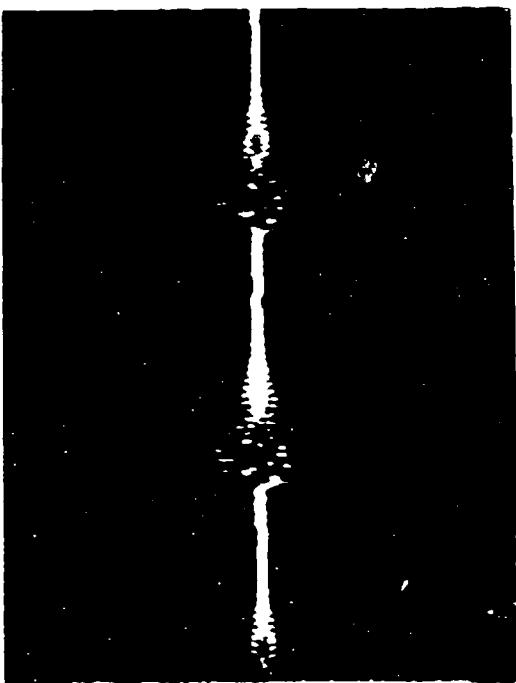
CALL #180



CALL #182



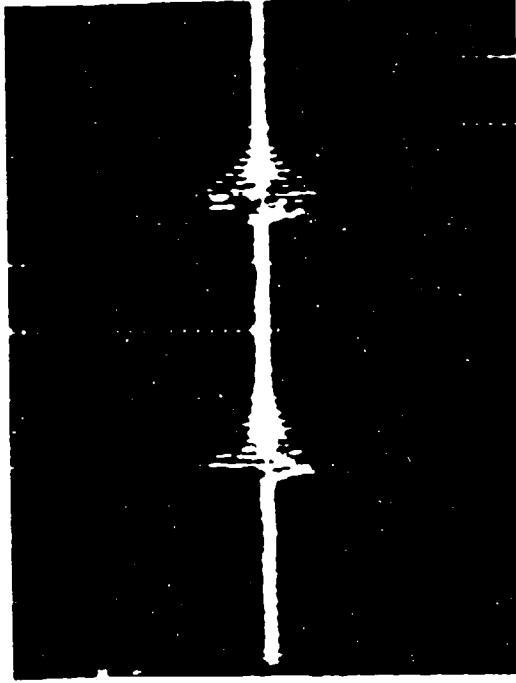
CALL #190



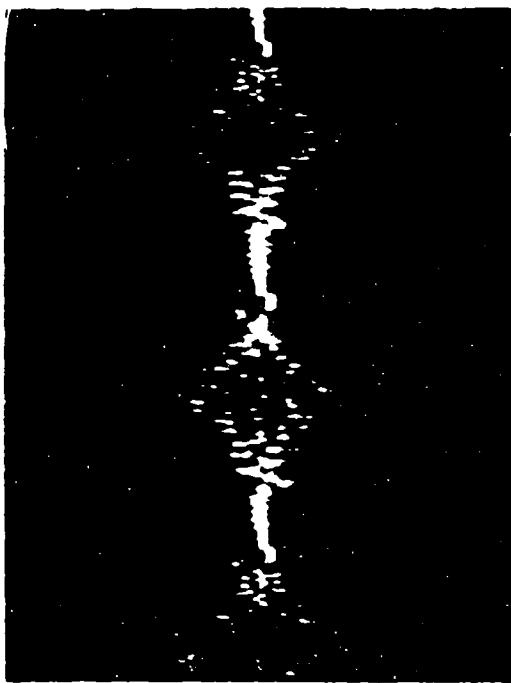
CALL #210



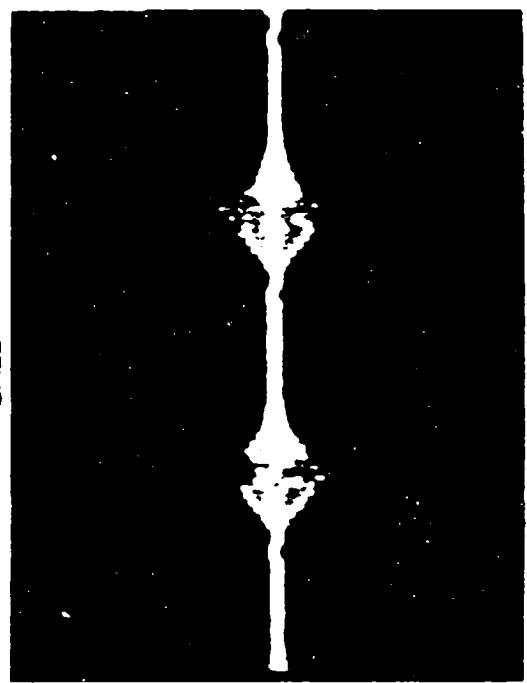
CALL #188



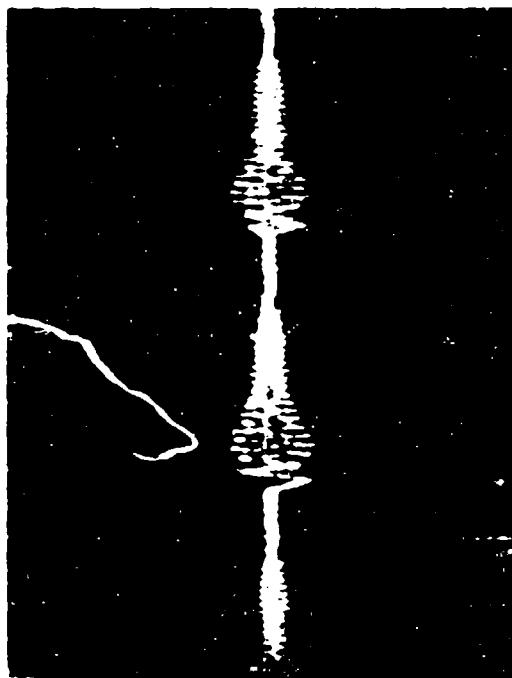
CALL #196



CALL #225



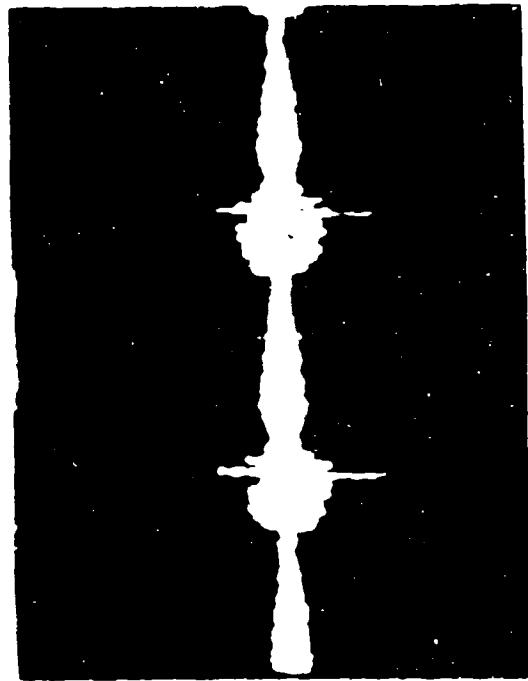
CALL #312



CALL #224



CALL #292



CALL #313

## APPENDIX E

### TEST SENTENCES

The following test sentences, from the 1965 revised list of phonetically balanced sentences from IEEE recommended practice for speech quality measurements,<sup>12</sup> were used during the test program. The particular list used for each call is given in the data tables of Appendix C.

List 1:

The birch canoe slid on the smooth planks.

Glue the sheet to the dark blue background.

It's easy to tell the depth of a well.

These days a chicken leg is a rare dish.

Rice is often served in round bowls.

The juice of lemons makes fine punch.

The box was thrown beside the parked truck.

The hogs were fed chopped corn and garbage.

Four hours of steady work faced us.

A large size in stockings is hard to sell.

List 2:

The boy was there when the sun rose.

A rod is used to catch pink salmon.

The source of the huge river is the clear spring.

Kick the ball straight and follow through.

Help the woman get back to her feet.

A pot of tea helps to pass the evening.

Smokey fires lack flame and heat.

The soft cushion broke the man's fall.

The salt breeze came across from the sea.

The girl at the booth sold 50 bonds.

List 3:

The small pup gnawed a hole in the sock.  
The fish twisted and turned on the bent hook.  
Press the pants and sew a button on the vest.  
The swan dive was far short of perfect.  
The beauty of the view stunned the young boy.  
Two blue fish swam in the tank.  
Her purse was full of useless trash.  
The colt reared and threw the tall rider.  
It snowed, rained and hailed the same morning.  
Read verse out loud for pleasure.

List 4:

Hoist the load to your left shoulder.  
Take the winding path to reach the lake.  
Note closely the size of the gas tank.  
Wipe the grease off his dirty face.  
Mend the coat before you go out.  
The wrist was badly strained and hung limp.  
The stray cat gave birth to kittens.  
The young girl gave no clear response.  
The meal was cooked before the bell rang.  
What joy there is in living.

List 5:

A king ruled the state in the early days.  
The ship was torn apart on the sharp reef.  
Sickness kept him home the third week.  
The wide road shimmered in the hot sun.  
The lazy cow lay in the cool grass.  
Lift the square stone over the fence.  
The rope will bind the 7 books at once.  
Hop over the fence and plunge in.  
The friendly gang left the drug store.  
Mesh wire keeps chicks inside.

List 6:

The frosty air passed through the coat.  
The crooked maze failed to fool the mouse.  
Adding fast leads to wrong sums.  
The show was a flop from the very start.  
A saw is a tool used for making boards.  
The wagon moved on we'll oiled wheels.  
March the soldiers past the next hill.  
A cup of sugar makes sweet fudge.  
Place a rose bush near the porch steps.  
Both lost their lives in the raging storm.

List 7:

We talked of the side show in the circus.

Use a pencil to write the first draft.

He ran halfway to the hardware store.

The clock struck to mark the third period.

A small creek cut across the field.

Cars and busses stalled in the snow drift.

The set of china hit the floor with a crash.

This is a grand season for hikes on the road.

The dune rose from the edge of the water.

Those words were the cue for the actor to leave.

List 8:

A yacht slid around the point into the bay.

The two met while playing on the sand.

The ink stain dried on the finished page.

The walled town was seized without a fight.

The lease ran out in 16 weeks.

A tame squirrel makes a nice pet.

The horn of the car woke the sleeping cop.

The heart beats strongly and with firm strokes.

The pearl was worn in a thin silver ring.

The fruit peel was cut in thick slices.

List 9:

The Navy attacked the big task force.

See the cat glaring at the scared mouse.

There are more than two factors here.

The hat brim was wide and too droopy.

The lawyer tried to lose his case.

The grass curled around the fence post.

Cut the pie into large parts.

Men strive but seldom get rich.

Always close the barn door tight.

He lay prone and hardly moved a limb.

List 10:

The slush lay deep along the street.

A wisp of cloud hung in the blue air.

A pound of sugar costs more than eggs.

The fin was sharp and cut the clear water.

The play seemed dull and quite stupid.

Bail the boat; stop it from sinking.

The term ended in late June that year.

A tusk was used to make costly gifts.

Ten pins were set in order.

The bill was paid every third week.

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8. "Leased Overseas Circuits and CONUS Extension Report," (DECCO(M) 650-9, 31 Oct. 1976, Pacific Area, Defense Communications Agency, APO 96515 San Francisco, Cal.
9. "NCS Transoceanic Circuits," NCS 0070, 370-026, 17 Nov. 1976, Pacific Area, Defense Communications Agency, APO 96515, San Francisco, Cal.
10. "The World's Submarine Telephone Cable Systems," Department of Commerce, August 1975, Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402.
11. DCA Pacific Circuit/MUX Diagrams dated 1 July 1976.
12. 1965 Revised List of Phonetically Balanced Sentences from IEEE Recommended Practice for Speech Quality Measurements.

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RADC plans and conducts research, exploratory and advanced development programs in command, control, and communications (C<sup>3</sup>) activities, and in the C<sup>3</sup> areas of information sciences and intelligence. The principal technical mission areas are communications, electromagnetic guidance and control, surveillance of ground and aerospace objects, intelligence data collection and handling, information system technology, ionospheric propagation, solid state sciences, microwave physics and electronic reliability, maintainability and compatibility.





DEPARTMENT OF THE AIR FORCE  
AIR FORCE RESEARCH LABORATORY (AFRL)

1 Jun 04

MEMORANDUM FOR DTIC-OCQ

ATTN: Larry Downing  
Ft. Belvoir, VA 22060-6218

FROM: AFRL/IFOIP

SUBJECT: Distribution Statement Change

1. The following documents have been reviewed and have been approved for Public Release; Distribution Unlimited:

ADB084552, "Project Birdwatch at Dover AFB", RADC-TR-84-7

ADB191869, "Acousto-Optic Beam Steering Study", RL-TR-94-121

AD0800669, "Use of Commercial Broadcast Facilities for Emergency DoD Communications", RADC-TR-66-392

ADB058979, "Multi-Rate Secure Processor Terminal Architecture Study", RADC-TR-81-77, Vol 1.

ADB053656, "16 KB/S Modem (AN/GCS-38) CONUS Test", RADC-TR-80-89

ADB055136, "VINSON/AUTOVON Interface Applique for the Modem, Digital Data, AN/GCS-8", RADC-TR-80-341

ADB043556, "16 KB/S Data Modem Partitioning", RADC-TR-79-278

ADB029131, "16 Kilobit Modem Evaluation", RADC-TR-78-127.

2. Please contact the undersigned should you have any questions regarding this document. Thank you very much for your time and attention to this matter.

*Kelly Cagwin*  
KELLY CAGWIN  
STINFO Officer  
Information Directorate  
315-330-7094/DSN 587-7094